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AN EULERIAN METHOD FOR CALCULATING STRENGTH
DEPENDENT DEFORMATION

PART THREE

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PART THREE

THE FORTRAN IV PROGRAM AND INSTRUCTIONS FOR ITS USE

by

J. K. Dienes, M. W. Evans, L. J. Hageman,
W. E. Johnson, and J. M. Walsh

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1. INTRODUCTION

In PART ONE of the OIL-RPM report the equations of motion were derived from first principles and discussed from a fundamental point of view. PART TWO then described the difference equations, the equation of state, the constitutive equations and the differencing scheme for velocity gradients used in formulating the FORTRAN IV program. Here, in PART THREE, the computer program is listed in detail and the general information necessary to set up and run problems is provided. A dictionary of terms used in the program is also included, as well as a number of tables and charts describing the program in outline form. Forms for setting up a sample problem are also given. This information provides the user with a capability to run his own problems and, in addition, the intent is to describe the code in enough detail that any changes the user may require can be readily made.

The program is the result of contributions by quite a number of people whose names are cited in the references. Briefly, the techniques described here originated from the PIC particle-in-cell method developed at Los Alamos by Evans and Harlow⁽¹⁾ and programmed in machine language. The code was rewritten in FORTRAN and modified for application in the ORION program by Johnson⁽²⁾ and the General Atomic version was called SHELL. At the suggestion of B. E. Freeman a continuous version was developed by Walsh and Johnson⁽³⁾ for the solution of hypervelocity impact problems and called OIL. It made use of the equation of state programmed by Tillotson⁽⁴⁾. To develop OIL, the particles were replaced by a continuously varying mass in each cell. The capability to run multi-material problems could not be conveniently retained (the particles in PIC could be of different materials). However, the cost of running problems was significantly reduced and the flow profiles were substantially smoother, making it practical to run impact and explosion problems out to a time when the shock pressure was down to a few kilobars. The lowest pressure that could be resolved with PIC was several hundred kilobars.

In order to compute crater size from an impact directly, the shear strength of the cratered material had to be accounted for. The necessary changes to OIL were made in an experimental way by Johnson, Walsh, and Dienes in 1965. This modified version of OIL was called OIL-RPM.⁽⁵⁾

Subsequently, when it had been shown that crater size could be calculated with satisfactory accuracy, the program was streamlined by the authors so it could be used in production runs, and additional editing features were incorporated. The current version has been used in calculating over 50 different problems and the results have generally compared well with experiments, analytical solutions and other hydrodynamic codes.

2. DESCRIPTION OF THE PROGRAM

The equations of motion are integrated in Phases 1, 2 and 3 which account for the effect of pressure, transport, and shear stresses respectively. In addition to these subroutines, ten others have been introduced for the various peripheral tasks. These include INPUT, SETUP, CARDS, CDT (computes time step), EDIT, MAP (provides displays), ES (equation of state), REZONE and ERROR. "RPM" is used to denote both the routine controlling the main flow and the entire program; the choice is generally made clear by the context. A summary of the subroutines is given in Table 1 in the order in which they appear in the listing provided in Section 6. Included in the table are the names of the subroutines calling and called by each of the others. A few general comments are made in the paragraphs below on each of the subroutines.

2.1. RPM

The overall flow of the program is controlled by RPM, as shown in the flow chart of Fig. 1. RPM controls whether additional information is printed at intermediate phases of the calculation cycle for diagnostic purposes and debugging. The variable "INTER" controls these intermediate prints. When INTER = 0, no intermediate prints are made. When INTER \neq 0 EDIT is called and on print cycles EDIT prints are made after PH1 and PH3 as well as after CDT. Details of the Phase 2 calculation are obtained in addition to the EDIT prints by putting INTER = 7, which causes printing of the energy and mass transported as each cell is processed. For debugging of Phase 3 difficulties one puts INTER = 99 and thereby obtains detailed prints of stresses, strain rates and a few other parameters. These options should be used with extreme caution since an intermediate print uses considerable paper.

2.2. INPUT

Instructions for running problems are interpreted by INPUT, which can either start or restart a calculation. It calls SETUP and CARDS, as necessary, to prescribe the initial conditions and to read the input deck. A flow chart showing the relation of INPUT, CARDS, and SETUP is provided in Fig. 2.

TABLE 1
ORDER OF SUBROUTINES

Name	Called From	Calls
RPM	--	INPUT, CDT, EDIT PH1, PH2, PH3
INPUT	RPM	SETUP, CARDS
CARDS	INPUT, SETUP	--
SETUP	INPUT	CARDS, ERROR
CDT	RPM, EDIT	ES, ERROR
ES	CDT	--
EDIT	RPM, ERROR	MAP, REZONE, ERROR, CDT
MAP	EDIT	--
PH1	RPM	--
PH3	RPM	--
PH2	RPM	ERROR
REZONE	EDIT	--
ERROR	SETUP, CDT EDIT, PH2	EDIT

FLOW OF THE CONTROL SUBROUTINE "RPM"

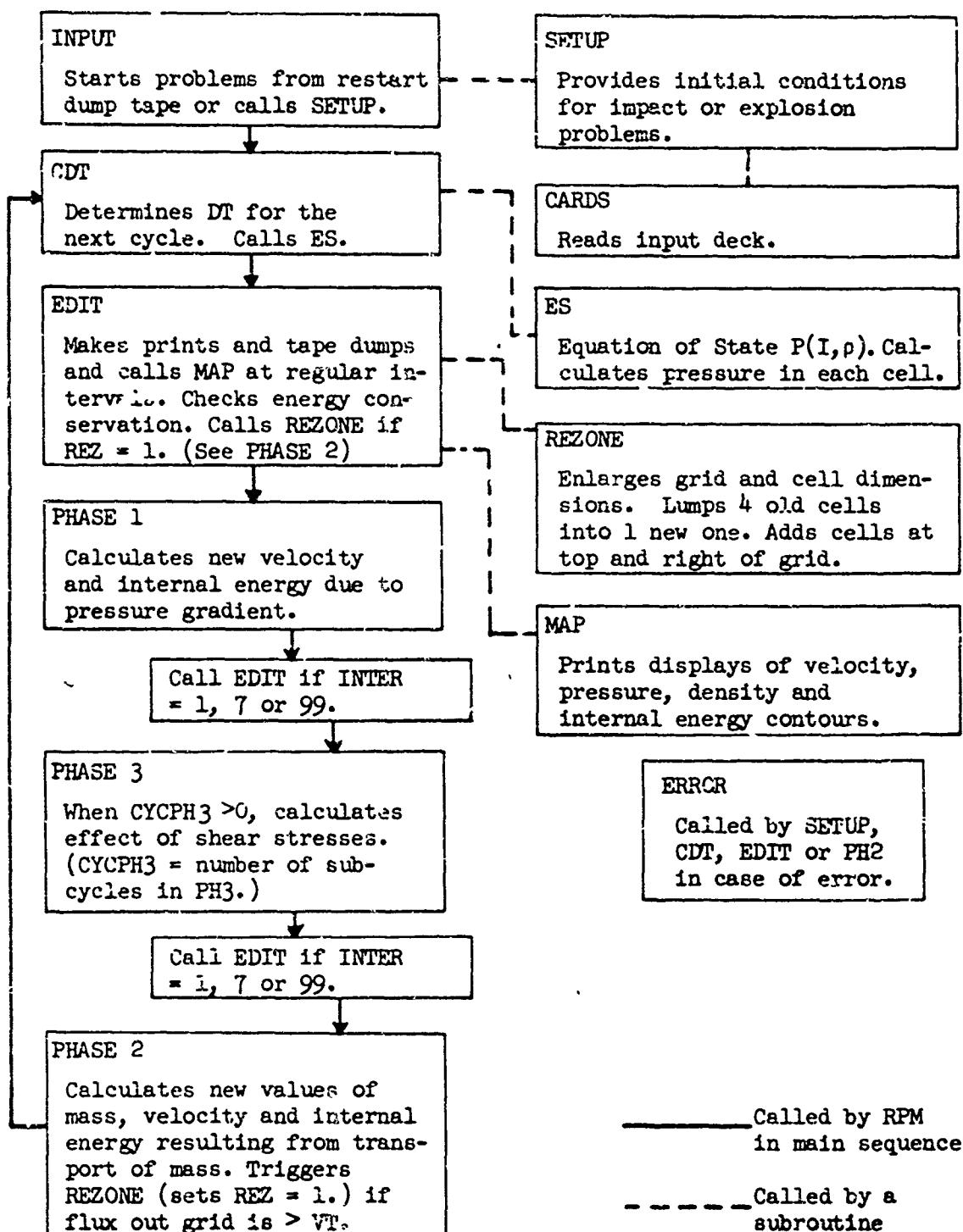


Fig. 1--Flow chart of main sequence

FLOW DIAGRAM OF INPUT, CARDS AND SETUP

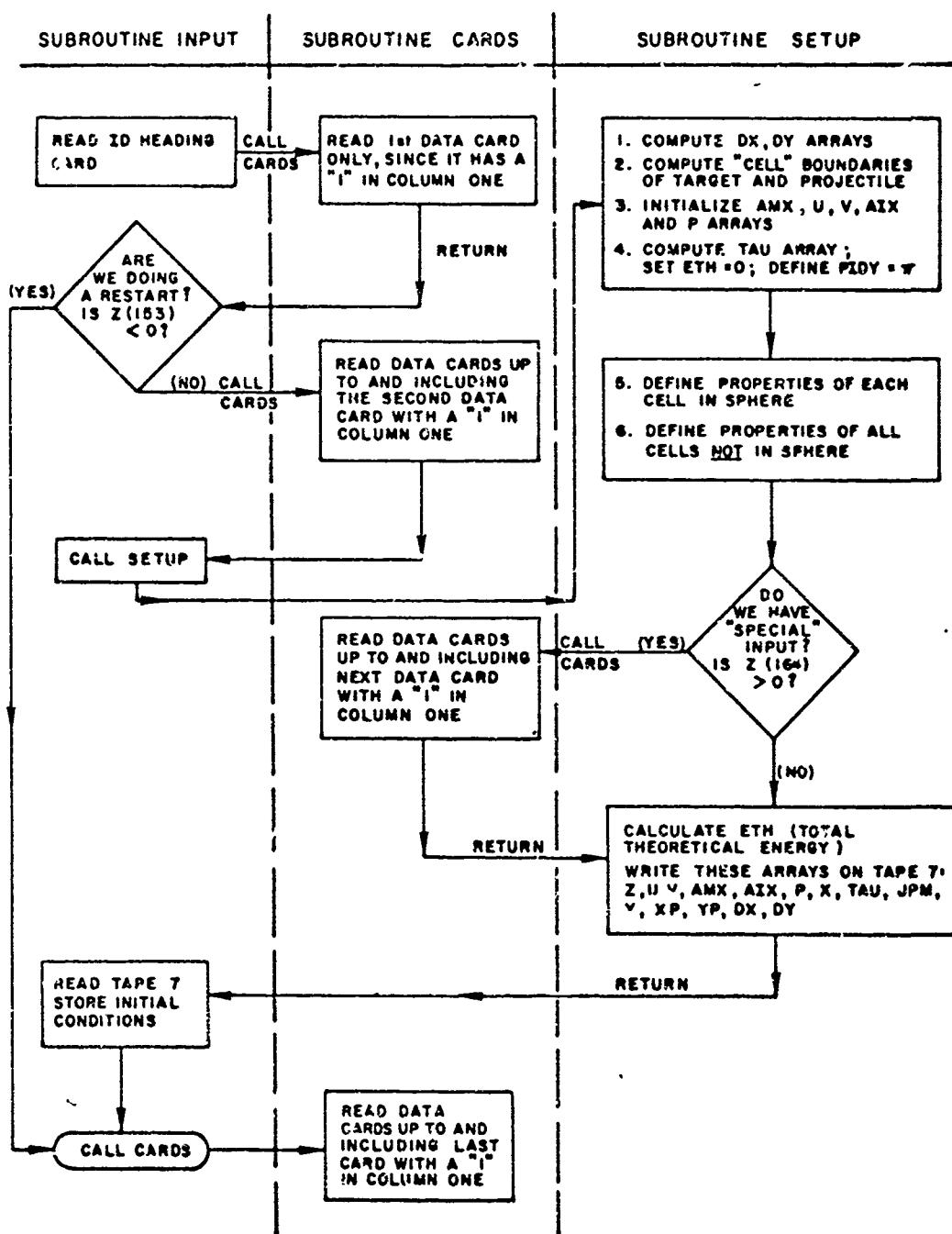


Fig. 2

2.3. CARDS

The reading of the input deck is called by this simple subroutine. Details are given in Fig. 2.

2.4. SETUP

The initial conditions for running problems are generated by SETUP. The most commonly used options are those in which a sphere or a cylinder (called the projectile) hits a target of finite thickness. The target of infinite thickness is an important special case. Another option is a geometry in which a sphere hits a thin plate (called the projectile) which has a filler behind it (typically void or of underdense "foamy" material) and then hits a second thin plate behind the filler. Further details are given in Section 3 describing how to set up various problems.

In an earlier report⁽³⁾ describing the OIL code a description and FORTRAN listing of a special generator code, CLAM, was given. This program provides a very general method for specifying initial conditions and for setting up OIL-RPM problems. A few changes in CLAM are required to make the write statements for the CLAM dump tape compatible with the READ statements in OIL-RPM,

2.5. CDT

The principal function of this subroutine is to compute a time step which ensures stability of the finite difference equations. This is done by finding the minimum of D/w for all the cells. Here D denotes the minimum of the radial and axial cell dimensions, and w denotes the maximum of the radial velocity, axial velocity and sound speed. For vaporized material sound speed is computed by $\sqrt{\gamma p/\rho}$ and for solid materials by the approximate relation $C = C_0 + \bar{B} \sqrt{p}$ where p is the pressure in the cell. The coefficient \bar{B} is obtained by determining a typical slope for the isentropes in Ref. 4 and using the relation

$$C = V \sqrt{-\delta p/dV}$$

to evaluate \bar{B} at a particular point. The pressure array is updated in CDT by calling the equation of state subroutine ES.

The array JPM(I) which determines the location of the pressure maximum and hence the cells on which deviator stresses act is also computed in CDT.

Unrealistic behavior in free surface cells containing a small amount of mass would occur, in the absence of a special treatment, when a neighboring cell has a high pressure. This causes large accelerations of the mass in the cell containing a free surface, and eventually velocities which are physically unrealistic. This difficulty is alleviated by reducing the pressure computed by the equation of state by a factor which is the ratio of the smallest mass in an adjacent cell to the mass in the cell itself. This factor reduces the pressure at the interface to a value which accounts for the position of the free surface.

2.6. ES

The equation of state subroutine is called by CDT to evaluate the pressure as a function of density and internal energy. The general method was originally described in Ref. 4, but a number of modifications have been made since that report was written. A general discussion is given in Section 4 of PART TWO. Values of the parameters for a number of materials are listed in Table 2. Parameters for some materials not given in Ref. 4 are supplied in Refs 6 and 7.

2.7. EDIT

The pressure, velocities, density, specific internal energy, and mass for each cell are displayed by EDIT in a "long" print. It also prints out the total internal energy, kinetic energy, axial and radial momentum and mass above and below a dividing line which is the top of the cell whose J index is JPROJ. The changes in energy due to evaporation and losses out the boundaries are also accounted for in the EDIT prints. The crater depth is calculated by "packing down" material in each column to its normal density. This describes in a rough way the extent of the crater even while it still contains low density material.

"Short" EDIT prints display the integrated quantities, and the cell variables for the one column of cells that is adjacent to the axis. These

TABLE 2
EQUATION OF STATE CONSTANTS FOR SEVERAL MATERIALS

	a	b	A lynes/cm ²	B dynes/cm ²	$\bar{\varepsilon}_0$ ergs/g	a	$\bar{\varepsilon}_S$	ρ g/cm ³	E' $\times 10^{-10}$
W	.5	1.04	3.08×10^{12}	2.5×10^{12}	.225 $\times 10^{12}$	10	10	1.11×10^{10}	19.17
Cu	.5	1.5	1.39	1.1	.325	5	5	1.38	3.9
Fe	.5	1.5	1.28	1.05	.095	5	5	2.14	7.9
Al	.5	1.63	.75	.65	.05	5	5	3.0	2.7
Be	.55	.62	1.7	.55	.175	5	5	10.0	1.8
Tl	.5	.60	1.03	.5	.07	5	5	3.5	~5
Ni	.5	1.33	1.91	1.5	.09	5	5	2.95	3.9
Mo	.2	1.02	2.11	.55	.005	5	5	2.2	10.2
Th	.4	.86	.53	.5	.025	9	.88	2.0	11.7
Granite*	.5	1.3	.19	.18	.16	5	5	3.5	2.7
Andesite*	.5	1.3	.18	.18	.15	5	5	3.5	2.7
Wet Tuff	.5	1.3	.10	.06	.11	5	5	3.2	2.0
Dry Tuff	.5	1.3	.045	.03	.06	5	5	3.2	1.7
Oil Shale	.5	1.0	.28	.11	.11	5	5	3.2	2.3
Dolomite	.5	.5	.85	.30	.10	5	5	2.5	2.8
Limestone	.5	.6	.4	.67	.10	5	5	2.5	2.7
Fallite	.5	.6	.25	.30	.05	5	5	2.0	2.2
CH ₂	.6	2.0	.075	.024	.07	10	5	2.4	.9
Pb	.4	2.4	.466	.0025	.02	10	2	.26	11.3

*These fits include additional parameters

Ref. 4

Ref. 1

Ref. 2

Ref. 3

short prints require only a few pages of printing, and hence are normally called for at more frequent intervals than the "long" prints.

Tracer points are positioned at the center of every other cell in SETJP, and the positions of these points are updated in PH2. The current position of each tracer point is printed in both the long and the short prints, providing the basis for a Lagrangian description of the flow. The positions are written on the restart dump tape and can be used by plo' routines to make a plot of material deformation.

2.8. MAP

This subroutine is called by EDIT and displays the properties of each cell in the active grid using an alphabetic scale. One obtains contour maps of the density, pressure, radial and axial velocities, and internal energy in the active grid.

2.9. PH1

The effect of the pressure gradient in updating the velocities and the internal energy is computed here. The calculation method is described in detail in Section 3.2 of PART TWO.

2.10. PH3

The deviator stresses acting on each cell edge and the hoop stress are determined in PH3 and the resulting velocity and energy increments are computed. Details are given in Section 5 of PART TWO. If CYCPH3 is -1, Phase 3 is bypassed and the effect of strength is not accounted for in the calculation. In this case the code is "hydrodynamic" in the classical sense.

2.11. PH2

Mass transport and the associated flux of momentum and energy are accounted for in PH2. The tracer points are also moved with velocities obtained by a simple weighting scheme.

2.12. REZONE

The masses of four cells are lumped into one in this subroutine. The JPM, DX, DY, X, Y, and TAU arrays are adjusted accordingly. Momentum and total energy are conserved, thereby converting some kinetic energy into

internal in a process loosely called "thermalizing." Every other tracer point is deleted in rezone, and new tracer points are placed in the added cells, retaining constant the total number of tracer points.

2.13. ERROR

This subroutine, which is called in the case of certain error conditions tested on by the code, prints a message identifying the error conditions, calls EDIT for a long print and tape dump, and then calls EXIT.

2.14. TAPE DUMPS

Each OIL-RPM tape dump consists of eight or nine records depending on whether tracer points are used. (See list below.) The first record contains three words: 555.0, the value of CYCLE at the time of the dump, and the value of N3 ($N3 = 1$ when tracer points are used; otherwise, $N3 = 0$). The last record also contains three words: 666.0, 666.0, 666.0. However, before each dump after cycle 0, TAPE 7 is backspaced one record and this last record is written over. Therefore, this last record remains only on the last dump of a run and in that case is followed by an end of file mark.

On cycle 0, after all input cards but the last have been read and the properties of all cells have been defined, SETUP does a tape dump. Thereafter, all tape dumps are made by EDIT at set intervals defined by NDUMP7. However, when $NODUMP \neq 0$, all tape dumps after cycle 0 are suppressed. This makes it possible to restart a problem from a dump tape without writing on the dump tape which is sometimes useful in special studies.

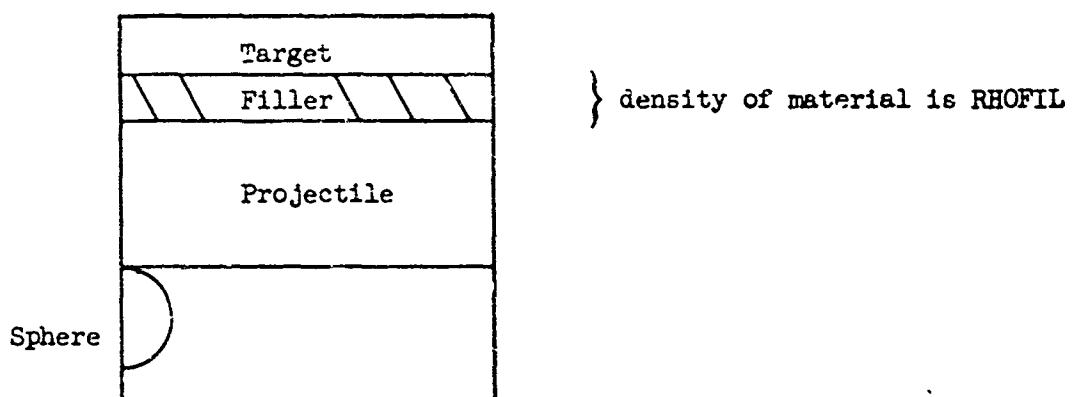
Record Number	Description
1	555.0, CYCLE, N3
2	Z(I), I = 1, MZT
3	U(I), V(I), AMX(I), AIX(I), P(I), I = 1, KMAX
4	X(0), (X(I), TAU(I), JPM(I), I = 1, IMAX)
5	Y(I), I = 0, JMAX
6	((XP(I,J), YP(I,J), I = 1, II), J = 1, JJ)
7	DX(I), I = 1, IMAX
8	DY(I), I = 1, JMAX
9	666.0, 666.0, 666.0

3. SET-UP OF PROBLEMS

Most calculations performed with the OIL-RPM code involve either a sphere or a cylinder hitting a target. Since the cylinder (which is called a "projectile" in the code) can be stationary, the set-up can also provide for a sphere hitting a two-layer target with or without filling material between the layers, as sketched in the diagram below.

The geometries described by the code are limited by the following requirements:

1. The Y-axis of the "sphere" must be on the Y-axis of the grid, i.e. the code cannot setup problems involving toroids.
2. The center of the sphere must coincide with a cell boundary. (Note: the center can be at the origin of the grid.)
3. The edge of the sphere should be contiguous with the projectile or target.
4. The projectile package is assumed to be below the target package.
5. The filler material can be placed only between the projectile package and the target package and extends out to the right boundary of the grid.
6. The right and top boundaries of the grid are transmittive, although the bottom boundary can be either reflective or transmittive.



The input cards for setting up an OIL-RPM problem define (1) the dimensions of the grid as well as the packages (sphere, projectile, and target); (2) the properties of the packages (density, velocity, and specific internal energy); (3) the physical constants used in the equation of state and yield-strength calculation; (4) the calculational constants used in defining various cutoffs and flags; (5) the frequency of printing and of writing on the restart tape; and (6) the time or cycle at which to stop execution.

Most of the input variables are equivalenced to an element in the Z-array, the first array in Blank Common. The variables, therefore, are identified on the input cards by their location in Blank Common (i.e., in the Z-array). The list that follows gives the variable name associated with each input number, its location in Blank Common, and a brief description of its function in the code.

Following this list will be a discussion of the format and order of the input cards, and the RPM Setup Sheets illustrating the input for a typical impact problem.

3.1. DEFINITION OF RPM INPUT VARIABLES

3.1.1. Identification

Variable Name	Location in Blank Common	Definition
PK(1)	151	The problem number can be any number with at most 2 places to the left and at most 4 to the right of the decimal point. (Range: 00.001 to 99.9999)
PROB	1	The problem number is repeated if this is a new problem just being set up. (It is <u>not</u> repeated for restarts from tape. See "RPM Input for Restart.")

3.1.2. Dimensions

Variable Name	Location in Blank Common	Definition
IMAX	33	The number of columns in the calculational mesh. IMAX \leq 50 for the standard version. Unless IMAX = 1 for 1-D problem, IMAX must be <u>even</u> in order to rezone the grid.
JMAX	35	The number of rows in the calculational mesh. In the standard version JMAX \leq 100, and IMAX times JMAX \leq 2500. JMAX must be <u>even</u> to rezone the grid.
I1	47	The right-most column to be calculated initially. It should be two columns beyond the last column with non-zero energy (kinetic or internal). (I1 \leq IMAX)
I2	48	The top row to be calculated initially. It should be two rows above the last column with non-zero energy. (I2 \leq JMAX) I1 and I2 define the "active grid." I1 and I2 are automatically adjusted as the problem runs.
DXF	136	The value of all the DX's if DX is constant.
DYF	137	The value of all the DY's if DY is constant.
X(I)	269	The number of cms. from the axis to the right side of column I. The X-array is included in the input deck only if the radial dimension of the cells varies.
Y(J)	166	The number of cms. from the bottom of the grid to the top of row J. The Y-array is included in the input deck only if the axial dimension of the cells varies.

3.1.3. Projectile

Variable Name	Location in Blank Common	Definition
PRYBOT	67	The number of cms. from the bottom of the grid to the bottom of the projectile.
PRYTOP	68	The number of cms. from the bottom of the grid to the top of the projectile.
PRXRT	69	The number of cms. from the axis to the right of the projectile.
VINI	112	Initial axial velocity of the projectile.
PROJU	73	Initial radial velocity of the projectile.
PROJI	16	Initial specific internal energy of the projectile.
RHINI	111	Initial density of the projectile.

3.1.4. Target

Variable Name	Location in Blank Common	Definition
TAYBOT	86	The number of cms. between the bottom of the grid and the bottom of the target.
TAYTOP	89	The number of cms. between the bottom of the grid and the top of the target.
TAXRT	107	The number of cms. between the axis and the right of the target.
TARGV	52	Initial axial velocity of the target.
TARGI	72	Initial specific internal energy of the target.
RHINIT	15	Initial density of the target.

3.1.5. Sphere

Variable Name	Location in Blank Common	Definition
RADIUS	162	The radius (in cms.) of the sphere.
YCENTR	163	The number of cms. from the bottom of the grid to the center of the sphere. (Note: The center of the sphere must be on a cell boundary and on the axis of the grid.)
VINSPH	102	Initial axial velocity of the sphere.
SIESPH	101	Initial specific internal energy of the sphere.
RHOSPH	100	Initial density of the sphere.
RHOOUT	103	Initial density of material in the outside part of a cell cut by the sphere boundary.

3.1.6. Filler

Variable Name	Location in Blank Common	Definition
RHOFIL	51	Initial density of material between projectile and target.

3.1.7. Physical Constants

Variable Name	Location in Blank Common	Definition
AMDM	21	The lowest compression of material considered "solid." If $\rho/\rho_0 \leq AMDM$, and material is cold (specific internal energy $< ES'$) stresses and pressure are zero.
CZERO(Y_0)	42	Parameters used in yield-strength equation:
STK1(Y_1)	11	$Y = (Y_0 + Y_1\mu + Y_2\mu^2) \cdot (1 - E/E_0)$ where $\mu = \rho/\rho_0 - 1$, and E = specific internal energy.
STK2(Y_2)	28	However, (1) If $Y < 0$, stresses are set to 0. (2) If $E > E_0$, then $Y = 0$.
STEZ(E_0)	29	

<u>Variable Name</u>	<u>Location in Blank</u>	<u>Location in Common</u>	<u>Definition</u>
BBAR	149		A constant used to approximate sound speed for the calculation of DT. $C = C_0 + \bar{B} \cdot \sqrt{P(K)}$, where $C_0 = \sqrt{A/\rho_0}$.
RHOZ	115		The normal density of the material. This value is used in the equation of state, the calculations of PMIN and C_o , the strength calculations, and the "slaving" process.
ESA(a)	116		Gruneisen ratio at high energy, ~ .5.
ESEZ(E_0)	117		A constant in Gruneisen ratio.
ESB(b)	118		A constant in Gruneisen ratio.
ESCAPA(A)	119		Bulk modulus.
ESESP(ES')	120		Heat to vaporize material; must be larger than ESES.
ESESQ(ESQ)	121		Used to test whether material is "cold;" usually identical to ESESP.
ESES(ES)	122		Heat to bring material to vapor temperature; must be smaller than ESESP.
ESALPH(α)	123		Usually 5.
ESBETA(β)	124		Usually 5.
ESCAPB(B)	125		Usually of the same order as A.

3.1.8. Calculational Constants

<u>Variable Name</u>	<u>Location in Blank</u>	<u>Location in Common</u>	<u>Definition</u>
RHOMIN	138		The smallest density a cell can have and still influence the calculation of DT. (Usually $RHOMIN = RHOZ * 10^{-3}$.)

<u>Variable Name</u>	<u>Location in Blank Common</u>	<u>Definition</u>
DMIN	24	The allowable relative error in the energy sum. The error is the difference of the current total energy of all the cells and the total energy computed on cycle zero but adjusted for energy "evaporated" and lost across boundaries. The relative error is the difference divided by the total energy. If it exceeds DMIN, ERROR is called and the calculation is terminated.
DTMIN	144	The minimum value of DT (after STAB = FINAL) for the calculation to continue. DTMIN may be zero.
EVAP	75	This variable controls the "evaporation" of mass. If $\rho < EVAP * RHINI$, the cell mass is evaporated. The mass, energy and momentum of evaporated cells are accumulated in PH2 and printed in EDIT. (Usually EVAP = 10^{-4} .)
ROEPS	110	The "round-off epsilon" used in setting to zero certain calculated differences which could be due simply to machine round-off. (Usually ROEPS = 10^{-5} or 10^{-6} .)
STAB	139	The stability fraction used in determining DT. The input value of STAB is its initial value. If FINAL > 0., STAB is doubled on each cycle until it equals FINAL. However, if FINAL = 0., the initial value of STAB is used throughout the run. STAB is usually $\leq 10^{-3}$, but when all the energy is initially internal, setting STAB $\sim 10^{-8}$ is recommended.

<u>Variable Name</u>	<u>Location in Blank Common</u>	<u>Definition</u>
FINAL	113	FINAL is used in determining DT. If FINAL is > 0., then it is the largest value the stability fraction (STAB) will have. If FINAL = 0., the stability fraction will have the same value for each cycle. (FINAL is usually ~ .4.)
JSTR	25	JSTR (J strength) gives the value of I2 (active grid, J direction) at which stress calculations (PH3) are turned on and tensions are allowed.
N6	56	N6 specifies the J index of the cell behind which tensions (negative pressures) are to be allowed. If N6 = 0., tensions are allowed everywhere.
CYCPH3	70	CYCPH3 = -1. if no stress calculation is wanted. Otherwise, it is the number of sub-cycles of PH3 per time step. (Usually about 4.)
NUMREZ	12	The maximum number of times the grid will be rezoned.
NMPMAX	85	The maximum number of tracer points to be used.
Y2	81	Y2 = -2. if tracer points are to be calculated. Y2 = 0. if no tracer points are to be calculated.
REZFCT	71	REZFCT = 1. if rezones are allowed. REZFCT = 0. if rezones are not allowed.
SS4	130	SS4 = 1. if a rezone is to be forced on the second cycle of a run. (Often used to test the setup of problems to be rezoned.)

<u>Variable Name</u>	<u>Location in Blank Common</u>	<u>Definition</u>
SN	65	SN = 0., if negative specific internal energy is to be set to zero. SN = 1., if negative specific internal energy is to be left along.
CVIS	27	CVIS = 0., if the bottom boundary of the grid is to be reflective. CVIS = -1., if the bottom boundary of the grid is to be transmittive.
INTER	87	INTER = 0., gives no intermediate prints. INTER = 1., gives EDIT prints after PH1 and PH3, as well as CDT. INTER = 7., gives, in addition to the extra EDIT prints, details of PH2 calculations. INTER = 99., gives, in addition to the extra EDIT prints, details of PH3 stress and strain rates. CAUTION: INTER = 7., or = 99., gives <u>many</u> pages of output.
IVARDX	83	IVARDX = 0., if DX is constant and the X array is to be calculated from the value of DXF. IVARDX = 1., if DX varies and the X array is included in the input deck.
IVARDY	54	IVARDY = 0., if DY is to be constant and the Y array is to be calculated from the value of DYF. IVARDY = 1., if DY varies and the Y array is included in the input deck.

3.1.9. Output

Variable Name	Location in Blank Common	Definition
JPROJ	147	JPROJ is usually assigned the value of J at the top of the projectile. In EDIT, JPROJ is used as the zero in calculating the crater depth and is the division for the printout of total energy, mass and momentum.
PRDELT	45	The number of seconds between EDIT prints when printing on time. Otherwise 0.
IPCYCL	49	The number of <u>cycles</u> between EDIT prints when printing on cycles. Otherwise 0.
PRLIM	44	PRLIM is the time <u>or</u> cycle at which the EDIT print interval is to be increased. PRLIM is multiplied by PRFACT each time the print interval is adjusted.
PRFACT	46	The factor by which the print interval is increased. PRDELT (or IPCYCL) and PRLIM are multiplied by PRFACT when T = PRLIM.
NUMSCA	43	NUMSCA is the number of times the code will increase the interval time (or number of cycles) between EDIT prints.
NFRELP	5	NFRELP indicates the frequency of "long" EDIT prints. (A "long" print gives the velocities, pressure, mass, energy, density, and compression of all cells in the active grid; the "short" print gives this information only for the cells in the first column of the active grid.) A "long" print will occur every NFRELP short prints.

<u>Variable Name</u>	<u>Location in Blank Common</u>	<u>Definition</u>
NDUMP7	6	NDUMP7 indicates the frequency of "tape dumps," where most of Blank Common is written on an output tape. A tape dump will occur every NDUMP7 EDIT prints. These "tape dumps" are used for restarting problems and for making automatic plots of tracer points.
NODUMP	96	NODUMP = 1. allows the user to pick up a run at some intermediate point on the restart tape without writing over the subsequent dumps on that tape.

3.1.10. Stopping

<u>Variable Name</u>	<u>Location in Blank Common</u>	<u>Definition</u>
ICSTOP	7	The cycle for execution to stop when stopping on cycles.
TSTOP	50	The value of T for execution to stop when stopping on time rather than cycles. NOTE: This card, because of its "1" in column one, must always be included in the initial input deck. If stopping on cycles set to zero.
Z(150)	150	Dummy end card. Used in the RPM input deck for <u>setting up</u> problems. (Do not include this card in an input deck when <u>restarting</u> a problem.)

3.2. FORMAT AND ORDER OF OIL-RPM INPUT CARDS

Except for the ID header card, all RPM input cards have the same format and are normally punched on 7-word data cards.

The RPM setup sheets provide the information to be punched in Col. 1, Cols. 2-6, and Col. 7 for each input variable. The values of the variables are punched in the seven 9-space fields in Cols. 8-70. These values must

be punched with a decimal point even when they define integer variables. If the E-format is used, the exponent must be right-adjusted in the field. Only those variables which occur in consecutive order in Blank Common can be punched on the same card.

Col. 1	Cols. 2-6	Col. 7	Cols. 8-16	Cols. 17-25 etc.
Punch "1" on first and last two cards of deck. (See Setup Sheet.) Punch "2" on all cards defining integer variables. Otherwise no punch.	N Location in Blank Common of variable defined in Cols. 8-16.	Number of variables being defined on this card.	Z(N) Value of variable equivalenced to Z(N).	Z(N+1) Value of variable equivalenced to Z(N+1).

For a normal setup deck, the only data cards which must be in a specific order are those listed on the Setup Sheet with a "1" in column one, and they must be the first and the last two cards in the deck.

3.3. OIL-RPM INPUT FOR "SPECIAL SETUPS"

The properties (density, velocity, internal energy) of each cell are defined by the subroutine SETUP according to the input parameters associated with the sphere, cylinder, filler and target (e.g., SIESPH, VINI, RHOFIL, TARGV). The RPM "special setup" allows the user to assign a special mass (not density), velocity or internal energy to specific cells in the grid.

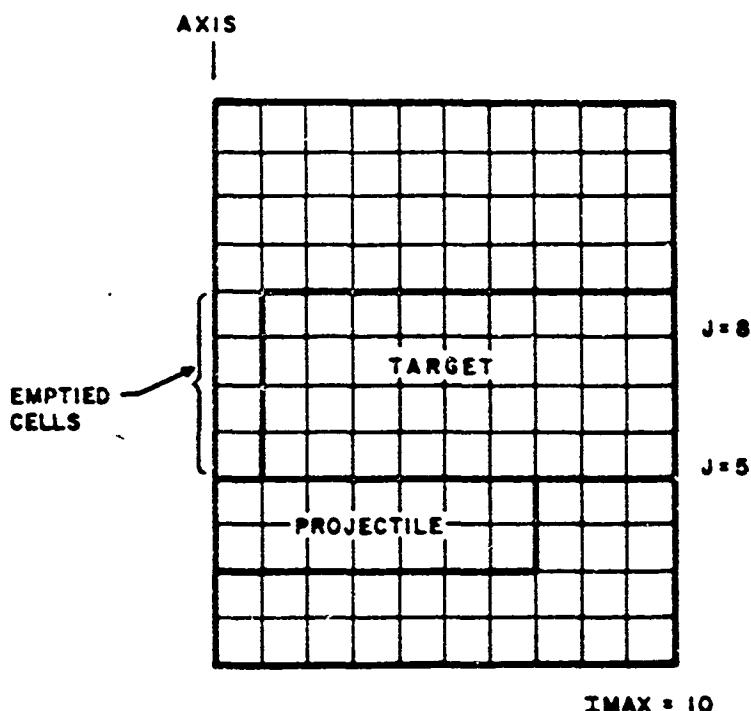
To assign special properties to a specific cell the user must do the following:

1. Find the I and J of the cell, then compute its K-index.
 $(K = (J - 1)* IMAX + I + 1).$
2. Find the location in Blank Common of AMX(K), U(K), V(K), and AIX(K), whichever is being specifically defined. (See Table 3, page 26, "Location of Arrays in Blank Common.")
3. Using the format of the other RPM input cards, punch a card with the location and value for each property being assigned.

Precede these input cards by a flag card which has a "1" in column one and which sets $Z(164) = PK(14) = 1$. (See Figure 2, page "Flow Diagrams of INPUT, CARDS and SETUP.") Place the special input cards in the

RPM input deck just before the card that defines ICSTOP(Z(7)). The flag card (PK(14) = 1.) must be the second card with a "1" in the column one in the input deck.

EXAMPLE: Suppose one column of cells in the target next to the axis is to be empty. The target is to range from J = 5 to J = 8, and IMAS = 10. (NOTE: This problem requires special input because RPM places all packages next to the axis of the grid.)



1. Compute the K-index of the empty cells.

$$I = 1, \quad J = 5, \quad K = 4*10 + 1 + 1 = 42$$

$$I = 1, \quad J = 6, \quad K = 52$$

$$I = 1, \quad J = 7, \quad K = 62$$

$$I = 1, \quad J = 8, \quad K = 72$$

2. Find the location in Blank Common of members of the AMX array which store the masses of these cells. Table 3 indicates that 482 is the location of AMX (1) in Blank Common.

Variable Name	Location in Blank Common
AMX(42)	523
AMX(52)	533
AMX(62)	543
AMX(72)	553

3. The input deck would be organized as follows:

Description of card	Col. 1	Col. 2-6	Col. 7	Col. 8-16
ID CARD				IMPACT
PK(1)	1	151	1	3.2
Z(1)=PROB	blank		1	3.2
.
.
.
NODUMP	2	96	1	0.
PK(14)	1	164	1	1.
AMX(42)	blank	523	1	0.
AMX(52)	blank	533	1	0.
AMX(62)	blank	543	1	0.
AMX(72)	blank	553	1	0.
ICSTOP	2	7	1	0.
TSTOP	1	50	1	1. - 06
Dummy End	1	150	1	0.

TABLE 3
LOCATION OF ARRAYS IN BLANK COMMON*

Name of Array	Location of First Member of Array
Z	1
PK	151
YY Note: YY(1) = Y(0)	166
XX Note: XX(1) = X(0)	270
DDX Note: DDX(1) = DX(0)	324
DDY Note: DDY(1) = DY(0)	378
AMX	482
AIX	2984
U	5486
V	7988
P	10490
TAU	12992
JPM	13044
UL	13096
PL	13300
XP	13504
YP	14830
CMXP	16156
CMYP	16161

* These location numbers should not be used if the dimension of any array in Blank Common is changed.

4. SAMPLE PROBLEM

The impact of an aluminum sphere on a target of like material was described in an earlier report,⁽⁸⁾ and the setup of the problem will be described in this section as an example. The sphere diameter was .4763 cms (3/16 in.), and its velocity was 7.35 km/sec. The zoning was chosen so that the sphere radius contained exactly 6 cells, the free surface of the target was 16 zones above the bottom of the grid, and the cells were square. It was found that after 16 microseconds the velocities were down to a value where the subsequent material motion would be negligible. The grid was rezoned twice during the computation. About two hours of computer time and about 450 cycles were required to complete the problem.

Details of the setup are given by the OIL-RPM Setup Sheets which list the appropriate values for the input parameters and describe the format of the data cards. Also, the main section of the printed output are illustrated and briefly discussed in addition to the control cards for the UNIVAC 1108.

7-WORD DATA
OIL-RPM SETUP SHEET

LOC	78	1	17	2	26	3	35	4	44	56	62	7	7173
N													
1	1.151	1.13.1.7351											
1	1.11.3.1.7351												
2	1.13.3	1.4.2.											
2	1.3.5	1.54.											
2	1.14.7	1.8.											
2	1.4.8	1.8.											
1	1.3.6	1.03.97.											
1	1.3.7	1.03.97.											

PK(1) = Problem number in the form 92.3456.
 PROB = Problem number (exactly the same as previous card).
 IMAX = Number of columns. An even number ≤ 50. unless IMAX = 1. { IMAX * JMAX ≤ 2500 unless variable dimensions are changed.
 JMAX = Number of rows. An even number ≤ 100.

I1 = Number of columns in "active" grid + 2. (If IMAX = 1., I1 = 1.)
 I2 = Number of rows in "active" grid + 2.
 DXF = DX if it is constant. If DX varies DXF = 0.
 DYF = DY if it is constant. If DY varies DYF = 0.

Insert X-array only if DX varies. (See Page 31) Insert Y-array only if DY varies. (See page 31)

1.6.7	1.-1.												
1.6.8	10.												
1.6.9	10.												
1.1.1.2	10.												
1.1.7.3	10.												
1.1.6.19.													
1.1.11.12.	0.7.												
1.8.8	1.6.35.2.												
1.8.9	14.0.9.1.1+1.0												
1.9.7	11.0.9.1.1+1.0												
1.5.2	19.												
1.7.2	19.												
1.1.5	12.0.7.												

7-WORD DATA
OIL-RPM SETUP SHEET

2 LOC	7 8	1	1 7	2	1 6	3	3 5	4	1 4	5 3	6 2	7	7 1 7 3
N	1.462	1.2.38.2.1.1.1.	RADIUS = radius (cm) of sphere. (RADIUS need <u>not</u> fall on cell boundary.)										
	1.163	1.3.9.7.1.1.1.	YCENTR = Y-center (cm) of sphere. (YCENTR must coincide with a cell boundary.)										
	1.102	1.7.1.3.5.1.1.1.1.1.	VINSPH = Initial velocity of sphere.										
	1.110.1	1.0.1.1.1.1.1.1.	SIESPH = Initial specific internal energy of sphere.										
	1.100.1	1.2.1.7.1.1.1.1.	RHOSPH = Initial density of sphere.										
	1.103	1.0.1.1.1.1.1.1.1.	RHOOUT = Initial density of material adjacent to sphere.										
	1.151.1	1.0.1.1.1.1.1.1.1.	RHOFIL = Initial density of filling material between projectile and target.										
	1.121	1.1.2.1.1.1.1.1.1.	AMDM = Allowable expansion of material considered "solid." (Usually between .9 & .99.)										
	1.142.1	1.2.1.2.3.9.1.1.1.1.1.1.	CZERO (Y ₀)										
	1.111.1	1.2.1.4.1.1.1.1.1.1.1.1.	STK1 (Y ₁)	Used in strength calculation									
	1.128.1	1.4.1.4.1.1.1.1.1.1.1.1.	STK2 (Y ₂)										
	1.129.1	1.7.1.9.1.1.1.1.1.1.1.1.	STEZ (E ₀)										
	1.144.9.1	1.1.5.1.1.1.1.1.1.1.1.1.	BRAR = Constant in "local sound speed" calculation. (C = C ₀ + BRAR * $\sqrt{P(K)}$)										
	1.141.5.1	1.2.1.7.1.1.1.1.1.1.1.1.	RHOZ = Normal density (ρ_0) for the equation of state.										
	1.116.5	1.5.1.1.1.1.1.1.1.1.1.1.		a, E ₀ , b, A, ES'	Equation of								
	1.121.5	1.3.1.0.1.1.1.1.1.1.1.1.		State Con-									
	1.138.1	1.1.0.1.1.1.1.1.1.1.1.1.		stants. Nor-									
	1.124.1	1.1.0.1.1.1.1.1.1.1.1.1.		mally ES=ESQ.									
	1.144.1	1.1.0.1.1.1.1.1.1.1.1.1.	RHOMIN = Minimum density for influencing DT. Usually $10^{-3} * RHOZ$.										
	1.175.1	1.1.0.1.1.1.1.1.1.1.1.1.	DMIN = Allowable relative error for total energy sum. Usually 10^{-3} .										
	1.110.1	1.1.0.1.1.1.1.1.1.1.1.1.	DTMIN = Minimum value of DT for program to continue execution. DTMN may be 0.										
	1.139.1	1.1.0.1.1.1.1.1.1.1.1.1.	EVAP = Minimum allowable compression. If $\rho/\rho_0 < EVAP$, mass of cell is "evaporated."										
	1.143.1	1.1.4.1.1.1.1.1.1.1.1.1.	ROEPS = Round-off epsilon. Usually 10^{-5} or 10^{-6} .										
			STAB = <u>Initial</u> value of "stability fraction." Usually $< 10^{-3}$.										
			FINAL = <u>Final</u> value of "stability fraction." Usually = .4.										

7-WOKU DATA
OIL-RPM SETUP SHEET

LOC	7	8	1	7	2	26	3	35	4	44	55	62	7	71	73
2	1	2	5	1	2	8	.	1	1	1	1	1	1	1	1
2	1	1	5	6	1	1	1	1	1	1	1	1	1	1	1
2	1	1	7	0	1	4	1	1	1	1	1	1	1	1	1
2	1	1	1	2	1	2	1	2	1	2	1	2	1	2	1
2	1	1	8	5	1	5	6	7	1	2	5	6	7	1	2
2	1	1	8	1	1	-2	3	1	1	1	1	1	1	1	1
2	1	1	7	1	1	1	1	1	1	1	1	1	1	1	1
2	1	1	1	3	0	1	0	1	0	1	0	1	0	1	0
2	1	1	6	2	1	1	1	1	1	1	1	1	1	1	1
2	1	1	2	7	1	-1	1	-1	1	-1	1	-1	1	-1	1
2	1	1	8	7	1	2	9	1	1	1	1	1	1	1	1
2	1	1	8	3	1	9	1	1	1	1	1	1	1	1	1
2	1	1	2	5	4	1	0	1	1	1	1	1	1	1	1
2	1	1	2	1	4	7	1	6	1	6	1	6	1	6	1
2	1	1	1	4	5	1	2	0	1	1	1	1	1	1	1
2	1	1	2	1	4	9	1	0	1	0	1	0	1	0	1
2	1	1	1	4	4	1	1	1	1	1	1	1	1	1	1
2	1	1	4	6	1	2	0	1	1	1	1	1	1	1	1
2	1	1	2	1	4	3	1	1	0	1	1	1	1	1	1
2	1	1	2	1	5	1	5	1	1	1	1	1	1	1	1
2	1	1	2	1	6	1	1	1	1	1	1	1	1	1	1
2	1	1	2	3	1	9	1	9	1	9	1	9	1	9	1
2	1	1	2	7	1	0	1	0	1	0	1	0	1	0	1
1	1	1	1	5	0	1	1	0	1	1	0	1	0	1	0
1	1	1	1	5	0	1	0	1	0	1	0	1	0	1	0

- JSTR = Value of I2 which triggers calculation of strength and negative pressures.
- N6 = Value of J below which negative pressures are not allowed.
- CYCPH3 = Number of times of subcycle PH3. CYCPH3 = -1., for no PH3.
- NUMREZ = Maximum number of rezones allowed.
- NMPMAX = Maximum number of tracer points desired. NMPMAX ≤ 1250.
- Y2 = -2., if tracer points are wanted. Y2 = 0. for no tracer points.
- REZFCT = 1. for allowing rezones. REZFCT = 0. for no rezones.
- SS4 = 1. for forcing rezone on second cycle of run. Usually SS4 = 0.
- SN = 1. leave negative S.I.E. alone. SN = 0. sets negative S.I.E. to 0.
- CVIS = -1. for transmittive bottom boundary. CVIS = 0. for reflective bottom boundary.
- INTER = Intermediate print flag.
- IVARDX = 1. if DX varies and the X-array is read in. IVARDX = 0. if DX is constant.
- IVARDY = 1. if DY varies and the Y-array is read in. IVARDY = 0. if DY is constant.
- JPROJ = Usually the J-value of top row of projectile. Used in EDIT print, crater depth calculation.
- PRDELT = Time between EDIT prints. PRDELT = 0. if printing on cycles.
- IPCYCL = Cycles between EDIT prints. IPCYCL = 0. if printing on time.
- PRLIM = Time or cycle at which to increase interval between prints.
- PFACT = Factor by which to increase print interval.
- NUMSCA = Maximum number of times print interval can be increased.
- NFRELIP = Ratio of "short" prints to "long" prints.
- NDUMPT = Ratio of prints to tape dumps.
- NODUMP = 0. allows tape dumps. NODUMP = 1. suppresses tape dumps after cycle 0.
- ICSTOP = Cycle to stop execution. ICSTOP = 0. if stopping on time.
- TSTOP = Time (value of T) to stop execution. TSTOP = 0. if stopping on cycles.
- Dummy end card.

7-WORD DATA
OIL-RPM SETUP SHEET--X AND Y ARRAYS*

² LOC	78	1	17	2	26	3	35	4	44	5	6	62	7	71	73
1	270	7													
1	271	7													
1	284	7													
1	291	7													
1	298	7													
1	305	7													
1	312	7													
1	319	2													
1	167	7													
1	173	7													
1	180	7													
1	187	7													
1	194	7													
1	201	7													
1	208	7													
1	215	7													
1	222	7													
1	229	7													
1	236	7													
1	243	7													
1	250	7													
1	257	7													
1	264	3													

X(0), ..., X(50)
Input these
values only if
DX varies.

Y(0), ..., Y(100)
Input these
values only if
DY varies.

*These location numbers (cols. 2-6) must be changed if the dimension of Z, PK, or YY is changed.

4.1. OIL-RPM Output

The pages of OIL-RPM output which follow were produced by the sample problem, "Standard Crater," described above. The printed headings make most of the listing self-explanatory. Sections needing further description are numbered in the listing and discussed below.

1. The first few pages of the output for a setup run* display the input deck and describe the initial conditions of the problem. (Each time the CARDS routine is called "INPUT CARDS" is printed.)
2. When a sphere is placed, SETUP assures that the value of YCENTR is on a cell boundary and prints the input and adjusted values of YCENTR.
3. On every cycle subroutine CDT prints the value of T, the time, and DT, the time step. The integers following "CDT" in the printout are the I and J of the cell controlling the time step. MAXCUV represents the maximum sound speed or velocity in the active grid. Likewise, MAXUV represents the maximum velocity. UMIN and PMIN are velocity and pressure cutoffs, respectively, used in MAP and PH2.
4. The first page printed by EDIT gives the total energies, mass and momenta of the cells above the JPROJ row and of the cells below and in the JPROJ row. (JPROJ is an input parameter, usually the J of the top row of the projectile package.)
5. On each cycle EDIT calculates the relative error in the total energy sum. On print cycles EDIT prints the maximum error calculated and the number of the cycle in which the maximum error occurred.
6. The total work done due to stresses calculated in PH3 is printed under "PLASTIC-WORK."
7. Also printed is a running total of the mass, energy, and axial and radial momentum lost when material crosses a transmittive boundary or is "evaporated" in PH2.

*For a restart run only the input deck is printed.

8. The "J OF PRESSURE MAXIMUM" describes the shock front by giving the location of the peak pressure in each column.
9. The tracer point coordinates are printed in centimeter units. The I and J of the cell in which a tracer point originated is also printed. This enables the user to follow the movement of a given tracer point. However, if the mass of a cell is "evaporated" the coordinates of the tracer points in that cell are set to zero and thereafter are not printed out.
10. The range of values assigned to the symbols on the contour maps are adjusted as the calculation proceeds. Therefore, a given symbol in the compression map, for instance, does not represent the same compression from one print to the next. A negative pressure, velocity, or internal energy is denoted by a symbol representing its absolute value and preceded by a minus sign.
11. The crater depth is measured from JPROJ. After a crater is formed, the negative values for the crater depth will describe the crater's "lip". The volume of the crater is printed along with the volume of a hemisphere of radius equal to the crater's depth in column one.
12. The J-index, radial velocity, axial velocity, pressure, mass, density, specific internal energy, compression, and distance (in cms.) from the bottom of the grid are printed for non-empty cells. The "long" EDIT print lists these properties for every column of the active grid, whereas the "short" EDIT print describes the non-empty cells in column one only.
13. Several error conditions are tested for during execution, and when one is detected, subroutine ERROR is called. ERROR in turn identifies the error test, prints the entire Z-array, and calls EDIT to do a long print and tape dump before stopping.

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-2 113 4 4.000000-01
-2 25 1 2.000000+01
-2 56 4 1.000000+01
-2 70 4 4.000000+00
-2 65 1 6.000000+00
-2 65 1 5.070000+02
-2 61 1 -2.000000+00
-2 71 1 1.000000+00
-2 130 4 1.000000
-2 65 4 1.000000+00
-2 27 4 -1.000000+00
-2 67 1 1.000000
-2 63 1 1.000000
-2 54 4 1.000000
-2 147 4 1.000000+01
-2 45 4 1.000000-06
-2 45 4 1.000000-06
-2 40 4 1.000000-06
-2 40 4 2.000000+00
-2 42 1 1.000000+01
-2 2 4 2.000000+00
-2 0 1 1.000000+00
-2 90 4 1.000000
-2 7 4 1.000000
-2 50 4 1.000000-06

```

(2) INPUT YCE,TR = 3.970000-01 ADJUSTED YCENTR = 3.970000-01

INITIAL CONDITIONS

SPHERE	PACKAGE 1	PACKAGE 2	FILLER
DENSITY	2.7000+00	2.7000+00	0.0000
S.I.E.	0.0000	0.0000	0.0000
V	7.3333+00	0.0000	0.0000
U	0.0000	0.0000	0.0000
KADIUS	2.3020-01	1.0000+10	1.0000+10
YCENTER	3.9700-01	0.0100-1.0000+00	0.0000+10
	RIGHT 0.0000		

INPUT CARUS

```

1 150 1 0.000000
IPCYCLE= 0 ISTOP= 0 JSTRE= 28 N6= 10 IMAX= 42 JMAX= 54 I1= 8 I2= 18 JEROJ= 16 NMPIMAX= 567 INTRE= 0 NUMSCA=10
NFREL= 5 NDUMP= 1 NODUMP= 0 IVAROX= 0 IVARY= 0

```

(3)

cut 17 12 $t = 2.73304042-07$ $ut = 1.7105428-08$ MAXCUV = 9.2836024+05 $\lambda_{XUV} = 9.2836024+05$ $u_{MIN} = 9.2836023-01$ $p_{MIN} = 1.3228399+06$
 cut 17 11 $t = 2.9040684-07$ $ut = 1.71d0432-08$ MAXCUV = 9.2430734+05 $\lambda_{XUV} = 9.2430734+05$ $u_{MIN} = 9.2430732-01$ $p_{MIN} = 1.17069+06$
 cut 17 11 $t = 2.0.0758227-07$ $ut = 1.79e0208-08$ MAXCUV = 8.d4176A3+05 $\lambda_{XUV} = 8.4417683-05$ $u_{MIN} = 8.4417681-01$ $p_{MIN} = 1.2598892+06$
 cut 10 12 $t = 2.0.2554047-07$ $ut = 1.7412566-08$ MAXCUV = 9.1198503+05 $\lambda_{XUV} = 9.1198503+05$ $u_{MIN} = 9.1198502-01$ $p_{MIN} = 1.2995066+06$
 cut 10 12 $t = 2.0.4296205-07$ $ut = 1.62d2935-08$ MAXCUV = 8.72308675+05 $\lambda_{XUV} = 8.72308675+05$ $u_{MIN} = 8.72308675-01$ $p_{MIN} = 1.243021+06$
 cut 10 11 $t = 2.0.6116-96-07$ $ut = 1.8313324-08$ MAXCUV = 8.0712820+05 $\lambda_{XUV} = 8.0712820+05$ $u_{MIN} = 8.0712819-01$ $p_{MIN} = 1.2355822+06$
 cut 10 11 $t = 2.0.7447629-07$ $ut = 1.9107477-08$ MAXCUV = 8.3108d22+05 $\lambda_{XUV} = 8.3108d22+05$ $u_{MIN} = 8.3108a22-01$ $p_{MIN} = 1.1842350+06$
 cut 10 26 $t = 2.0.4805076-07$ $ut = 1.95d6046-08$ MAXCUV = 8.132d770+05 $\lambda_{XUV} = 8.966046-05$ $u_{MIN} = 8.132d768-01$ $p_{MIN} = 1.158137+06$
 cut 9 27 $t = 2.0.101141-07$ $ut = 1.9712737-08$ MAXCUV = 8.0557049+05 $\lambda_{XUV} = 7.6116d04+05$ $u_{MIN} = 8.0557048-01$ $p_{MIN} = 1.1478743+06$
 cut 10 27 $t = 2.0.37d2514-07$ $ut = 1.9654013-08$ MAXCUV = 8.0630364+05 $\lambda_{XUV} = 7.252011+05$ $u_{MIN} = 8.0630363-01$ $p_{MIN} = 1.1499169+06$
 cut 9 28 $t = 2.0.3751195-07$ $ut = 1.9867581-08$ MAXCUV = 8.0009749+05 $\lambda_{XUV} = 7.1909469+05$ $u_{MIN} = 8.0009748-01$ $p_{MIN} = 1.1400757+06$
 cut 11 27 $t = 2.0.17d6752-07$ $ut = 1.99d6495-08$ MAXCUV = 7.9772964+05 $\lambda_{XUV} = 6.9658096+05$ $u_{MIN} = 7.9772903-01$ $p_{MIN} = 1.1367017+06$
 cut 10 28 $t = 2.0.6727402-07$ $ut = 1.9937062-08$ MAXCUV = 7.96d0253+05 $\lambda_{XUV} = 6.7095737+05$ $u_{MIN} = 7.05d0252-01$ $p_{MIN} = 1.1349247+06$
 cut 11 29 $t = 2.0.12167-07$ $ut = 2.0.0005277-08$ MAXCUV = 7.9050396+05 $\lambda_{XUV} = 6.5599599+05$ $u_{MIN} = 7.0050095-01$ $p_{MIN} = 1.126401+06$
 cut 10 29 $t = 2.0.3730020-07$ $ut = 2.0.0092037-08$ MAXCUV = 7.90362d6+05 $\lambda_{XUV} = 6.6331750+05$ $u_{MIN} = 7.0036284-01$ $p_{MIN} = 1.1262066+06$
 cut 11 29 $t = 2.0.5739225-07$ $ut = 2.0.0253253-08$ MAXCUV = 7.d407156+05 $\lambda_{XUV} = 6.588937+05$ $u_{MIN} = 7.0407155-01$ $p_{MIN} = 1.117240+06$
 cut 11 29 $t = 2.0.77d4597-07$ $ut = 2.0.024493-08$ MAXCUV = 7.d4391A5+05 $\lambda_{XUV} = 6.5202171+05$ $u_{MIN} = 7.04391084-01$ $p_{MIN} = 1.117696+06$
 cut 10 30 $t = 2.0.9789040-07$ $ut = 2.0.03d1241-08$ MAXCUV = 7.d029636+05 $\lambda_{XUV} = 6.4354d66+05$ $u_{MIN} = 7.029636-01$ $p_{MIN} = 1.1118606+06$
 cut 12 29 $t = 2.0.1d2469-07$ $ut = 2.0.03d2880-08$ MAXCUV = 7.7910425+05 $\lambda_{XUV} = 6.3772d11+05$ $u_{MIN} = 7.7910423-01$ $p_{MIN} = 1.1101619+06$
 cut 10 31 $t = 2.0.5862407-07$ $ut = 2.0.0512106-08$ MAXCUV = 7.7417693+05 $\lambda_{XUV} = 6.3620342+05$ $u_{MIN} = 7.7417693-01$ $p_{MIN} = 1.1031469+06$
 cut 12 30 $t = 2.0.5913017-07$ $ut = 2.0.0516787-08$ MAXCUV = 7.74d0029+05 $\lambda_{XUV} = 6.3356140+05$ $u_{MIN} = 7.74d0029-01$ $p_{MIN} = 1.102d03+06$
 cut 11 31 $t = 2.0.7905495-07$ $ut = 2.0.065496-08$ MAXCUV = 7.b95d8d7+05 $\lambda_{XUV} = 6.2956331+05$ $u_{MIN} = 7.6954986-01$ $p_{MIN} = 1.0965463+06$
 cut 13 30 $t = 2.0.9999999-07$ $ut = 2.0.0698d30-08$ MAXCUV = 7.0721163+05 $\lambda_{XUV} = 6.2401286+05$ $u_{MIN} = 7.6721162-01$ $p_{MIN} = 1.0932159+06$

PROBLT-1		11AE 9 99999,9-07	CYCLE 70	101. EN-THEUR. 3.937223+10	MAX. REL. ERROR-CYCLE -R.35139U8-06	IE SET TO ZERO-phi1 0.0000000	IE SET TO ZERO-phi2 -5.6A78873+07	PLASTIC-WORK 3.0655210+08
4	J.61-JPKOJ	4.41045,57+10	AE	AE	TUT.EN. (SUM)	WASS	WV	WV (POSITIVE)
	J.LC-JPKOJ	4.400U780+09		2.186E779+10	3.5606988+01	1.2888103+05	2.0767698+05	2.0768153+04
				2.024U066+09	3.428052+09	1.2117721+01	-1.5975029+04	1.2621583+04
	TOTALS	1.000U150+10		2.3880766+10	3.9971941+10	3.5728759+01	1.1290600+05	2.2027423+05
BOUNDARY		BOTTO	RIGHT	TOP			SEVAPORATEDS	
MAS	UUT	0.UUUUUUUU	0.0000000	0.0000000			0.0971166-04	
ELEMG	UUT	0.UUUUUUUU	0.0000000	0.0000000			0.3158280+09	
MU	UUT	0.UUUUUUUU	0.0000000	0.0000000			5.3078244+02	
MV	UUT	0.UUUUUUUU	0.0000000	0.0000000			-5.6164385+02	
WORK	UUT	0.UUUUUUUU	0.0000000	0.0000000				

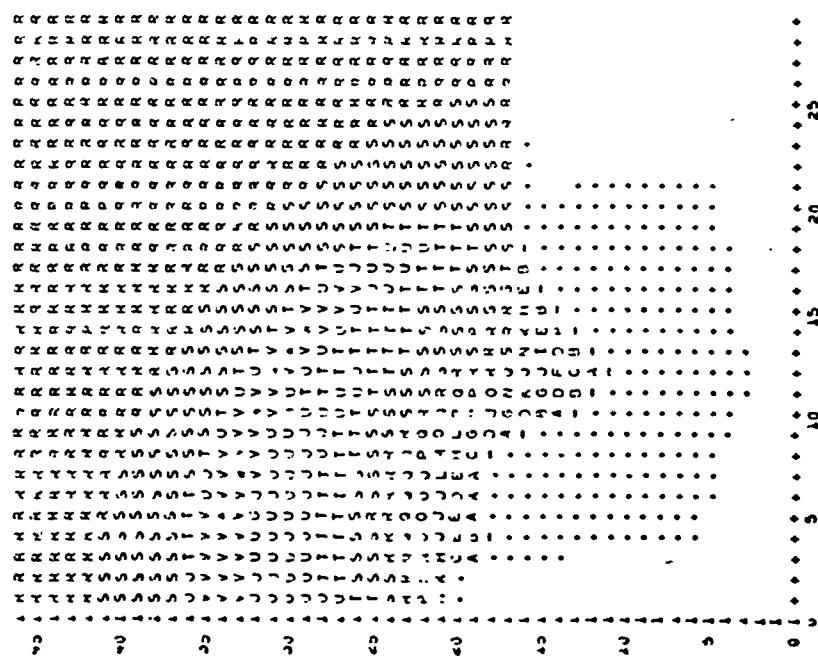
OF MEASUREMENTS

תְּמִימָה תְּמִימָה עֲלֵיכֶם גַּדְרֶת 70

7

q. CURRENT LOCATION IN C₀ = COORDINATES (X,Y) - CURRENT LOCATION IN C₀₀

CU TRUNG



19

*** ERROR EXIT - SEE STATEMENT NUMBER 65 IN CDT

(13)

I= 8 J= 10 K=705

L=LUCK

I	REAL FORMAT Z(I)	INTEGER FORMAT Z(I)
1	.137350+02	17831957620
2	-.100000+01	-17381195770
3	.000000	0
4	.000000	0
5	.500000-38	5
6	.500000-38	1
7	.000000	0
8	.314159+01	17553718990
9	.000000	0
10	.000000	0
11	.240000+11	21971239664
12	.500000-38	2
13	.000000	0
14	.000000	0
15	.270000+01	17536901600
16	.000000	0
17	.000000	0
18	.166740+01	17425984211
19	.500000-38	1
20	.500000-38	2
21	.970000-00	17310060380
22	.000000	0
23	.000000	0
24	.100000-02	16040629108
25	.500000-38	28
26	.000000	0
27	-.100000+01	-17381195770
28	.410000+11	22091785517
29	.700000+10	21718429208
30	-.500000-38	-1
31	.000000	0
32	.000000	0
33	.500000-38	42
34	.500000-38	43
35	.600000-38	54
36	.600000-38	55
37	.540000-38	2269
38	.540000-38	2270
39	.000000	0
40	.000000	0
41	.000000	0
42	.239000+10	21549523980
43	.500000-38	10
44	.100000-05	14700101090

4.2. UNIVAC 1108 CONTROL CARDS

▽ ASG P = 1184

Program Tape

▽ ASG 7 = 2213

Restart Tape*

▽ XQT CUR

IN

TRI P

TOC

▽ VP HDG

STANDARD CRATER

▽ XQT RPM

STANDARD CRATER

1	151	1	13.735	
.	.	.	.	
.	65	1	1.0	
.	.	.	.	
.	50	1	1.0	-06

} Input deck

* Can assign a drum area for tape dumps instead of a tape by using:
▽D ASG 7 = 100000

5. RESTART OF PROBLEMS

Periodically during a calculation EDIT writes on tape the problem parameters and the current state of the material in each cell. By reading this tape the user can "restart" and continue a calculation from an intermediate point. Because the initial conditions are saved on tape, SETUP is not called and the following three cards are the only ones which must be in the restart input deck:

Description of Card	Col. 1	Col. 2-6	Col. 7	Col. 8-16	Col. 17-25	Col. 26-34
ID CARD				IMPACT		
PK(1),PK(2), PK(3)	1	151	3	3.2	88.	-1.
TSTOP	1	50	1	1. - 06		

PK(1) = The same problem number used when the problem was initially setup. (NOTE: This can be any number between 00.0000 and 99.9999.)

PK(2) = The restart cycle number. The problem can be restarted on any cycle which is marked as a tape dump cycle in the printed output.

PK(3) = The restart flag. If it is -1. EDIT makes a long print of the restart cycle. However the user may wish to avoid making a long print on the restart cycle. He can do this by setting PK(3) = -2.

TSTOP = The new time at which execution will stop.

Other variables besides TSTOP may be redefined when restarting a problem. The copy of the "Setup Sheet for OIL-RPM Restarts" on page 44 lists those variables most likely to be redefined at an intermediate point in the calculation.

The cards in a restart input deck can be in any order as long as the first card is the ID card, the second card defines PK(1), PK(2) and PK(3) and has a "1" in column one, and the last card has a "1" in column one.

Examples:

1.

Description of Card	Col. 1	Col. 2-6*	Col. 7	Col. 8-16	Col. 17-25	Col. 26-34
ID CARD				IMPACT 1		
PK(1),PK(2) PK(3)	1	151	3	26.1	32.	-1.
INTER	2	87	1	0.		
RHOMIN		138	1	1. -03		
ICSTOP	2	7	1	135.		
TSTOP	1	50	1	0.		

2.

Description of Card	Col. 1	Col. 2-6*	Col. 7	Col. 8-16	Col. 17-25	Col. 26-34
ID CARD				IMPACT 2		
PK(1),PK(2) PK(3)	1	151	3	35.013	2019.	-2.
TSTOP	1	50	1	1.0 -05		

3.

Description of Card	Col. 1	Col. 2-6*	Col. 7	Col. 8-16	Col. 17-25	Col. 26-34
ID CARD				IMPACT 3		
PK(1),PK(2) PK(3)	1	151	3	8.2	128.	-2.
ICSTOP	2	7	1	200.		
TSTOP	1	50	1	0.		

*All numbers must be right-adjusted within col. field.

**7-WORD DATA
SETUP SHEET FOR OIL-RPM "RESTART"**

2 LOC	7 8	1	17	2	26	3	35	4	44	5	6	62	7	71	73
2	LOC	N													
1	1.15	1.3													
1	1.70	1													
1	2.1														
1	2.8	1													
1	3.1														
1	24	1													
1	44	1													
1	55	1													
1	65	1													
1	7.9	1													
2	1.14	1													
2	1.14	1													
2	1.15	1													
2	1.16	1													
2	1.17	1													
1	1.50	1													

(a) Problem number. (b) Pickup cycle #. (c) Restart flag (-1. or -2.)

CYCPH3 = Number of times to subcycle PH3.

AMDM = Allowable expansion of material considered "solid": ~.95 to .99.

RHOMIN = Minimum ρ for influencing DT.

FINAL = Final value of "stability fraction."

DMIN = Allowable relative error for total energy sum: $\sim 10^{-4}$.

DTMIN = Minimum for DT.

VT = Minimum Δp from one cell across a grid boundary to trigger rezone.

SN = 0., when negative S.I.E. is to be set to 0. If SN = 1., negative S.I.E. left alone.
 EVAP = ρ/ρ_0 of cells to be "evaporated."
 ROEPS = Round-off epsilon.

JPROJ = Used in EDIT print and crater depth calculation.

NFRELIP = Ratio of "short" print frequency to "long" print frequency.
 NDUMPT = Ratio of print frequency to tape dump frequency.
 ICSTOPF = Cycle to stop. Set to 0, if stopping on time.

TSTOPP = Time (value of T) to stop. Set to 0, if stopping on cycles. (This must be the last card of a restart deck.)

6. LISTING OF THE FORTRAN IV PROGRAM

This section consists simply of a listing of the FORTRAN IV program.

```

C RPM 10
C C 20
C C 30
C C 40
C C
C C DIMENSION AMX(2502),AIX(2502),U(2502) ,V(2502) ,P(2502) ,
1 X(52) ,XX(54) ,TAU(52) ,JPM(52) , 50
2 Y(102) ,YY(104) ,FLEFT(102),YAMC(102),SIGC(102), 60
3 GAMC(102), 70
4 PK(15), Z(150) , 80
5 XP(26,51),YP(26,51), 90
6 PL(204) ,UL(204) ,PR(204) , 100
7 RSN(52), RST(52), 110
8 CMXP(5) ,CMYP(5) ,IJ(5) ,JK(5) , 120
9 DX(52) ,DDX(54) ,DY(102) ,DDY(104) , 130
S SNB(52) ,STB(52) ,UK(52,3) ,VK(52,3) ,RHO(52,3) 140
150
C *** DIMENSIONED ARRAYS 160
C *** Z-BLOCK IS SAVED ON TAPE. 170
C COMMON Z 180
C COMMON PK 190
C COMMON YY, XX 200
C COMMON DDX, DDY 210
C COMMON AMX, AIX, U, V, P 220
C COMMON TAU, JPM 230
C COMMON UL, PL 240
C COMMON XP, YP, CMXP, CMYP 250
C *** NON-DIMENSIONED VARIABLES 260
C COMMON AID, AMMV, AMMY, AMPY, AMUR, AMUT, AMVR, 270
1AMVT, DEL:L, DELER, DELET, DELM, DTODX, DXYMIN, EAMMP, EAMPY, 280
2E, ERDUMP, I, I3, IWS, J, K, KA, KB, 290
3LL, MD, ME, MZT, NERR, NK, NPRINT, 300
4NR, NRZ, NULLE, PIOTS, SIEM(N,SNR, SNT, STR, SOLID, 310
5SUM, TESTRH, TWOP, URR, WS, WSA, WSB, WSC, WFLAGF, 320
6WFLAGL, WFLAGP, 330
COMMON LAST 335
C *** THE FOLLOWING EQUIVALENCES MAKE AVAILABLE 340
C X(0), Y(0), DX(0), DY(0) 350
C C
C C EQUIVALENCE (XX(2), X(1)), (YY(2), Y(1)) 380
C C EQUIVALENCE (DDX(2), DX(1)), (DDY(2), DY(1)) 390
C C *** SPECIAL EQUIVALENCES FOR PH2 ONLY 400
C C
C C EQUIVALENCE (UL,FLEFT), (UL(103),YAMC), 430
1 (PL,GAMC,PR), (PL(103),SIGC) 440
C C *** SPECIAL EQUIVALENCES FOR PH3 ONLY 450
C C
C C EQUIVALENCE (UL,RSN), (UL(103),YAMC), 480
1 (PL,RST), (PL(103),SIGC) 490
2 (P(157),VK), (P(313),SNB), 500
3 (P(365),STB), (P(417),RHO) 510
C C *** SPECIAL EQUIVALENCES FOR EDIT 520
C C
C C EQUIVALENCE (PR(1), IJ), (PR(6), JK) 530
C C *** Z-STORAGE EQUIVALENCES 540
C C
C C

```

C	EQUIVALENCE	(Z(1),PROB),(Z(2),CYCLE),	580
1(Z(3),DY),(Z(4),NUMSP),(Z(5),NFRELP),(Z(6),NDUMP7),		590	
2(Z(7),ICSTOP),(Z(8),PIDY),(Z(9),TOPMU),(Z(10),RTMU),		600	
3(Z(11),STK1),(Z(12),NUMREZ),(Z(13),ETH),(Z(14),UN14),		610	
4(Z(15),RHINIT),(Z(16),PROJI),(Z(17),UN17),(Z(18),XMAX),		620	
5(Z(19),NZ),(Z(20),NREZ),(Z(21),AMDM),(Z(22),UVMAX),		630	
6(Z(23),UN23),(Z(24),DMIN),(Z(25),JSTR),(Z(26),DTNA),		640	
7(Z(27),CVIS),(Z(28),STK2),(Z(29),STEZ),(Z(30),NC),		650	
8(Z(31),UN31),(Z(32),NRC),(Z(33),IMAX),(Z(34),IMAXA),		660	
9(Z(35),JMAX),(Z(36),JMAXA),(Z(37),KMAX),(Z(38),KMAXA)		670	
EQUIVALENCE			680
1(Z(39),BOTM),(Z(40),BOTMV),(Z(41),NUMSPT),(Z(42),CZERO),		690	
2(Z(43),NUMSCA),(Z(44),PRLIM),(Z(45),PRDELT),(Z(46),PRFACT)		700	
EQUIVALENCE			710
1(Z(47),I1),(Z(48),I2),(Z(49),IPCYCL),(Z(50),TSTOP),		720	
2(Z(51),RHOFIL),(Z(52),TARGV),(Z(53),N3),(Z(54),IVARDY),		730	
3(Z(55),VT),(Z(56),N6),(Z(57),RTM),(Z(58),RTMV),		740	
4(Z(59),UN59),(Z(60),N10),(Z(61),N11),(Z(62),GAMMA),		750	
5(Z(63),TOPM),(Z(64),BOTMU),(Z(65),SN),(Z(66),TOPMV),		760	
6(Z(67),PRYBOT),(Z(68),PRYTOP),(Z(69),PRXRT),(Z(70),CYCPH3),		770	
7(Z(71),REZFCT),(Z(72),TARGI),(Z(73),PROJU),(Z(74),BBOUND),		780	
8(Z(75),EVAP),(Z(76),ECK),(Z(77),NECYCL),(Z(78),II),		790	
9(Z(79),JJ),(Z(80),NMP),(Z(81),Y2),(Z(82),EZPH1)		800	
EQUIVALENCE			810
1(Z(83),IVAROX),(Z(84),T),(Z(85),NMPMAX),(Z(86),PMIN),		820	
2(Z(87),INTER),(Z(88),TAYBOT),(Z(89),TAYTOP),(Z(90),IEMAP),		830	
3(Z(91),MC),(Z(92),MR),(Z(93),MZ),(Z(94),MB)		840	
EQUIVALENCE			850
1(Z(95),REZ),(Z(96),NODUMP),(Z(97),UN97),(Z(98),UN98),		860	
2(Z(99),UN99),(Z(100),EVAPM),(Z(101),EVAPEN),(Z(102),EVAPMU),		870	
3(Z(103),EVAPMV),(Z(104),EZPH2),(Z(105),SNL),(Z(106),STL),		880	
4(Z(107),TAXRT),(Z(108),IDNMAP),(Z(109),IPRMAP),(Z(110),ROEPS),		890	
5(Z(111),RHINI),(Z(112),VINI),(Z(113),FINAL),(Z(114),IVMAP),		900	
6(Z(115),RHOZ),(Z(116),ESA),(Z(117),ESEZ),(Z(118),ESB),		910	
7(Z(119),ESCAPA),(Z(120),ESESQ),(Z(121),ESESQ),(Z(122),ESES),		920	
8(Z(123),ESALPH),(Z(124),ESBETA),(Z(125),ESCAPB),(Z(126),IUMAP),		930	
9(Z(127),SS1),(Z(128),SS2),(Z(129),UMIN),(Z(130),SS4)		940	
EQUIVALENCE			950
1(Z(131),PRTIME),(Z(132),EOR),(Z(133),EOT),(Z(134),EOB),		960	
2(Z(135),EMOR),(Z(136),DXF),(Z(137),DYF),(Z(138),RHOMIN),		970	
3(Z(139),STAB),(Z(140),XIENRG),(Z(141),XKENRG),(Z(142),XTENRG),		980	
4(Z(143),STT),(Z(144),DTMIN),(Z(145),TRNSFC),(Z(146),EMOT),		990	
5(Z(147),JPROJ),(Z(148),CNAUT),(Z(149),BBAR),(Z(150),EMOB)		1000	
			1010
C		1020
C		1030
C	END OF COMMON		1040
C		1050
C		1060
C		1070
C	*** INITIALE BLANK COMMON		1080
LAST = 1			1081
IQ = 0			1082
IQ = IQ+1			1083
Z(IQ) = 0,			1084
IF(LAST.NE.0) GO TO 5			1085
			1086

```

10    CALL INPUT          1090
20    CALL CDT           1110
      CALL EDIT          1130
C      *** ASK WFLAGL WHETHER THIS IS THE LAST CYCLE. 1140
C      WFLAGL IS SET IN EDIT. 1145
      IF (WFLAGL.GT.0.) GO TO 40 1150
      CALL PH1            1160
C      *** NPRINT=1 ON EDIT PRINT CYCLES. 1162
C      INTER.NE.0 WHEN INTERMEDIATE EDIT PRINTS ARE WANTED. 1164
      IF (INTER.NE.0.AND.NPRINT.EQ.1) CALL EDIT 1170
C      *** CYCPH3=-1. WHEN PHASE 3 IS NOT USED. OTHERWISE, 1172
C      CYCPH3=NUMBER OF TIMES PHASE 3 CALCULATIONS ARE 1174
C      SUBCYCLED. 1176
      IF (CYCPH3.EQ.(-1.)) GO TO 30 1180
      CALL PH3             1190
      IF (INTER.NE.0.AND.NPRINT.EQ.1) CALL EDIT 1200
30    CALL PH2             1210
      GO TO 20             1220
40    CALL EXIT            1230
      END                  1240-

```

SUBROUTINE INPUT INP 10
 INP 20
 INP 30
 INP 40
 INP 50
 INP 60
 INP 70
 INP 80
 INP 90
 INP 100
 INP 110
 INP 120
 INP 130
 INP 140
 INP 150
 INP 160
 INP 170
 INP 180
 INP 190
 INP 200
 INP 210
 INP 220
 INP 230
 INP 240
 INP 250
 INP 260
 INP 270
 INP 280
 INP 290
 INP 300
 INP 310
 INP 320
 INP 330
 INP 340
 INP 350
 INP 360
 INP 370
 INP 380
 INP 390
 INP 400
 INP 410
 INP 420
 INP 430
 INP 440
 INP 450
 INP 460
 INP 470
 INP 480
 INP 490
 INP 500
 INP 510
 INP 520
 INP 530
 INP 540
 INP 550
 INP 560
 INP 570
 INP 580

C C
 DIMENSION AMX(2502),AIX(2502),U(2502),V(2502),P(2502),
 1 X(52),XX(54),TAU(52),JPM(52),
 2 Y(102),YY(104),FLEFT(102),YAMC(102),SIGC(102),
 3 GAMC(102),
 4 PK(15),Z(150),
 5 XP(26,51),YP(26,51),
 6 PL(204),UL(204),PR(204),
 7 RSN(52),RST(52),
 8 CMXP(5),CMYP(5),IJ(5),JK(5),
 9 DX(52),DDX(54),DY(102),DDY(104),
 S SNB(52),STB(52),UK(52,3),VK(52,3),RHO(52,3)

C C
 *** DIMENSIONED ARRAYS
 *** Z-BLOCK IS SAVED ON TAPE.

COMMON Z
 COMMON PK
 COMMON YY, XX
 COMMON DDX, DDY
 COMMON AMX, AIX, U, V, P
 COMMON TAU, JPM
 COMMON UL, PL
 COMMON XP, YP, CMXP, CMYP

C C
 *** NON-DIMENSIONED VARIABLES

COMMON AID,AMMV,AMMY,AMPY,AMUR,AMUT,AMVR,
 1 AMVT,DELEB,DELER,DELET,DELM,DTODX,DXYMIN,EAMMP,EAMPY,
 2 E,ERDUMP,I,I3,IWS,J,K,KA,KB,
 3 LL,MD,ME,MZT,NERR,NK,NPRINT,
 4 NR,NRZ,NULLE,PIDTS,SIEMIN,SNR,SNT,STR,SOLID,
 5 SUM,TESTRH,TWOP,I,URR,WS,WSA,WSB,WSC,WFLAGF,
 6 WFLAGL,WFLAGP

C C
 *** THE FOLLOWING EQUIVALENCES MAKE AVAILABLE
 X(0), Y(0), DX(0), DY(0)

C C
 EQUIVALENCE (XX(2), X(1)), (YY(2), Y(1))
 EQUIVALENCE (DDX(2), DX(1)), (DDY(2), DY(1))

C C
 *** SPECIAL EQUIVALENCES FOR PH2 ONLY

C C
 EQUIVALENCE (UL,FLEFT), (UL(103),YAMC),
 1 (PL,GAMC,PR), (PL(103),SIGC)

C C
 *** SPECIAL EQUIVALENCES FOR PH3 ONLY

C C
 EQUIVALENCE (UL,RSN),
 1 (PL,RST), (P,UK),
 2 (P(157),VK), (P(313),SNB),
 3 (P(365),STB), (P(417),RHO)

C C
 *** SPECIAL EQUIVALENCES FOR EDIT

C C
 EQUIVALENCE (PR(1), IJ), (PR(6), JK)

C C
 *** Z-STORAGE EQUIVALENCES

C C
 EQUIVALENCE (Z(1),PROB),(Z(2),CYCLE),(Z(3),RHO)

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1(Z( 3),DT ),(Z( 4),NUMSP ),(Z( 5),NFRELP ),(Z( 6),NDUMP7 ), INP 590
2(Z( 7),ICSTOP ),(Z( 8),PIDY ),(Z( 9),TOPMU ),(Z(10),RTMU ), INP 600
3(Z(11),STK1 ),(Z(12),NUMREZ ),(Z(13),ETH ),(Z(14),UN14 ), INP 610
4(Z(15),RHINIT ),(Z(16),PROJI ),(Z(17),UN17 ),(Z(18),XMAX ), INP 620
5(Z(19),NZ ),(Z(20),NREZ ),(Z(21),AMDM ),(Z(22),UVMAX ), INP 630
6(Z(23),UN23 ),(Z(24),DMIN ),(Z(25),JSTR ),(Z(26),DTNA ), INP 640
7(Z(27),CVIS ),(Z(28),STK2 ),(Z(29),STEZ ),(Z(30),NC ), INP 650
8(Z(31),UN31 ),(Z(32),NRC ),(Z(33),IMAX ),(Z(34),IMAXA ), INP 660
9(Z(35),JMAX ),(Z(36),JMAXA ),(Z(37),KMAX ),(Z(38),KMAXA ) INP 670
EQUIVALENCE INP 680
1(Z(39),BOTM ),(Z(40),BOTMV ),(Z(41),NUMSPT ),(Z(42),CZERO ), INP 690
2(Z(43),NUMSCA ),(Z(44),PRLIM ),(Z(45),PRDELT ),(Z(46),PRFACT ) INP 700
EQUIVALENCE INP 710
1(Z(47),I1 ),(Z(48),I2 ),(Z(49),IPCYCL ),(Z(50),TSTOP ), INP 720
2(Z(51),RHOFIL ),(Z(52),TARGV ),(Z(53),N3 ),(Z(54),IVARDY ), INP 730
3(Z(55),VT ),(Z(56),N6 ),(Z(57),RTM ),(Z(58),RTMV ), INP 740
4(Z(59),UN59 ),(Z(60),N10 ),(Z(61),N11 ),(Z(62),GAMMA ), INP 750
5(Z(63),TOPM ),(Z(64),BOTMU ),(Z(65),SN ),(Z(66),TOPMV ), INP 760
6(Z(67),PRYBOT ),(Z(68),PRYTOP ),(Z(69),PRXRT ),(Z(70),CYCPH3 ), INP 770
7(Z(71),REZFCT ),(Z(72),TARGI ),(Z(73),PROJU ),(Z(74),BBOUND ), INP 780
8(Z(75),EVAP ),(Z(76),ECK ),(Z(77),NECYCL ),(Z(78),II ), INP 790
9(Z(79),JJ ),(Z(80),NMP ),(Z(81),Y2 ),(Z(82),EZPH1 ) INP 800
EQUIVALENCE INP 810
1(Z(83),IVARDX ),(Z(84),T ),(Z(85),NMPMAX ),(Z(86),PMIN ), INP 820
2(Z(87),INTER ),(Z(88),TAYBOT ),(Z(89),TAYTOP ),(Z(90),IEMAP ), INP 830
3(Z(91),MC ),(Z(92),MR ),(Z(93),MZ ),(Z(94),MB ) INP 840
EQUIVALENCE INP 850
1(Z(95),REZ ),(Z(96),NODUMP ),(Z(97),UN97 ),(Z(98),UN98 ), INP 860
2(Z(99),UN99 ),(Z(100),EVAPM ),(Z(101),EVAPEN ),(Z(102),EVAPMU ), INP 870
3(Z(103),EVAPMV ),(Z(104),EZPH2 ),(Z(105),SNL ),(Z(106),STL ), INP 880
4(Z(107),TAXRT ),(Z(108),IDNMAP ),(Z(109),IPRMAP ),(Z(110),ROEPS ), INP 890
5(Z(111),RHINI ),(Z(112),VINI ),(Z(113),FINAL ),(Z(114),IVMAP ), INP 900
6(Z(115),RHOZ ),(Z(116),ESA ),(Z(117),ESEZ ),(Z(118),ESB ), INP 910
7(Z(119),ESCAPA ),(Z(120),ESEESP ),(Z(121),ESESQ ),(Z(122),ESES ), INP 920
8(Z(123),ESALPH ),(Z(124),ESBETA ),(Z(125),ESCAPB ),(Z(126),IUMAP ) INP 930
9(Z(127),SS1 ),(Z(128),SS2 ),(Z(129),UMIN ),(Z(130),SS4 ) INP 940
EQUIVALENCE INP 950
1(Z(131),PRTIME ),(Z(132),EOR ),(Z(133),EOT ),(Z(134),EOB ), INP 960
2(Z(135),EMOR ),(Z(136),DXF ),(Z(137),DYF ),(Z(138),RHOMIN ), INP 970
3(Z(139),STAB ),(Z(140),XIENRG ),(Z(141),XKENRG ),(Z(142),XTENRG ), INP 980
4(Z(143),STT ),(Z(144),DTMIN ),(Z(145),TRNSFC ),(Z(146),EMOT ), INP 990
5(Z(147),JPROJ ),(Z(148),CNAUT ),(Z(149),BBAR ),(Z(150),EMOB ) INP1000
INP1010
C ..... INP1020
C ..... INP1030
C END OF COMMON INP1040
C ..... INP1050
C ..... INP1060
C ..... INP1070
C *** MZT MUST EQUAL NUMBER OF WORDS IN Z-ARRAY. INP1080
C MZT=150 INP1090
C *** SET WFLAGF=1. TO SAY THIS IS FIRST CYCLE OF THIS RUN. INP1095
C WFLAGF=1. INP1100
C *** READ AND PRINT ID HEADING CARD (FIRST CARD IN INP1110
C INPUT DECK) INP1115
C READ (5,370) IWS INP1120
C WRITE (6,370) IWS INP1130

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C *** CARDS ROUTINE WILL READ AND PRINT FIRST DATA CARD. INP1140
C CALL CARDS INP1150
C *** PK(3).LT.0. MEANS THIS PROBLEM IS BEING RESTARTED FROM INP1152
C TAPE 7 AND SETUP IS NOT NEEDED. INP1155
C IF (PK(3).LT.0.) GO TO 70 INP1160
C *** SINCE THE SETUP ROUTINE WRITES ON TAPE 7, MAKE INP1170
C SURE THIS IS A SETUP AND NOT A RESTART RUN TO AVOID INP1180
C WRITING OVER A GOOD DUMP TAPE. INP1190
C CALL CARDS INP1190
C *** Z(1)=PROB IS DEFINED BY THE SECOND CARD OF A SETUP INP1200
C DECK, BUT IS NOT DEFINED IN A RESTART DECK. INP1205
C THEREFORE IF Z(1)=0., THIS IS A RESTART RUN, AND IF INP1210
C Z(1).NE.0., THIS IS A SETUP RUN. INP1215
5 IF(PROB.EQ.0.)GO TO 230 INP1220
CALL SETUP INP1230
GO TO 70 INP1240
10 CONTINUE INP1250
CALL CARDS INP1260
C *** INITIALIZE P-STORAGE. INP1265
20 DO 30 K=1,KMAXA INP1270
30 P(K)=0.0 INP1280
C *** SET T AND NC SO THEY WILL EQUAL ZERO ON FIRST EDIT INP1282
C PRINT AFTER BEING INCREMENTED BY CDT. INP1284
T=T-DTNA INP1290
NC=NC-1 INP1300
C *** CHECK FATAL INPUT ERRORS. INP1305
32 IF(RHOZ.LE.0.) GO TO 260 INP1310
34 IF(ESCAPA.LT.0.) GO TO 270 INP1320
36 IF(IMAX.EQ.0.OR.JMAX.EQ.0) GO TO 280 INP1340
C *** DEFINE CONSTANTS USED THROUGHOUT CALCULATION. INP1345
CNAUT=SQRT(ESCAPA/RHOZ) INP1350
WS=ESESP-ESES INP1360
IF (WS.LE.0.) WS=1. INP1370
SS1=1./WS INP1380
TESTRH=.2*RHOZ INP1390
CYCLE=NC INP1400
NRZ=NREZ-NUMREZ INP1420
SOLID=AMDM*RHOZ INP1430
GAMMA=ESA+1. INP1440
TWOP1=2.*PIDY INP1450
PMIN=10.**6 INP1460
TRNSFC=.4 INP1470
VT=10.**(-5) INP1475
SS2=1. INP1480
C *** SET NUMBER OF SYMBOLS TO BE USED IN PRINTED CONTOUR INP1482
C MAPS. INP1484
IDNMAP=28. INP1490
IPRMAP=26. INP1500
IVMAP=26. INP1510
IUMAP=26. INP1520
IEMAP=26. INP1530
C *** PRINT VALUES OF MOST INPUT PARAMETERS. INP1555
WRITE(6,310) NUMREZ,JSTR,N6,IMAX,JMAX,I1,I2,JPROJ,NMPMAX,INTER,NUINP1560
1MSCA,IPCYCL,ICSTOP,NFREL,P,NDUMP7,NODUMP,IVARDX,IVARDY INP1570
WRITE(6,320) DXF,DYF,RHOMIN,TESTRH,RHOZ,RHINI,RHINIT,AMDM,SOLID,VINP1580
1T,EVAP,ROEPS,SN,BBAR,CNAUT,FINAL,STAB,DMIN,CVIS,SS2,CYCPH3,CZERO,SINP1590
2TK1,STK2,STEZ,ESA,ESB,ESCAPA,ESCAPB,ESALPH,ESBETA,ESEZ,ESES,ESESP,INP1600

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3ESESQ,REZFCT,SS4,Y2,TRNSFC,DTMIN,PRDELT,PRFACT,PRLIM,TSTOP      INP1610
C   *** PRINT DX,DY ARRAYS WHEN THE CELL DIMENSIONS ARE          INP1620
C   VARIABLE.                                                 INP1625
C   IF (IVARDX.EQ.0) GO TO 40                                     INP1630
C   WRITE (6,330)                                                 INP1640
C   WRITE (6,350) (I,DX(I),I=1,IMAX)                                INP1650
40  IF (IVARDY.EQ.0) GO TO 50                                     INP1660
C   WRITE (6,340)                                                 INP1670
C   WRITE (6,350) (J,DY(J),J=1,JMAX)                                INP1680
50  CONTINUE                                                 INP1690
C   *** WHEN T.GT.0., PROBLEM IS BEING RESTARTED.                 INP1695
C   IF (T.GT.0.) GO TO 60                                         INP1700
C   *** DEFINE TIME OF FIRST EDIT PRINT AFTER CYCLE 0.           INP1705
PRTIME=PRDELT
GO TO 300
C   *** PRDELT = 0. WHEN PRINTING ON CYCLES RATHER TIME.        INP1725
60  IF (PRDELT.EQ.0.) GO TO 300                                    INP1730
C   *** DEFINE TIME OF FIRST EDIT PRINT AFTER RESTART CYCLE.    INP1735
IWS=T/PRDELT+1.
PRTIME=FLOAT(IWS)*PRDELT
GO TO 300
C   *** READ DUMP TAPE 7.                                         INP1740
70  CONTINUE                                                 INP1750
IWS=0
80  REWIND 7                                         INP1760
90  READ (7) PR(1),PR(2),N3
C   *** NR = NUMBER OF RECORDS WRITTEN BY EACH TAPE DUMP.       INP1770
C   WHEN N3=1, TRACER POINTS ARE BEING USED AND MAKE UP          INP1780
C   ANOTHER RECORD IN EACH TAPE DUMP.                               INP1790
NR=N3+7
C   *** FIRST WORD OF FIRST RECORD OF EACH DUMP SHOULD BE       INP1800
C   555.0. TEST THIS THREE TIMES BEFORE EXITING.                INP1810
IF (PR(1)-555.0) 100,110,100
100 IWS=IWS+1
IF (MOD(IWS,3)) 220,220,80
110 IF (PR(2)) 100,120,120
C   *** WHEN SETTING UP A PROBLEM PR(2) = PK(2) = 0. WHEN       INP1820
C   RESTARTING A PROBLEM, TAPE 7 IS READ UNTIL                  INP1830
C   PR(2).GE.PK(2), THE RESTART CYCLE NUMBER.                   INP1840
120 IF (PK(2)-PR(2)) 150,150,130
130 DO 140 L=2,NR
140 READ (7)
GO TO 90
150 READ (7) (Z(I),I=1,MZT)
C   *** MAKE SURE PROBLEM NUMBER ON TAPE (PROB) MATCHES        INP1850
C   PROBLEM NUMBER ON INPUT CARDS (PK(1)).                      INP1860
IF (ABS(PROB-PK(1))-0.01) 160,160,210
160 READ (7) (U(I),V(I),AMX(I),AIX(I),P(I),I=1,KMAXA)        INP1870
READ (7) X(0),(X(I),TAU(I),JPM(I),I=1,IMAX)                  INP1880
READ (7) (Y(I),I=0,JMAX)                                     INP1890
C   *** Y2=-1. WHEN TRACER POINTS ARE USED.                   INP1900
IF (Y2.GT.(-1.)) GO TO 170
170 READ (7) ((XP(I,J),YP(I,J),I=1,II),J=1,JJ)              INP1910
READ (7) (DX(I),I=1,IMAX)                                     INP1920
READ (7) (DY(J),J=1,JMAX)                                     INP1930
READ (7) PR(1),PR(2),PR(3)
C   *** THE FIRST WORD OF THE LAST RECORD OF EACH DUMP SHOULD INP1940

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3ESESQ,REZFCT,SS4,Y2,TRNSFC,DTMIN,PRDELT,PRFACT,PRLIM,TSTCP INP1610
      *** PRINT DX,DY ARRAYS WHEN THE CELL DIMENSIONS ARE INP1620
      VARIABLE. INP1625
C       IF (IVARDX.EQ.0) GO TO 40 INP1630
C       WRITE (6,330) INP1640
C       WRITE (6,350) (I,DX(I),I=1,IMAX) INP1650
40     IF (IVARDY.EQ.0) GO TO 50 INP1660
C       WRITE (6,340) INP1670
C       WRITE (6,350) (J,DY(J),J=1,JMAX) INP1680
50     CONTINUE INP1690
C           *** WHEN T.GT.0., PROBLEM IS BEING RESTARTED. INP1695
IF (T.GT.0.) GO TO 60 INP1700
C           *** DEFINE TIME OF FIRST EDIT PRINT AFTER CYCLE 0. INP1705
PRTIME=PRDELT INP1710
GO TO 300 INP1720
C           *** PRDELT = 0. WHEN PRINTING ON CYCLES RATHER TIME. INP1725
60     IF (PRDELT.EQ.0.) GO TO 300 INP1730
C           *** DEFINE TIME OF FIRST EDIT PRINT AFTER RESTART CYCLE. INP1735
IWS=T/PRDELT+1. INP1740
PRTIME=FLOAT(IWS)*PRDELT INP1750
GO TO 300 INP1760
C           *** READ DUMP TAPE 7. INP1770
70     CONTINUE INP1800
IWS=0 INP1810
80     REWIND 7 INP1820
90     READ (7) PR(1),PR(2),N3 INP1830
C           *** NR = NUMBER OF RECORDS WRITTEN BY EACH TAPE DUMP. INP1832
C           WHEN N3=1, TRACER POINTS ARE BEING USED AND MAKE UP INP1834
C           ANOTHER RECORD IN EACH TAPE DUMP. INP1836
NR=N3+7 INP1840
C           *** FIRST WORD OF FIRST RECORD OF EACH DUMP SHOULD BE INP1842
C           555.0. TEST THIS THREE TIMES BEFORE EXITING. INP1844
IF (PR(1)-555.0) 100,110,100 INP1850
100    IWS=IWS+1 INP1860
IF (MOD(IWS,3)) 220,220,80 INP1870
110    IF (PR(2)) 100,120,120 INP1880
C           *** WHEN SETTING UP A PROBLEM PR(2) = PK(2) = 0. WHEN INP1882
C           RESTARTING A PROBLEM, TAPE 7 IS READ UNTIL INP1884
C           PR(2).GE.PK(2), THE RESTART CYCLE NUMBER. INP1886
120    IF (PK(2)-PR(2)) 150,150,130 INP1890
130    DO 140 L=2,NR INP1900
140    READ (7) INP1910
      GO TO 90 INP1920
150    READ (7) (Z(I),I=1,MZT) INP1930
C           *** MAKE SURE PROBLEM NUMBER ON TAPE (PROB) MATCHES INP1932
C           PROBLEM NUMBER ON INPUT CARDS (PK(1)). INP1934
IF (ABS(PROB-PK(1))-0.1) 160,160,210 INP1940
160    READ (7) (U(I),V(I),AMX(I),AIX(I),P(I),I=1,KMAXA) INP1950
      READ (7) ((0),(X(I),TAU(I),JPM(I),I=1,IMAX) INP1960
      READ (7) (Y(I),I=0,JMAX) INP1970
C           *** Y2=-1. WHEN TRACER POINTS ARE USED. INP1980
IF (Y2.GT.(-1.)) GO TO 170 INP1990
      READ (7) ((XP(I,J),YP(I,J),I=1,II),J=1,JJ) INP2000
170    READ (7) (DX(I),J=1,IMAX) INP2010
      READ (7) ((Y(J),J=1,JMAX) INP2020
      READ (7) PR(1),PR(2),PR(3) INP2030
C           *** THE FIRST WORD OF THE LAST RECORD OF EACH DUMP SHOULD INP2032

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C           BE 555.0 OR 666.0.          INP2034
175      IF(PR(1)=555.0) 240,10,180   INP2040
180      IF(PR(2)=666.0) 250,10,250   INP2050
200      CALL CARDS                 INP2070
        CALL SETUP                  INP2080
        GO TO 20                   INP2090
C           *** PROBLEM NUMBER ON TAPE 7 NOT THE SAME AS PROBLEM
C           NUMBER ON INPUT CARDS.    INP2092
C           NK=150                  INP2100
        GO TO 290                  INP2110
C           *** CANNOT FIND FIRST WORD OF FIRST RECORD.    INP2115
220      NK=100                  INP2120
        GO TO 290                  INP2130
C           *** NOT A RESTART AND YET Z(1) = 0.    INP2135
230      NK=5                   INP2140
        GO TO 290                  INP2150
C           *** FIRST WORD OF LAST RECORD IS INCORRECT.    INP2155
240      NK=175                  INP2160
        GO TO 290                  INP2170
C           *** FIRST WORD OF LAST RECORD IS INCORRECT.    INP2175
250      NK=180                  INP2180
        GO TO 290                  INP2190
C           *** RH0Z.LE.0.          INP2200
260      NK=32                   INP2210
        GO TO 290                  INP2220
C           *** ESCAPA.LT.0.        INP2230
270      NK=34                   INP2240
        GO TO 290                  INP2250
C           *** IMAX OR JMAX IS ZERO    INP2260
280      NK=36                   INP2270
290      NR=1                   INP2280
C           *** PRINT FIRST THREE WORDS OF DUMP (PR(1),PR(2),N3)
C           AND Z(151),Z(152),Z(153).    INP2282
C           WRITE(6,360) PR(1), Z(151), PR(2), Z(152), N3, Z(153)    INP2284
CALL ERROR
300      RETURN
C
310      FORMAT (//12X,9H NUMREZ=,I2,7H JSTR=,I3,5H N6=I3,7H IMAX=,I3,7H
1H JMAX=,I3,5H I1=,I3,5H I2=,I3,8H JPROJ=,I3,9H NMPMAX=,I5,8H    INP2330
2 INTER=,I2,9H NUMSCA=,I2,7H IPCYCL=,I3,9H ICSTOP=,I4,9H NFRELPI    INP2350
3=,I3,9H NDUMP7=,I3,9H NODUMP=,I2,9H IVARDX=,I2,9H IVARDY=,I2,9H    INP2360
4)
320      FORMAT (1X,120H          DXF          DYF          RHOMIN      TESTRH    INP2380
1     RHOZ       RHINI      RHI1 1      AMDM        SOLID      INP2390
2     VT/1X,1P10E12.4//1X,120H          .PS        SN          INP2400
3     SBAR       CNAUT      FINAL       STAB        DMIN       CVI       INP2410
4S    SS2/1X,1P10E12.4//1X,120H          CYCPH3    CZERO      INP2420
5     STK1       STK2       STEZ       ESA         ESB        ESCAPA    INP2430
6     ESCAPB     ESALPH/1X,1P10E12.4//1X,96H          ESBETA    ESINP2440
7EZ   ESES       ESESP      ESESQ      REZFCT    SS4        INP2450
8     Y2/1X,1P8E12.4//1X,72H          TRNSFC    DTMIN      PRDELT    INP2460
9     PRFACT     PRLIM      TSTOP/1X,1P6E12.4)          ESBETA
330      FORMAT (//7(3H I,6X,2HDR,7X))          INP2480
340      FORMAT (//7(3H J,6X,2HDZ,7X))          INP2490
350      FORMAT (7(I4,2X,1PE9.3,3X))          INP2500
360      FORMAT (1H1,5X,72H*** CHECK FIRST RECORD OF THE DUMP AND FIRST DAT
1A CARD OF THE INPUT DECK // 4X,7HON TAPE,41X,8HON CARDS / 4X,

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24HWS =,F6.1,4X,7H(555.0),24X, 8HZ(151) =,F8.4,3X,16H(PROBLEM NUMBER
3R) / 8H CYCLE =,F6.1,4X,18H(CYCLE BEING READ),13X, 8HZ(152) =F5.1,
46X,15H(RESTART CYCLE) / 4X,4HN3 =,I4,6X,19H(TRACER POINT FLAG) ,
512X, 8HZ(153) =,F5.1,6X,14H(RESTART FLAG))

370 FORMAT (I1,71H

1)

END

INP2520
INP2530
INP2540~

```

SUBROUTINE CARDS CRD 10
DIMENSION TABLE(1),CARD(7),LABEL(1) CRD 20
DIMENSION INPERR(1) CRD 30
COMMON TABLE CRD 40
EQUIVALENCE(TABLE(1),LABEL(1)) CRD 50
INPERR=0 CRD 60
WRITE (6,80) CRD 70
10 READ (5,90) IEND,LOC,NUMWPC,(CARD(I),I=1,NUMWPC) CRD 80
      WRITE (6,100) IEND,LOC,NUMWPS,(CARD(I),I=1,NUMWPC) CRD 90
      IF (NUMWPC.LT.1) GO TO 50 CRD 100
      IF (LOC.LT.1) GO TO 70 CRD 110
      DO 30 I=1,NUMWPC CRD 120
      J=LOC+I-1 CRD 130
      IF (IEND.NE.2) GO TO 20 CRD 140
      LABEL(J)=;FIX(CARD(I)) CRD 150
      GO TO 30 CRD 160
20 TABLE(J)=CARD(I) CRD 170
30 CONTINUE CRD 180
40 IF (IEND.NE.1) GO TO 10 CRD 190
      IF (INPERR.EQ.0) RETURN CRD 200
      STOP CRD 210
50 IF (LOC.NE.0) GO TO 70 CRD 220
      DO 60 I=1,7 CRD 230
      IF (CARD(I).NE.0.) GO TO 70 CRD 240
60 CONTINUE CRD 250
      WRITE (6,120) CRD 260
      GO TO 40 CRD 270
70 WRITE (6,110) CRD 280
      INPERR=1 CRD 290
      GO TO 40 CRD 300
C FORMATS CRD 310
C
80 FORMAT (/18H INPUT CARDS//) CRD 320
90 FORMAT (I1,I5,I1,0P7E9.4) CRD 330
100 FORMAT (1H I4,I7,I3,1P7E14.6) CRD 340
110 FORMAT (//42H **** ERROR ON PRECEDING DATA CARD *****/) CRD 350
120 FORMAT (//18H BLANK CARD *****/) CRD 360
      END CRD 370
                               CRD 380-

```

SUBROUTINE SETUP

```

C   .....SET 10
C   .....SET 20
C   .....SET 30
C   .....SET 40
C   DIMENSION AMX(2502),AIX(2502),U(2502),V(2502),P(2502),
1      X(52),XX(54),TAU(52),JPM(52),SET 50
2      Y(102),YY(104),FLEFT(102),YAMC(102),SIGC(102),SET 60
3      GAMC(102),SET 70
4      PK(15),Z(150),SET 80
5      XP(26,51),YP(26,51),SET 90
6      PL(204),UL(204),PR(204),SET 100
7      RSN(52),RST(52),SET 110
8      CMXP(5),CMYP(5),IJ(5),JK(5),SET 120
9      DX(52),DDX(54),DY(102),DDY(104),SET 130
$      SNB(52),STB(52),UK(52,3),VK(52,3),RHO(52,3)SET 140
C   *** DIMENSIONED ARRAYS
C   *** Z-BLOCK IS SAVED ON TAPE.

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```

COMMON Z
COMMON PK
COMMON YY, XX
COMMON DDX, DDY
COMMON AMX, AIX, U, V, P
COMMON TAU, JPM
COMMON UL, PL
COMMON XP, YP, CMXP, CMYP

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*** NON-DIMENSIONED VARIABLES

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COMMON AID,AMMV,AMMY,AMPY,AMUR,AMUT,AMVR,
1AMVT,DELEB,DELER,DELET,DELM,DTODX,DXYMIN,EAMMP,EAMPY,
2E,ERDUMP,I,I3,IWS,J,K,KA,KB,
3LL,MD,ME,MZT,NERR,NK,NPRINT,
4NR,NRZ,NULLE,PIDTS,SIEMIN,SNR,SNT,STR,SOLID,
5SUM,TESTRH,TWOP,URR,WS,WSA,WSB,WSC,WFLAGF,
6WFLAGL,WFLAGP

```

*** THE FOLLOWING EQUIVALENCES MAKE AVAILABLE
 $X(0)$, $Y(0)$, $DX(0)$, $DY(0)$

EQUIVALENCE (XX(2), X(1)), (YY(2), Y(1))
EQUIVALENCE (DDX(2), DX(1)), (DDY(2), DY(1))

*** SPECIAL EQUIVALENCES FOR PH2 ONLY

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EQUIVALENCE (UL,FLEFT),
1          (PL,GAMC,PR), (UL(103),YAMC),
          (PL(103),SIGC)

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*** SPECIAL EQUIVALENCES FOR PH3 ONLY.

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EQUIVALENCE (UL,RSN),
1          (PL,RST),
2          (P(157),VK),
3          (P(365),STB), (P,UK),
          (P(313),SNB),
          (P(417),RHO)

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*** SPECIAL EQUIVALENCES FOR EDIT.

EQUIVALENCE (PR(1), IJ), (PR(6), JK)

*** Z-STORAGE EQUIVALENCES

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EQUIVALENCE (Z( 1),PROB),(Z( 2),CYCLE),SET 580

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), (Z( 3),DT ), (Z( 4),NUMSP ), (Z( 5),NFRELP ), (Z( 6),NDUMP7 ), SET 590
2(Z( 7),ICSTOP ), (Z( 8),PIDY ), (Z( 9),TOPMU ), (Z( 10),RTMU ), SET 600
3(Z( 11),STK1 ), (Z( 12),NUMREZ ), (Z( 13),ETH ), (Z( 14),UN14 ), SET 610
4(Z( 15),RHINIT ), (Z( 16),PROJI ), (Z( 17),UN17 ), (Z( 18),XMAX ), SET 620
5(Z( 19),NZ ), (Z( 20),NREZ ), (Z( 21),AMDM ), (Z( 22),UVMAX ), SET 630
6(Z( 23),UN23 ), (Z( 24),DMIN ), (Z( 25),JSTR ), (Z( 26),DTNA ), SET 640
7(Z( 27),CVIS ), (Z( 28),STK2 ), (Z( 29),STEZ ), (Z( 30),NC ), SET 650
8(Z( 31),JN31 ), (Z( 32),NRC ), (Z( 33),IMAX ), (Z( 34),IMAXA ), SET 660
9(Z( 35),JMAX ), (Z( 36),JMAXA ), (Z( 37),KMAX ), (Z( 38),KMAXA ) SET 670
EQUIVALENCE SET 680
1(Z( 39),BOTM ), (Z( 40),BOTMV ), (Z( 41),NUMSPT ), (Z( 42),CZERO ), SET 690
2(Z( 43),NUMSCA ), (Z( 44),PRLIM ), (Z( 45),PRDELT ), (Z( 46),PRFACT ) SET 700
EQUIVALENCE SET 710
1(Z( 47),I1 ), (Z( 48),I2 ), (Z( 49),IPCYCL ), (Z( 50),TSTOP ), SET 720
2(Z( 51),RHOFIL ), (Z( 52),TARGV ), (Z( 53),N3 ), (Z( 54),IVARDY ), SET 730
3(Z( 55),VT ), (Z( 56),N6 ), (Z( 57),RTM ), (Z( 58),RTMV ), SET 740
4(Z( 59),UN59 ), (Z( 60),N10 ), (Z( 61),N11 ), (Z( 62),GAMMA ), SET 750
5(Z( 63),TOPM ), (Z( 64),BOTMU ), (Z( 65),SN ), (Z( 66),TOPMV ), SET 760
6(Z( 67),PRYBOT ), (Z( 68),PRYTOP ), (Z( 69),PRXRT ), (Z( 70),CYCPH3 ), SET 770
7(Z( 71),REZFCT ), (Z( 72),TARGI ), (Z( 73),PROJU ), (Z( 74),BBOUND ), SET 780
8(Z( 75),EVAP ), (Z( 76),ECK ), (Z( 77),NECYCL ), (Z( 78),II ), SET 790
9(Z( 79),JJ ), (Z( 80),NMP ), (Z( 81),Y2 ), (Z( 82),EZPH1 ) SET 800
EQUIVALENCE SET 810
1(Z( 83),IVARDX ), (Z( 84),T ), (Z( 85),NMPMAX ), (Z( 86),PMIN ), SET 820
2(Z( 87),INTER ), (Z( 88),TAYBOT ), (Z( 89),TAYTOP ), (Z( 90),IEMAP ), SET 830
3(Z( 91),MC ), (Z( 92),MR ), (Z( 93),MZ ), (Z( 94),MB ) SET 840
EQUIVALENCE SET 850
1(Z( 95),REZ ), (Z( 96),NODUMP ), (Z( 97),UN97 ), (Z( 98),UN98 ), SET 860
2(Z( 99),UN99 ), (Z(100),EVAPM ), (Z(101),EVAPEN ), (Z(102),EVAPMU ), SET 870
3(Z(103),EVAPMV ), (Z(104),EZPH2 ), (Z(105),SNL ), (Z(106),STL ), SET 880
4(Z(107),TAXRT ), (Z(108),IDNMAP ), (Z(109),IPRMAP ), (Z(110),ROEPS ), SET 890
5(Z(111),RHINI ), (Z(112),VINI ), (Z(113),FINAL ), (Z(114),IVMAP ), SET 900
6(Z(115),RHOZ ), (Z(116),ESA ), (Z(117),ESEZ ), (Z(118),ESB ), SET 910
7(Z(119),ESCAPA ), (Z(120),ESESP ), (Z(121),ESESQ ), (Z(122),ESES ), SET 920
8(Z(123),ESALPH ), (Z(124),ESBETA ), (Z(125),ESCAPB ), (Z(126),IUMAP ), SET 930
9(Z(127),SS1 ), (Z(128),SS2 ), (Z(129),UMIN ), (Z(130),SS4 ) SET 940
EQUIVALENCE SET 950
1(Z(131),PRTIME ), (Z(132),EOR ), (Z(133),EOT ), (Z(134),EOB ), SET 960
2(Z(135),EMOR ), (Z(136),DXF ), (Z(137),DYF ), (Z(138),RHOMIN ), SET 970
3(Z(139),STAB ), (Z(140),XIENRG ), (Z(141),XKENRG ), (Z(142),XTENRG ), SET 980
4(Z(143),STT ), (Z(144),DTMIN ), (Z(145),TRNSFC ), (Z(146),EMOT ), SET 990
5(Z(147),JPROJ ), (Z(148),CNAUT ), (Z(149),BBAR ), (Z(150),EMOB ) SET 1000
SET1010

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*** SPECIAL EQUIVALENCES FOR SETUP ONLY SET1020

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EQUIVALENCE (RADIUS,PK(12)), (YCENTR,PK(13)), (RHOSPH,Z(100)), SET1030
1 (SIESPH,Z(101)), (VINSPH,Z(102)), (RHOUT,Z(103)) SET1050

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COMMON/ SPHERE / ADDVL, AREAFC, ISPHMX, JCENTR, JSPHBT, JSPHTP, SET1070
1 RSGRD, VOLSPH, XL2 , XR2 , YBOTTM, YC2 , SET1080
2 YDIFFB, YDIFI, YDIF=0, YDIFT, YLINTA, YLINTB, SET1090
3 YLOWER, YRINTA, YRINTB, YTOP , YUPPER . SET1100

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***** SET1120
SET1130
END OF COMMON SET1140
SET1150

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C .....SET1160
C SET1170
C SET1180
C SET1190
C SET1200
C SET1210
C SET1220
C SET1230
C SET1240
C SET1250
C SET1260
C SET1270
C *** IF DY VARIABLE, Y(I) WILL BE READ IN RATHER THAN
C CALCULATED. SET1280
C
C Y(1)=DYF .
C DO 10 J=2,JMAX SET1290
C Y(J)=Y(J-1)+DYF
C CONTINUE SET1300
C
C *** IF DY VARIABLE, DY(I) WILL BE CALCULATED FROM THE Y(I) SET1310
C READ IN. IF DY CONSTANT, DY(I) WILL EQUAL DYF FOR
C ALL I. SET1320
C
C DO 20 I=1,JMAX SET1330
C DY(I)=DYF
C GO TO 50 SET1340
C
C *** CALCULATE VARIABLE DY(I). SET1350
C DO 40 I=1,JMAX SET1360
C DY(I)=Y(I)-Y(I-1)
C CONTINUE SET1370
C
C *** IF DX VARIABLE, X(I) WILL BE READ IN RATHER THAN
C CALCULATED SET1380
C
C IF (IVARDX.GT.0) GO TO 80 SET1390
C X(1)=DXF
C DO 60 I=2,IMAX SET1400
C X(I)=X(I-1)+DXF
C CONTINUE SET1410
C
C *** IF DX VARIABLE, DX(I) WILL BE CALCULATED FROM
C THE X(I) READ IN. IF DX CONSTANT, DX(I) WILL
C EQUAL DXF FOR ALL I. SET1420
C
C DO 70 I=1,IMAX SET1430
C DX(I)=DXF
C CONTINUE SET1440
C GO TO 100 SET1450
C
C *** CALCULATE VARIABLE DX(I) SET1460
C
C DO 90 I=1,IMAX SET1470
C DX(I)=X(I)-X(I-1)
C *** MAKE SURE DX AND DY ARRAYS HAVE BEEN DEFINED. SET1480
C
C 95 IF (DX(1).GT.0..AND.DY(1).GT.0.) GO TO 100 SET1490
C GO TO 770 SET1500
C CONTINUE SET1510
C
C *** PK(3) = -3. WHEN RESTARTING FROM A CLAM TAPE.
C PROPERTIES OF CELLS HAVE ALREADY BEEN DEFINED
C BUT TRACER POINTS HAVE NOT. SET1520
C
C 100 IF (PK(3).EQ.(-3.)) GO TO 700 SET1530
C *** PRYBOT=-1. MEANS THE PROJECTILE PACKAGE SET1540

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C           IS NOT BEING USED.          SET1674
C   IF (PRYBOT.LT.0.) GO TO 200      SET1680
C           *** DEFINE CELL BOUNDARIES (MB,MC,MR) OF PROJECTILE
C           PACKAGE.                  SET1690
C   IF (IVARDY.GT.0) GO TO 110       SET1695
C           *** CALCULATION FOR CONSTANT DY.
C   MB=INT(PRYBOT/DYF+.5)+1         SET1710
C   IF (MB.GT.JMAX) GO TO 200       SET1720
C   M=1                            SET1730
C   MC=INT(PRYTOP/DYF+.5)           SET1740
C   IF (MC.GT.JMAX) MC=JMAX        SET1750
C   GO TO 160                      SET1760
C           *** CALCULATION FOR VARIABLE DY.
110  DYSUM=0.                      SET1765
I=0
C           *** SEARCH FOR J-VALUE OF BOTTOM OF PROJECTILE (MB).
C   IF (PRYBOT.EQ.0.) GO TO 130      SET1790
DO 120 I=1,JMAX                   SET1800
DYSUM=DYSUM+DY(I)                 SET1810
IF (PRYBOT.LT.DYSUM+.5*DY(I+1).AND.PRYBOT.GE.DYSUM-.5*DY(I)) GO TO 130 SET1820
1 130
120  CONTINUE                      SET1830
     GO TO 200                      SET1840
130  MB=MIN0(I+1,JMAX)             SET1850
M=1
C           *** SEARCH FOR J-VALUE OF TOP OF PROJECTILE (MC).
DO 140 I=MB,JMAX                 SET1880
DYSUM=DYSUM+DY(I)                 SET1890
IF (PRYTOP.GE.DYSUM-.5*DY(I).AND.PRYTOP.LT.DYSUM+.5*DY(I+1)) GO TO 150 SET1900
1 150
140  CONTINUE                      SET1910
     MC=JMAX                        SET1920
     GO TO 160                      SET1930
150  MC=I                          SET1940
C           *** CALCULATION OF I-VALUE OF RIGHT SIDE OF PROJECTILE (MR)
160  IF (IVARDX.GT.0) GO TO 170      SET1950
C           *** CALCULATION FOR CONSTANT DX.
MR=INT(PRXRT/DXF+.5)              SET1960
IF (MR.GT.IMAX) MR=IMAX            SET1965
GO TO 210                          SET1970
C           *** CALCULATION FOR VARIABLE DX.
170  DXSUM=0.                      SET1980
DO 180 I=1,IMAX                   SET1990
DXSUM=DXSUM+DX(I)                 SET2000
IF (PRXRT.GE.DXSUM-.5*DX(I).AND.PRXRT.LT.DXSUM+.5*DX(I+1)) GO TO 190 SET2030
1 190
180  CONTINUE                      SET2040
     MR=IMAX                        SET2050
     GO TO 210                      SET2060
190  MR=I                           SET2070
     GO TO 210                      SET2080
C           *** M=0 MEANS THE PROJECTILE PACKAGE IS NOT BEING USED.
200  M=0                            SET2090
C           *** TAYBOT=-1. MEANS THE TARGET PACKAGE IS NOT BEING USED.
210  IF (TAYBOT.LT.0.) GO TO 310      SET2110
C           *** DEFINE CELL BOUNDARIES(MZ,N,ME) OF TARGET PACKAGE.
IF (IVARDY.GT.0) GO TO 220        SET2120
                                         SET2130
                                         SET2140

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C   *** CALCULATION FOR CONSTANT DY.
    MZ=INT(TAYBOT/DYF+.5)+1          SET2145
    IF (MZ.GT.JMAX) GO TO 310       SET2150
    MD=1                            SET2160
    N=INT(TAYTOP/DYF+.5)            SET2170
    IF (N.GT.JMAX) N=JMAX          SET2180
    GO TO 270                      SET2190
C   *** CALCULATION FOR VARIABLE DY.
220  DYSUM=0.                      SET2200
    I=0                            SET2205
C   *** SEARCH FOR J-VALUE OF BOTTOM OF TARGET (MZ).
    IF (TAYBOT.EQ.0.) GO TO 240     SET2210
    DO 230 I=1,JMAX                SET2220
    DYSUM=DYSUM+DY(I)              SET2225
    IF (TAYBOT.GE.DYSUM-.5*DY(I).AND.TAYBOT.LT.DYSUM+.5*DY(I+1)) GO TOSET2260
1 240
230  CONTINUE                     SET2270
    GO TO 310                      SET2280
240  MZ=MIN0(I+1,JMAX)           SET2290
    MD=1                            SET2300
C   *** SEARCH FOR J-VALUE OF TOP OF TARGET (N).
    DO 250 I=MZ,JMAX              SET2310
    DYSUM=DYSUM+DY(I)              SET2315
    IF (TAYTOP.GE.DYSUM-.5*DY(I).AND.TAYTOP.LT.DYSUM+.5*DY(I+1)) GO TOSET2340
1 260
250  CONTINUE                     SET2350
    N=JMAX                         SET2360
    GO TO 270                      SET2370
260  N=I                           SET2380
C   *** CALCULATION OF I-VALUE OF RIGHT SIDE OF TARGET(ME).
270  IF (IVARDX.GT.0) GO TO 280    SET2390
C   *** CALCULATION FOR CONSTANT DX.
    ME=INT(TAXRT/DXF+.5)           SET2395
    IF (ME.GT.IMAX) ME=IMAX        SET2400
    GO TO 320                      SET2405
C   *** CALCULATION FOR VARIABLE DX.
280  DXSUM=0.                      SET2410
    DO 290 I=1,IMAX                SET2420
    DXSUM=DXSUM+DX(I)              SET2430
    IF (TAXRT.GE.DXSUM-.5*DX(I).AND.TAXRT.LT.DXSUM+.5*DX(I+1)) GO TO 3SET2470
100
290  CONTINUE                     SET2480
    ME=IMAX                         SET2490
    GO TO 320                      SET2500
300  ME=I                           SET2510
    GO TO 320                      SET2520
C   *** MD = 0 MEANS THE TARGET PACKAGE IS NOT BEING USED.
310  MD=0                            SET2530
320  KMAX=IMAX*JMAX+1              SET2540
    KMAXA=KMAX+1                   SET2550
    JMAXA=JMAX+1                   SET2560
    IMAXA=IMAX+1                   SET2570
C   *** INITIALIZE PROPERTY ARRAYS.
    DO 330 K=1,KMAX                SET2580
    U(K)=0.0                        SET2590
    V(K)=0.0                        SET2595
    P(K)=0.0                        SET2600

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AMX(K)=0.0 SET2640
AIX(K)=0.0 SET2650
330 CONTINUE SET2660
PIDY=3.1415927 SET2670
WS=X(1)**2 SET2680
C *** CALCULATE CELL-FACE AREA, THE AREA GENERATED BY SEGMENTSET2682
C X(I),X(I+1) ROTATED ABOUT THE Z-AXIS. SET2684
TAU(1)=PIDY*WS SET2690
DO 340 I=2,IMAX SET2700
WSA=X(I)**2 SET2710
TAU(I)=PIDY*(WSA-WS) SET2720
WS=WSA SET2730
340 CONTINUE SET2740
ETH=0.0 SET2750
C *** RADIUS.GT.0. MEANS SPHERE IS TO BE USED. SET2760
C SEE SPECIAL EQUIVALENCES FOR SETUP FOR LOCATION SET2770
C OF PARAMETERS DEFINING DIMENSIONS AND PROPERTIES OF SET2780
C SPHERE. SET2790
IF (RADIUS.LE.0.) GO TO 540 SET2850
C *** COMPLETE ISPHMX, THE I-INDEX OF THE RIGHT-MOST COLUMN SET2860
C CONTAINING A PART OF THE SPHERE. SET2870
DO 350 I=1,IMAX SET2900
IF (X(I).GE.RADIUS-.000001*DX(I)) GO TO 360 SET2910
350 CONTINUE SET2920
360 ISPHMX=I SET2930
TOTSPH=0. SET2940
C *** COMPUTE JCENTR=J-INDEX OF SPHERE-CENTER SET2950
DO 370 J=0,JMAX SET2960
IF ((Y(J)+.5*DY(J+1)).GT.YCENTR) GO TO 380 SET2970
370 CONTINUE SET2980
C *** YCENTR SHOULD FALL ON CELL BOUNDARY, SET2990
PRINT OUT INPUT VALUE AND ADJUSTED VALUE. SET3000
380 WRITE (6,790) YCENTR,Y(J) SET3010
YCENTR=Y(J) SET3020
JCENTR=J SET3030
C COMPUTE JRADA AND JRADB. SET3035
C *** JRADB = THE NUMBER OF CELLS CONTAINING A PART OF THE SET3040
C SPHERE FROM THE CENTER TO BOTTOM EDGE. SET3050
C *** JRADA = THE NUMBER OF CELLS CONTAINING A PART OF THE SET3060
C SPHERE FROM THE CENTER TO TOP EDGE. SET3070
JRADB=0 SET3080
JRADA=0 SET3090
JB=JCENTR SET3100
JA=JCENTR+1 SET3110
SUM1=0. SET3120
SUM2=0. SET3130
IF (JCENTR.EQ.0) GO TO 400 SET3140
390 SUM1=SUM1+DY(JB) SET3150
JB=JB-1 SET3160
JRADB=JRADB+1 SET3170
IF (SUM1.LT.(RADIUS-.000001*DY(JB))) GO TO 390 SET3180
400 SUM2=SUM2+DY(JA) SET3190
JA=JA+1 SET3200
JRADA=JRADA+1 SET3210
IF (SUM2.LT.(RADIUS-.000001*DY(JA))) GO TO 400 SET3220
C *** COMPUTE(1)JSPHTP=J-INDEX OF UPPER-MOST ROW SET3230
C *** WHICH CONTAINS PART OF THE SPHERE SET3240

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C.           *** (2) JSPHBT=J=INDEX OF LOWEST ROW          SET3250
C.           *** WHICH CONTAINS PART OF THE SPHERE      SET3250
C. JSPHBT=MAX0(1,JCENTR-JRADB+1)                      SET3270
C. JSPHTP=MIN0(JMAX,JCENTR+JRADA)                     SET3280
C.
C. YC2=YCENTR**2                                     SET3290
C. RSQRD=RADIUS**2                                  SET3300
C.           *** FOR EACH CELL IN RECTANGLE FROM X=0.    SET3310
C.           *** TO X=(ISPHMX-1)*DXF AND FROM             SET3320
C.           *** Y=(JSPHBT-1)*DYF TO Y=(JSPHTP)*DYF       SET3330
C.           *** FIND VOLSPH=VOLUME OF SPHERE IN CELL K   SET3340
C.           *** AND SET MASS AND SPEC. INT. ENERGY.     SET3350
C. DO 530 I=1,ISPHMX                                SET3360
C. K=(JSPHBT-1)*IMAX+I+1                            SET3370
C.           *** X(I-1)=VALUE OF X AT LEFT OF COLUMN      SET3380
C.           *** X(I)=VALUE OF X AT RIGHT OF COLUMN       SET3390
C. XL2=(X(I-1))**2                                 SET3400
C. XR2=(X(I))**2                                   SET3410
C.           *** YLINTA=Y-LEFT-INTERCEPT-ABOVE-CENTER    SET3420
C.           *** YLINTB=Y-LEFT-INTERCEPT-BELOW-CENTER     SET3430
C. WS=SQRT(RSQRD-XL2)                               SET3440
C. YLINTA=YCENTR+WS                                SET3450
C. YLINTB=YCENTR-WS                                SET3460
C.           *** DOES CURVE INTERSECT X=X(I)            SET3470
C. IF (RSQRD.LE.XR2) GO TO 410                      SET3480
C.           *** YES                                     SET3490
C. WS=SQRT(RSQRD-XR2)                               SET3500
C. YRINTA=YCENTR+WS                                SET3510
C. YRINTB=YCENTR-WS                                SET3520
C. GO TO 420                                         SET3530
410 YRINTA=YCENTR                                SET3540
C. YRINTB=YCENTR                                SET3550
C. CONTINUE                                         SET3560
C. 420 DO 520 J=JSPHBT,JSPHTP                      SET3570
C.           *** SKIP IF SPECIAL CELL                  SET3610
C. IF (AMX(K).NE.0.) GO TO 520                      SET3620
C. YT0P=Y(J)                                         SET3630
C. YBOTTM=Y(J-1)                                    SET3640
C. YDIFT=(YT0P-YCENTR)**2                           SET3650
C. YDIFFB=(YBOTTM-YCENTR)**2                         SET3660
C. YDIFO=AMAX1(YDIFT,YDIFFB)                       SET3670
C. YDIFI=AMIN1(YDIFT,YDIFFB)                        SET3680
C.           *** IS ALL OF CELL WITHIN SPHERE BOUNDARY.  SET3690
C. IF ((YDIFO+XR2).GT.RSQRD) GO TO 430            SET3695
C.           *** YES. DEFINE VOLUME OF CELL.          SET3700
C. VOLSPH=TAU(I)*DY(J)                            SET3705
C. GO TO 470                                         SET3710
C.           *** NO. IS ALL OF CELL OUTSIDE SPHERE BOUNDARY. SET3720
430 IF ((YDIFI+XL2).LT.RSQRD) GO TO 440          SET3725
C.           *** YES.                                SET3730
C. VOLSPH=0.                                         SET3735
C. GO TO 510                                         SET3740
C.           *** NO. PART OF CELL IS WITHIN SPHERE. COMPUTE VOLUME  SET3750
C.           *** OF PART OF CELL INSIDE THE SPHERE AND STORE    SET3754
C.           *** IN VOLSPH.                                SET3756
440 IF (J.GT.JCENTR) GO TO 450                      SET3760
C. YLOWER=AMAX1(YBOTTM,YLINTB)                      SET3770

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YUPPER=AMIN1(YTOP,YRINTB) SET3790
ADDVL=(YTOP-YUPPER)*TAU(I) SET3790
GO TO 460 SET3800
450 YLOWER=AMAX1(YBOTTM,YRINTA) SET3810
YUPPER=AMIN1(YTOP,YLINTA) SET3820
ADDVL=(YLOWER-YBOTTM)*TAU(I) SET3830
460 VOLSPH=ADDVL+PIDY*((RSQRD-YC2-XL2)*(YUPPER-YLOWER)-(YUPPER**3-YLOWSET3840
1ER**3)/3.+YCENTR*(YUPPER**2-YLOWER**2)) SET3850
470 WS=VOLSPH*RHOSPH SET3860
AMX(K)=WS SET3870
C *** CHECK WHETHER THE CELL IS FULL SET3880
WSA=TAU(I)*DY(J) SET3890
WSB=WSA-VOLSPH SET3900
IF (ABS(WSB/WSA).LT.ROEPS) GO TO 490 SET3910
C *** ADD RHOOUT MATERIAL TO CELL SET3920
WSB=WSB*RHOOUT SET3930
AMX(K)=WS+WSB SET3940
C *** CHECK WHETHER MASS IS TOO SMALL TO KEEP SET3945
IF(AMX(K)/WSA.LT.EVAP*RHINI) GO TO 510 SET3950
C *** USE A WEIGHTED AVERAGE OF THE PROPERTIES OF THE SPHERE SET3960
AND THE PROJECTILE FOR CELLS PARTIALLY IN THE SPHERE. SET3965
AIX(K)=(WS*SIESPH+WSB*PROJI)/AMX(K) SET3970
V(K)=(WS*VINSPH+WSB*VINI)/AMX(K) SET3980
GO TO 500 SET3990
C *** ESSENTIALLY ALL OF CELL IS IN SPHERE SET4030
490 AIX(K)=SIESPH SET4040
V(K)=VINSPH SET4050
C *** SUM SPHERE VOLUME SET4060
500 TOTSPH=TOTSPH+VOLSPH SET4070
GO TO 520 SET4080
510 AMX(K)=0. SET4090
C *** END OF J-LOOP SET4100
520 K=K+IMAX SET4110
C *** END OF I-LOOP SET4120
530 CONTINUE SET4130
540 WRITE (6,800) RHOSPH,RHINI,RHINIT,RHOFIL,SIESPH,PROJI,TARGI,VINSPHSET4140
1,VINI,TARGV,PROJU,RADIUS,PRYTOP,TAYTOP,YCENTR,PRYBOT,TAYBOT,PRXRT,SET4150
2TAXRT SET4160
C *** RESET BORROWED Z-STORAGE TO ZERO. SET4162
EVAPM = 0. SET4164
EVAPEN = 0. SET4166
EVAPMU = 0. SET4168
EVAPMV = 0. SET4169
C *** M=0 MEANS THE PROJECTILE PACKAGE IS NOT BEING USED. SET4170
IF (M.EQ.0) GO TO 610 SET4220
DO 600 I=M,MR SET4230
K=(MB-1)*IMAX+I+1 SET4240
C *** ASSIGN PROPERTIES TO CELLS IN PROJECTILE. SET4250
DO 590 J=MB,MC SET4260
IF (AMX(K).NE.0.) GO TO 550 SET4270
AMX(K)=RHINI*D(Y(J))*TAU(I) SET4280
C IF (V(K).NE.0.) GO TO 560 SET4290
V(K)=VINI SET4300
560 IF (U(K).NE.0.) GO TO 570 SET4310
U(K)=PROJU SET4320
570 IF (AIX(K).NE.0.) GO TO 580 SET4330
AIX(K)=PROJI SET4340

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580 CONTINUE SET4350
590 K=K+IMAX SET4360
600 CONTINUE SET4370
C     *** MD=0 MEANS THE TARGET PACKAGE IS NOT BEING USED. SET4380
610 IF (MD.EQ.0) GO TO 650 SET4390
C     *** ASSIGN PROPERTIES TO CELLS IN TARGET. SET4395
DO 640 I=MD,ME SET4400
K=(MZ-1)*IMAX+I+1 SET4410
DO 630 J=MZ,N SET4420
IF (V(K).NE.0.) GO TO 620 SET4430
V(K)=TARGV SET4440
IF (AMX(K).NE.0.) GO TO 630 SET4450
AMX(K)=RHINIT*DY(J)*TAU(I) SET4460
620 AIX(K)=TARGI SET4470
630 K=K+IMAX SET4480
640 CONTINUE SET4490
650 CONTINUE SET4500
C CYCLE=0.0 SET4510
DT=0.0 SET4520
NREZ=NUMREZ SET4530
NZ=1 SET4540
C     *** RHOFIL=0. WHEN THERE IS NO FILLER MATERIAL BETWEEN SET4550
C PROJECTILE AND TARGET. SET4560
IF (RHOFIL.EQ.0.) GO TO 680 SET4570
C     *** FILL BETWEEN PACKAGES WITH MATERIAL OF DENSITY=RHOFIL. SET4580
MC=MC+1 SET4590
MZ=MZ-1 SET4600
DO 670 I=1,IMAX SET4610
K=(MC-1)*IMAX+I+1 SET4620
DO 660 J=MC,MZ SET4630
AMX(K)=RHOFIL*DY(J)*TAU(I) SET4640
660 K=K+IMAX SET4650
670 CONTINUE SET4660
680 N3=0 SET4670
C     *** PK(14).GT.0. MEANS SOME CELLS WILL BE DEFINED SET4672
C AFTER PACKAGES ARE SET UP. SET4674
IF (PK(14).GT.0.) CALL CARDS SET4680
C     *** CALCULATE INITIAL VALUE OF TOTAL ENERGY TO BE ADJUSTED SET4682
C WHEN MATERIAL IS EVAPORATED OR CROSSES A TRANSMITTIVE SET4684
C BOUNDARY AND TO BE USED IN EDIT TO CHECK ERROR IN SET4686
C ENERGY SUM. SET4688
DO 690 K=2,KMAX SET4690
ETH=ETH+AMX(K)*( .5*(U(K)**2+V(K)**2)+AIX(K)) SET4700
690 CONTINUE SET4710
XMAX=X(IMAX) SET4720
TXMAX=XMAX*2.0 SET4730
YMAX=Y(JMAX) SET4740
TYMAX=YMAX*2.0 SET4750
700 IF (Y2.GT.(-1.)) GO TO 750 SET4760
C     *** PUT TRACER POINT IN CENTER OF EVERY OTHER NONEMPTY CELL SET4770
C IN EVERY OTHER ROW. THE TRACER POINT COORDINATES OF SET4772
C EMPTY CELLS ARE (0,0). SET4774
II=IMAX/2 SET4780
JJ=JMAX/2 SET4790
DO 720 J=1,JJ SET4800
DO 720 I=1,II SET4810

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K=2*((J-1)*IMAX+I) SET4820
IF (AMX(K).EQ.0.) GO TO 710 SET4830
XP(I,J)=FLOAT(2*I-1)-.5 SET4840
YP(I,J)=FLOAT(2*j-1)-.5 SET4850
NMP=NMP+1 SET4860
710 C *** NMPMAX IS THE MAXIMUM NUMBER OF TRACER POINTS TO SET4862
C BE USED AND IS DEFINED IN THE INPUT DECK. SET4864
IF (NMP.GE.NMPMAX) GO TO 730 SET4870
720 CONTINUE SET4880
GO TO 740 SET4890
730 JJ=J SET4900
C *** N3=1 MEANS TRACER POINTS ARE BEING USED, ADDING SET4902
C ONE MORE RECORD TO EACH TAPE DUMP. SET4904
740 N3=1 SET4910
750 REWIND 7 SET4920
WS=555.0 SET4930
C WRITE OUTPUT FOR OIL ON TAPE. SET4940
WRITE (7) WS,CYCLE,N3 SET4950
WRITE (7) (Z(I),I=1,M2T) SET4960
WRITE (7) (U(I),V(I),AMX(I),AIX(I),P(I),I=1,KMAXA) SET4970
WRITE (7) X(0),(X(I),TAU(I),JPM(I),I=1,IMAX) SET4980
WRITE (7) (Y(I),I=0,JMAX) SET4990
IF (Y2.GT.(-1.)) GO TO 760 SET5000
WRITE (7) ((XP(I,J),YP(I,J),I=1,II),J=1,JJ) SET5010
760 WRITE (7) (DX(I),I=1,IMAX) SET5020
WRITE (7) (DY(J),J=1,JMAX) SET5030
WS=666.0 SET5040
WRITE (7) WS,WS,WS SET5050
GO TO 780 SET5060
C *** DX AND/OR DY ARRAY NOT PROPERLY DEFINED. SET5062
C CHECK VALUE OF DXF AND DYF IF ZONE'S ARE CONSTANT. SET5064
C IF VARIABLE, CHECK LOCATION NUMBERS USED FOR SET5065
C READING IN X AND/OR Y ARRAY ESPECIALLY IF ANY SET5066
C VARIABLE DIMENSIONS WERE CHANGED. SET5068
770 NK=95 SET5070
NR=2 SET5080
CALL ERROR SET5090
780 RETURN SET5100
C
790 FORMAT (/5X,15HINPUT YCENTR = ,1PE12.6,6X,18HADJUSTED YCENTR = ,1PSET5120
1E12.6) SET5130
800 FORMAT (///17X,18HINITIAL CONDITIONS//11X,6HSHERE,13X,9HPACKAGE SET5140
11,21H PACKAGE 2 FILLER//8H DENSITY,1P1E12.4,6X,1P3E12.4/8H S,SET5150
2I.E.,1P1E12.4,6X,1P2E12.4/8H V,1P1E12.4,6X,1P2E12.4/8H SET5160
3 U,13X,1P1E12.4/8H RADIUS,1P1E12.4,5X,3HTOP,1P1E10.4,1P1E12.4/8H SET5170
4YCENTER,1P1E12.4,2X,6HBOTTOM,1P1E10.4,1P1E12.4/23X,5HRIGHT,1P1E10,SET5180
54,1P1E12.4) SET5190
END SET5200-

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SUBROUTINE CDT
 CDT 10
 CDT 20
 CDT 30
 CDT 40
 CDT 50
 CDT 60
 CDT 70
 CDT 80
 CDT 90
 CDT 100
 CDT 110
 CDT 120
 CDT 130
 CDT 140
 CDT 150
 CDT 160
 CDT 170
 CDT 180
 CDT 190
 CDT 200
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 CDT 220
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 CDT 420
 CDT 430
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 CDT 450
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 CDT 470
 CDT 480
 CDT 490
 CDT 500
 CDT 510
 CDT 520
 CDT 530
 CDT 540
 CDT 550
 CDT 560
 CDT 570
 CDT 580

DIMENSION AMX(2502),AIX(2502),U(2502) ,V(2502) ,P(2502) ,
 1 X(52) ,XX(54) ,TAU(52) ,JPM(52) ,
 2 Y(102) ,YY(104) ,FLEFT(102), YAMC(102), SIGC(102),
 3 GAMC(102),
 4 PK(15), Z(150) ,
 5 XP(26,51),YP(26,51),
 6 PL(204) ,UL(204) ,PR(204) ,
 7 RSN(52), RST(52),
 8 CMXP(5) ,CMYP(5) ,IJ(5) ,JK(5) ,
 9 DX(52) ,DDX(54) ,DY(102) ,DDY(104) ,
 S SNB(52) ,STB(52) ,UK(52,3) ,VK(52,3) ,RHO(52,3)

*** DIMENSIONED ARRAYS
 *** Z-BLOCK IS SAVED ON TAPE.

COMMON Z
 COMMON PK
 COMMON YY, XX
 COMMON DDX, DDY
 COMMON AMX, AIX, U, V, P
 COMMON TAU, JPM
 COMMON UL, PL
 COMMON XP, YP, CMXP, CMYP

*** NON-DIMENSIONED VARIABLES

COMMON AID ,AMMV ,AMMY ,AMPY ,AMUR ,AMUT ,AMVR ,
 1AMVT ,DELEB ,DELER ,DELET ,DELM ,DTODX ,DXYMIN ,EAMMP ,EAMPY ,
 2E ,ERDUMP ,I ,I3 ,IWS ,J ,K ,KA ,KB ,
 3LL ,MD ,ME ,MZT ,NERR ,NK ,NPRINT ,
 4NR ,NRZ ,NULLE ,PIOTS ,SIEMIN ,SNR ,SNT ,STR ,SOLID ,
 5SUM ,TESTRH ,TWOPI ,URR ,WS ,WSA ,WSB ,WSC ,WFLAGF ,
 6WFLAGL ,WFLAGP

*** THE FOLLOWING EQUIVALENCES MAKE AVAILABLE
 X(0), Y(0), DX(0), DY(0)

EQUIVALENCE (XX(2), X(1)), (YY(2), Y(1))
 EQUIVALENCE (DDX(2), DX(1)), (DDY(2), DY(1))

*** SPECIAL EQUIVALENCES FOR PH2 ONLY.

EQUIVALENCE (UL,FLEFT), (UL(103),YAMC),
 1 (PL,GAMC,PR), (PL(103),SIGC)

*** SPECIAL EQUIVALENCES FOR PH3 ONLY

EQUIVALENCE (UL,RSN),
 1 (PL,RST), (P,UK),
 2 (P(157),VK), (P(313),SNB),
 3 (P(365),STB), (P(417),RHO)

*** SPECIAL EQUIVALENCES FOR EDIT

EQUIVALENCE (PR(1), IJ), (PR(6), JK)

*** Z-STORAGE EQUIVALENCES

EQUIVALENCE (Z(1),PROB),(Z(2),CYCLE)

1(Z(3),DT),(Z(4),NUMSP),(Z(5),NFRELP),(Z(6),NDUMP7), CDT 590
 2(Z(7),ICSTOP),(Z(8),PIDY),(Z(9),TOPMU),(Z(10),RTMU), CDT 600
 3(Z(11),STK1),(Z(12),NUMREZ),(Z(13),ETH),(Z(14),UN14), CDT 610
 4(Z(15),RHINIT),(Z(16),PPOJI),(Z(17),UN17),(Z(18),XMAX), CDT 620
 5(Z(19),NZ),(Z(20),NREZ),(Z(21),AMDM),(Z(22),UVMAX), CDT 630
 6(Z(23),UN23),(Z(24),DMIN),(Z(25),JSTR),(Z(26),DTNA), CDT 640
 7(Z(27),CVIS),(Z(28),STK2),(Z(29),STEZ),(Z(30),NC), CDT 650
 8(Z(31),UN31),(Z(32),NRC),(Z(33),IMAX),(Z(34),IMAXA), CDT 660
 9(Z(35),JMAX),(Z(36),JMAXA),(Z(37),KMAX),(Z(38),KMAXA) CDT 670
 EQUIVALENCE CDT 680
 1(Z(39),BOTM),(Z(40),BOTMV),(Z(41),NUMSPT),(Z(42),CZERO), CDT 690
 2(Z(43),NUMSCA),(Z(44),PRLIM),(Z(45),PRDELT),(Z(46),PRFACT) CDT 700
 EQUIVALENCE CDT 710
 1(Z(47),I1),(Z(48),I2),(Z(49),IPCYCL),(Z(50),TSTOP), CDT 720
 2(Z(51),RH0FIL),(Z(52),TARGV),(Z(53),N3),(Z(54),IVARDY), CDT 730
 3(Z(55),VT),(Z(56),N6),(Z(57),RTM),(Z(58),RTMV), CDT 740
 4(Z(59),UN59),(Z(60),N10),(Z(61),N11),(Z(62),GAMMA), CDT 750
 5(Z(63),TOPM),(Z(64),BOTMU),(Z(65),SN),(Z(66),TOPMV), CDT 760
 6(Z(67),PRYBOT),(Z(68),PRYTOP),(Z(69),PRXRT),(Z(70),CYCPH3), CDT 770
 7(Z(71),REZFCT),(Z(72),TARGI),(Z(73),PROJU),(Z(74),BBOUND), CDT 780
 8(Z(75),EVAP),(Z(76),ECK),(Z(77),NECYCL),(Z(78),II), CDT 790
 9(Z(79),JJ),(Z(80),NMP),(Z(81),Y2),(Z(82),EZPH1) CDT 800
 EQUIVALENCE CDT 810
 1(Z(83),IVARDX),(Z(84),T),(Z(85),NMPMAX),(Z(86),PMIN), CDT 820
 2(Z(87),INTER),(Z(88),TAYBOT),(Z(89),TAYTOP),(Z(90),IEMAP), CDT 830
 3(Z(91),MC),(Z(92),MR),(Z(93),MZ),(Z(94),MB) CDT 840
 EQUIVALENCE CDT 850
 1(Z(95),REZ),(Z(96),NODUMP),(Z(97),UN97),(Z(98),UN98), CDT 860
 2(Z(99),UN99),(Z(100),EVAPM),(Z(101),EVAPEN),(Z(102),EVAPMU), CDT 870
 3(Z(103),EVAPMV),(Z(104),EZPH2),(Z(105),SNL),(Z(106),STL), CDT 880
 4(Z(107),TAXRT),(Z(108),IDNMAP),(Z(109),IPRMAP),(Z(110),ROEPS), CDT 890
 5(Z(111),RHINI),(Z(112),VINI),(Z(113),FINAL),(Z(114),IVMAP), CDT 900
 6(Z(115),RHOZ),(Z(116),ESA),(Z(117),ESEZ),(Z(118),ESB), CDT 910
 7(Z(119),ESCAPA),(Z(120),ESESP),(Z(121),ESESQ),(Z(122),ESES), CDT 920
 8(Z(123),ESALPH),(Z(124),ESBETA),(Z(125),ESCAPB),(Z(126),IUMAP), CDT 930
 9(Z(127),SS1),(Z(128),SS2),(Z(129),UMIN),(Z(130),SS4) CDT 940
 EQUIVALENCE CDT 950
 1(Z(131),PRTIME),(Z(132),EOR),(Z(133),EOT),(Z(134),ECB), CDT 960
 2(Z(135),EMOR),(Z(136),DXF),(Z(137),DYF),(Z(138),RHOMIN), CDT 970
 3(Z(139),STAB),(Z(140),XIENRG),(Z(141),XKENRG),(Z(142),XTENRG), CDT 980
 4(Z(143),STT),(Z(144),DTMIN),(Z(145),TRNSFC),(Z(146),EMOT), CDT 990
 5(Z(147),JPROJ),(Z(148),CNAUT),(Z(149),BBAR),(Z(150),EMOB) CDT1000
 CDT1010
 CDT1020
 CDT1030
 END OF COMMON CDT1040
 CDT1050
 CDT1060
 CDT1070
 *** SPECIAL EQUIV FOR ES AND CDT CDT1080
 EQUIVALENCE (RHOW,NULLE) CDT1090
 CDT1100
 ***CHECK COURANT CONDITION AND PARTICLE VELOCITY. CDT1110
 ***RECORD I AND J OF ZONE WHERE DT IS CONTROLLED. CDT1120
 ***FIRST CALCULATE PRESSURES FROM EQ. OF ST. CDT1130
 CDT1140
 CDT1220

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10 TRIAL=0. CDT1230
    SRATIO=10.**10 CDT1240
C           **WSC WILL BE MAXIMUM U OR V CDT1250
    WSC=0. CDT1260
    DO 60 I=1,I1 CDT1270
    K=I+1 CDT1280
    DO 60 J=1,I2 CDT1290
    RHOW=AMX(K)/(TAU(I)*DY(J)) CDT1330
    CALL ES CDT1340
C           *** IF DENSITY OF CELL K IS LESS THAN RHOMIN, IT'S CDT1342
C           VELOCITY OR SOUND SPEED IS NOT USED IN DETERMINING DT. CDT1344
    IF (RHOW.LT.RHOMIN) GO TO 601 CDT1350
    IF (ABS(P(K)).LT.PMIN) P(1)=0. CDT1360
    IF (CNAUT.GT.0.) GO TO 20 CDT1370
C           ***CALCULATE SOUND SPEED FOR POLYTOPIC GAS WITH CDT1380
C           ***GAMMA EQUAL TO ESA+1. CDT1390
    WS=SQRT(GAMMA*ABS(P(K))/RHOW) CDT1400
    GO TO 40 CDT1410
C           ***CHECK FOR NEGATIVE PRESSURE. CDT1420
20 IF (P(K).GT.0.) GO TO 30 CDT1430
C           *** NEGATIVE PRESSURES NOT ALLOWED ALONG GRID BOUNDARY CDT1440
C           AND NOT ALLOWED ANYWHERE UNTIL ACTIVE GRID REACHES CDT1450
C           JSTR(INPUT PARAMETER FOR TURNING ON STRENGTH CDT1452
C           CALCULATIONS). CDT1454
    IF ((IMAX.NE.1.AND.I.EQ.IMAX).OR.J.EQ.JMAX.OR.I2.LT.JSTR) P(K)=0. CDT1456
C           ***PRESSURE IS NEGATIVE OR ZERO CDT1458
    WS=CNAUT CDT1460
    GO TO 40 CDT1470
C           ***PRESSURE IS POSITIVE. CDT1480
30 WS=CNAUT+BBAR*SQRT(P(K)) CDT1490
    WSA=SQRT(GAMMA*P(K)/RHOW) CDT1500
    WS=AMAX1(WS,WSA) CDT1510
C           *** WS IS SOUND SPEED OF CELL K. CDT1520
    *** WSB IS MAXIMUM OF RADIAL AND AXIAL VELOCITY OF CELL K. CDT1530
    *** WSC STORES MAXIMUM VELOCITY OF CELLS USED TO DETERMINE CDT1540
C           DT. PRINTED AS MAXUV. CDT1556
    WSB=AMAX1(ABS(U(K)),ABS(V(K))) CDT1558
    WSC=AMAX1(WSC,WSB) CDT1560
    WS=AMAX1(WS,WSB) CDT1570
C           *** TRIAL STORES MAXIMUM OF VELOCITY AND SOUND SPEED USED CDT1580
C           TO DETERMINE DT. PRINTED AS MAXCUV. CDT1582
    IF (WS.LE.TRIAL) GO TO 50 CDT1584
    TRIAL=WS CDT1590
50 IF (WS.LE.0.) GO TO 60 CDT1600
    DXYMIN=AMIN1(DX(I),DY(J)) CDT1610
    RATIO=DXYMIN/WS CDT1620
    IF (RATIO.GT.SRATIO) GO TO 60 CDT1630
C           *** I AND J OF CELL CONTROLLING DT STORED IN N10 AND N11 CDT1640
C           FOR PRINTOUT. CDT1642
    N10=I CDT1644
    N11=J CDT1650
C           *** SRATIO IS SMALLEST VALUE CALCULATED FOR RATIO. CDT1660
    SRATIO=RATIO CDT1665

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DTNA=DT          CDT2170
C   *** TESTRH = .2*RHOZ CDT2171
C   THE PRESSURE OF COLD, FREE SURFACE CELLS IS REDUCED BY ACDT2172
C   FACTOR, F, WHICH ACCOUNTS FOR THE EFFECT OF FREE SURFACECDT2173
C   LOCATION ON THE PRESSURE GRADIENT. F IS THE DENSITY OF CDT2174
C   THE LOWEST DENSITY ADJACENT CELL DIVIDED BY THE NORMAL CDT2175
C   DENSITY, OR F IS TESTRH = WHICHEVER IS SMALLEST CDT2176
C
WT=TESTRH        CDT2180
DO 140 I=1,I1    CDT2190
K=I+1            CDT2200
DO 140 J=1,I2    CDT2210
RHOW=AMX(K)/(DY(J)*TAU(I)) CDT2220
WTB=WT           CDT2230
IF (AIX(K).GE.ESESQ) GO TO 140 CDT2240
IF (RHOW.LT.SOLID) GO TO 140 CDT2250
IF (I.EQ.IMAX) GO TO 100 CDT2260
WTA=AMX(K+1)/(DY(J)*TAU(I+1)) CDT2270
IF (WTA.LT.WT) WTB=WTA CDT2280
100 IF (I.EQ.1) GO TO 110 CDT2290
WTA=AMX(K-1)/(DY(J)*TAU(I-1)) CDT2300
IF (WTA.LT.WTB) WTB=WTA CDT2310
110 IF (J.EQ.JMAX) GO TO 120 CDT2320
KA=K+IMAX        CDT2330
WTA=AMX(KA)/(DY(J+1)*TAU(I)) CDT2340
IF (WTA.LT.WTB) WTB=WTA CDT2350
120 IF (J.EQ.1) GO TO 130 CDT2360
KB=K-IMAX        CDT2370
WTA=AMX(KB)/(DY(J-1)*TAU(I)) CDT2380
IF (WTA.LT.WTB) WTB=WTA CDT2390
130 IF (WTB.LT.WT) P(K)=P(K)*WTB/RHOZ CDT2400
140 K=K+IMAX        CDT2410
GO TO 190         CDT2420
C
C   *** DT TOO SMALL CDT2430
150 NK=75          CDT2440
GO TO 180         CDT2450
C
C   *** T IS NEGATIVE CDT2460
160 NK=95          CDT2470
GO TO 180         CDT2480
C
C   *** DT WILL BE NEGATIVE OR ZERO. CDT2490
170 NK=65          CDT2500
GO TO 180         CDT2510
180 NR=3           CDT2520
CALL ERROR        CDT2530
C
C   ***FIND THE MAXIMUM PRESSURE ON EACH COLUMN AND CDT2540
C   ***STORE ITS CELL NUMBER AS JPM. THIS WILL BE USED CDT2550
C   ***IN DETERMINING THE REGION IN WHICH PHASE 3 IS CDT2560
C   ***USED. WSA WILL BE A RUNNING MAXIMUM OF THE CDT2570
C   ***PRESSURE IN THE GRID. CDT2580
190 WSA=-1.E30      CDT2590
DO 260 I=1,I1      CDT2600
C
C   *** WS WILL BE LOCAL MAXIMUM OF COLUMN I. CDT2610
WS=-1.E30          CDT2620
K=(I2-1)*IMAX+I+1 CDT2630
JP=I2              CDT2640
JINTL=1            CDT2650

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C           *** START AT TOP OF COLUMN AND LOOK FOR PRESSURE PEAK.      CDT2665
200 DO 210 J=JINTL,I2                                              CDT2670
      IF (P(K).LT.WS) GO TO 220                                     CDT2680
      WS=P(K)                                                       CDT2690
C           *** JP IS J-INDEX OF CELL WITH PEAK PRESSURE.          CDT2695
      JP=JP-1                                                       CDT2700
210 K=K-IMAX                                                       CDT2710
C           *** IF YOU FALL THROUGH, THEN THERE WAS NO MAXIMUM IN THIS CDT2720
C           COLUMN                                                 CDT2730
      GO TO 250                                                       CDT2740
C
C           *** COME HERE IF PRESSURE HAS PASSED A LOCAL MAXIMUM      CDT2750
C           *** PTEMP IS PEAK PRESSURE OF COLUMN I.                  CDT2760
220 PTEMP=P(K+IMAX)                                              CDT2770
      IF (PTEMP.LT.WSA) GO TO 230                                 CDT2780
C           *** WSA WILL BE PEAK PRESSURE IN ACTIVE GRID (ABSOLUTE CDT2790
C           MAXIMUM).                                         CDT2800
      WSA=PTEMP                                                       CDT2810
      GO TO 240                                                       CDT2820
C
C           *** PTEMP IS LOCAL MAXIMUM BUT IS LESS THAN ABSOLUTE      CDT2830
C           MAXIMUM                                                 CDT2840
230 IF (PTEMP.GT.0.3*WSA) GO TO 240                               CDT2850
C
C           *** THIS LOCAL MAXIMUM IS NOT BIG ENOUGH TO USE FOR JPM   CDT2860
C
      JINTL=J+1                                                       CDT2870
C
C           JP=JP-1                                                       CDT2880
C           *** WE MAY HAVE REACHED BOTTOM OF COLUMN                 CDT2890
      IF (JINTL.GE.I2) GO TO 250                                 CDT2900
C           *** CONTINUE DOWN COLUMN SEARCHING FOR SUFFICIENTLY LARGE CDT2910
C           LOCAL MAXIMUM.                                         CDT2930
      WS=P(K)                                                       CDT2940
      K=K-IMAX                                                       CDT2945
      GO TO 200                                                       CDT2950
C           *** IF POSITION OF PEAK PRESSURE IN COLUMN I DOES NOT CDT2952
C           ADVANCE FROM ONE CYCLE TO THE NEXT, DO NOT CHANGE CDT2954
C           VALUE OF JPM.                                         CDT2960
240 JP=JP+1                                                       CDT2970
      IF (JP.LE.JPM(I)) GO TO 260                               CDT2980
      JPM(I)=JP
C
C           ***IF JPM IS ZERO THE SHOCK HAS NEVER REACHED THIS      CDT3030
C           ***LOCATION. IF IT IS NONZERO THE SHOCK HAS PASSED      CDT3040
C           ***AND WE MUST CONTINUE TO INCREASE I UNTIL THE        CDT3050
C           ***RIGHT BOUNDARY OF THE SHOCK IS REACHED.            CDT3060
250 IF (JPM(I).LE.0) GO TO 270                                 CDT3070
C           *** END OF I LOOP.                                     CDT3075
260 CONTINUE
C           *** IF PEAK PRESSURE OF COLUMN I HAS GONE BELOW A THIRD CDT3090
C           THE GRID MAXIMUM, AND IF JPM(I)=0. FROM THE PREVIOUS CDT3100
C           CYCLE, WE HAVE REACHED THE RIGHT EDGE OF THE SHOCK.    CDT3110
270 CONTINUE
C           *** JPM(I) MUST BE MONOTONIC DECREASING               CDT3130
      K=I1-1                                                       CDT3140
                                                               CDT3150

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DO 280 IWS=1,K CDT3160
I=I1-IWS CDT3170
280 IF (JPM(I).LT.JPM(I+1)) JPM(I)=JPM(I+1) CDT3180
RETURN CDT3190
C CDT3200
290 FORMAT (/4H CDT,I3,I4,4H T=,1PE13.7,5H DT=,1PE13.7,9H MAXCUV=,1CDT3210
1PE13.7,8H MAXUV=,1PE13.7,7H UMIN=,1PE13.7,7H PMIN=,1PE13.7) CDT3220
END CDT3230-

SUBROUTINE ES ES 10

..... ES 20

..... ES 30

DIMENSION AMX(2502),AIX(2502),U(2502) ,V(2502) ,P(2502) , ES 40

1 X(52) ,XX(54) ,TAU(52) ,JPM(52) , ES 50

2 Y(102) ,YY(104) ,FLEFT(102),YAMC(102),SIGC(102), ES 60

3 GAMC(102). ES 70

4 PK(15), Z(150) , ES 80

5 XP(26,51),YP(26,51), ES 90

6 PL(204) ,UL(204) ,PR(204) , ES 100

7 RSN(52), RST(52), ES 110

8 CMXP(5) ,CMYP(5) ,IJ(5) ,JK(5) , ES 120

9 DX(52) ,DDX(54) ,DY(102) ,DDY(104) , ES 130

\$ SNB(52) ,STB(52) ,UK(52,3) ,VK(52,3) ,RHO(52,3) ES 140

*** DIMENSIONED ARRAYS ES 150

*** Z-BLOCK IS SAVED ON TAPE. ES 160

COMMON Z ES 170

COMMON PK ES 180

COMMON YY, XX ES 190

COMMON DDX, DDY ES 200

COMMON AMX, AIX, U, V, P ES 210

COMMON TAU, JPM ES 220

COMMON UL, PL ES 230

COMMON XP, YP, CMXP, CMYP ES 240

*** NON-DIMENSIONED VARIABLES ES 250

COMMON AID, AMMV, AMMY, AMPY, AMUR, AMUT, AMVR, ES 260

1AMVT, DELEB, DELER, DELET, DELM, DTODX, XYMIN, EAMMP, EAMPY, ES 270

2E, ERDUMP, I, I3, IWS, J, K, KA, KB, ES 280

3LL, MD, ME, MZT, NERR, NK, NPRINT, ES 290

4NR, NRZ, NULLE, PIDTS, SIEMIN, SNR, SNT, STR, SOLID, ES 300

5SUM, TESTRH, TWOP, URR, WS, WSA, WSB, WSC, WFLAGF, ES 310

6WFLAGL, WFLAGP ES 320

ES 330

*** THE FOLLOWING EQUIVALENCES MAKE AVAILABLE ES 340

X(0), Y(0), DX(0), DY(0) ES 350

ES 360

EQUIVALENCE (XX(2), X(1)), (YY(2), Y(1)) ES 370

EQUIVALENCE (DDX(2), DX(1)), (DDY(2), DY(1)) ES 380

ES 390

*** SPECIAL EQUIVALENCES FOR PH2 ONLY ES 400

ES 410

EQUIVALENCE (UL,FLEFT), (UL(103),YAMC), ES 420

1 (PL,GAMC,PR), (PL(103),SIGC) ES 430

ES 440

*** SPECIAL EQUIVALENCES FOR PH3 ONLY ES 450

ES 460

EQUIVALENCE (UL,RSN), (UL,RST), (P,UK), ES 470

1 (PL,RSN), (P,UK), (P(157),VK), (P(313),SN1), ES 480

2 (P(365),STB), (P(417),RHO) ES 490

3 ES 500

ES 510

*** SPECIAL EQUIVALENCES FOR EDIT ES 520

ES 530

EQUIVALENCE (PR(1), IJ), (PR(6), JK) ES 540

ES 550

*** Z-STORAGE EQUIVALENCES ES 560

ES 570

EQUIVALENCE (Z(1),PROB), (Z(2),CYCLE), ES 580

1(Z(3),DT),(Z(4),NUMSP),(Z(5),NFRELP),(Z(6),NDUMP7),	ES 590
2(Z(7),ICSTOP),(Z(8),PIDY),(Z(9),TOPMU),(Z(10),RTMU),	ES 600
3(Z(11),STK1),(Z(12),NUMREZ),(Z(13),ETH),(Z(14),UN14),	ES 610
4(Z(15),RHINIT),(Z(16),PROJI),(Z(17),UN17),(Z(18),XMAX),	ES 620
5(Z(19),NZ),(Z(20),NREZ),(Z(21),AMDM),(Z(22),UVMAX),	ES 630
6(Z(23),UN23),(Z(24),DMIN),(Z(25),JSTR),(Z(26),DTNA),	ES 640
7(Z(27),CVIS),(Z(28),STK2),(Z(29),STEZ),(Z(30),NC),	ES 650
8(Z(31),UN31),(Z(32),NRC),(Z(33),IMAX),(Z(34),IMAXA),	ES 660
9(Z(35),JMAX),(Z(36),JMAXA),(Z(37),KMAX),(Z(38),KMAXA)	ES 670
EQUIVALENCE	
1(Z(39),BOTM),(Z(40),BOTMV),(Z(41),NUMSPT),(Z(42),CZERO),	ES 690
2(Z(43),NUMSCA),(Z(44),PRLIM),(Z(45),PRDELT),(Z(46),PRFACT)	ES 700
EQUIVALENCE	
1(Z(47),I1),(Z(48),I2),(Z(49),IPCYCL),(Z(50),TSTOP),	ES 720
2(Z(51),RHOFIL),(Z(52),TARGV),(Z(53),N3),(Z(54),IVARDY),	ES 730
3(Z(55),VT),(Z(56),N6),(Z(57),RTM),(Z(58),RTMV),	ES 740
4(Z(59),UN59),(Z(60),N10),(Z(61),N11),(Z(62),GAMMA),	ES 750
5(Z(63),TOPM),(Z(64),BOTMU),(Z(65),SN),(Z(66),TOPMV),	ES 760
6(Z(67),PRYBOT),(Z(68),PRYTOP),(Z(69),PRXRT),(Z(70),CYCPH3),	ES 770
7(Z(71),REZFCT),(Z(72),TARGI),(Z(73),PROJU),(Z(74),BBOUND),	ES 780
8(Z(75),EVAP),(Z(76),ECK),(Z(77),NECYCL),(Z(78),II),	ES 790
9(Z(79),JJ),(Z(80),NMP),(Z(81),Y2),(Z(82),EZPH1)	ES 800
EQUIVALENCE	
1(Z(83),IVARDX),(Z(84),T),(Z(85),NMPMAX),(Z(86),PMIN),	ES 820
2(Z(87),INTER),(Z(88),TAYBOT),(Z(89),TAYTOP),(Z(90),IEMAP),	ES 830
3(Z(91),MC),(Z(92),MR),(Z(93),MZ),(Z(94),MB)	ES 840
EQUIVALENCE	
1(Z(95),REZ),(Z(96),NODUMP),(Z(97),UN97),(Z(98),UN98),	ES 860
2(Z(99),UN99),(Z(100),EVAPM),(Z(101),EVAPEN),(Z(102),EVAPMU),	ES 870
3(Z(103),EVAPMV),(Z(104),EZPH2),(Z(105),SNL),(Z(106),STL),	ES 880
4(Z(107),TAXRT),(Z(108),IDNMAP),(Z(109),IPRMAP),(Z(110),ROEPS),	ES 890
5(Z(111),RHINI),(Z(112),VINI),(Z(113),FINAL),(Z(114),IVMAP),	ES 900
6(Z(115),RHOZ),(Z(116),ESA),(Z(117),ESEZ),(Z(118),ESB),	ES 910
7(Z(119),ESCAPA),(Z(120),ESEESP),(Z(121),ESESQ),(Z(122),ESES),	ES 920
8(Z(123),ESALPH),(Z(124),ESBETA),(Z(125),ESCAPB),(Z(126),IUMAP),	ES 930
9(Z(127),SS1),(Z(128),SS2),(Z(129),UMIN),(Z(130),SS4)	ES 940
EQUIVALENCE	
1(Z(131),PRTIME),(Z(132),EOR),(Z(133),EOT),(Z(134),EOB),	ES 960
2(Z(135),EMOR),(Z(136),DXF),(Z(137),DYF),(Z(138),RHOMIN),	ES 970
3(Z(139),STAB),(Z(140),XIENRG),(Z(141),XKENRG),(Z(142),XTENRG),	ES 980
4(Z(143),SIT),(Z(144),DTMIN),(Z(145),TRNSFC),(Z(146),EMOT),	ES 990
5(Z(147),JPROJ),(Z(148),CNAUT),(Z(149),BBAR),(Z(150),EMOB)	ES 1000
	ES 1010
*** SPECIAL EQUIV FOR ES AND CDT	
EQUIVALENCE (RHOW,NULLE)	
.....	ES 1020
.....	ES 1030
END OF COMMON	ES 1040
.....	ES 1050
.....	ES 1060
*** P(K) CALCULATED FROM RHOW AND AIX(K).	ES 1065
RHOW IS CALCULATED IN CDT	ES 1070
IF (ESCAPA.LE.0.) GO TO 30	ES 1110
ETA=RHOW/RHOZ	ES 1120
VOW=1./ETA	ES 1130
IF (AIX(K).LE.0.) GO TO 20	ES 1140

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C     *** P1 AND P4 ARE THERMAL PRESSURE TERMS.          ES 1145
P1=AIX(K)*RHOW*ESA
P4=ESB/(AIX(K)/(ESEZ*ETA**2)+1.)*AIX(K)*RHOW      ES 1150
C     *** P5 IS MECHANICAL PRESSURE TERM               ES 1160
10    P5=ESCAPA*(ETA-1.)                                ES 1165
P2=-1.
C     *** IF MATERIAL IS UNDER-DENSE AND ITS ENERGY IS BETWEEN   ES 1170
C           ESES AND ESESP, A COMBINATION OF THE EXPANDED AND      ES 1180
C           CONDENSED EQUATIONS OF STATE IS USED.                  ES 1182
IF (ETA.GE.1.) GO TO 50                               ES 1184
C     *** ESESP = ENERGY TO VAPORIZATE MATERIAL. MUST EXCEED ESES.  ES 1186
IF (A.X(K).GT.ESESP) GO TO 40                      ES 1190
C     *** ESES = ENERGY TO BRING MATERIAL TO VAPOR TEMPERATURE.  ES 1195
IF (AIX(K).GT.ESES) P2=1.                            ES 1200
C     *** P2=1 MEANS BOTH THE EXPANDED AND COMPRESSED            ES 1205
C           FORMULATIONS WILL BE USED. OTHERWISE, P2=-1.          ES 1210
GO TO 50                                         ES 1212
C     *** WHEN SPECIFIC INTERNAL ENERGY OF CELL IS NEGATIVE,  ES 1214
C           THERMAL PRESSURES ARE SET TO ZERO.                  ES 1220
20    P1=0.                                           ES 1222
P4=0.
C     *** WHEN SPECIFIC INTERNAL ENERGY IS NEGATIVE OR ZERO AND  ES 1224
C           DENSITY IS LESS THAN SOLID, SET PRESSURE TO ZERO.      ES 1230
IF (ETA.LT.AMDM) GO TO 80                          ES 1230
GO TO 10                                         ES 1240
C     *** IDEAL GAS                                     ES 1242
30    P(K)=ESA*RHOW*AIX(K)                         ES 1244
GO TO 90                                         ES 1250
C     *** EXPANDED STATE                           ES 1260
40    P8=(1.-VOW)
P9=EXP(ESALPH*P8)
P12=EXP(-ESBETA*P8**2)
P(K)=P1+(P4+P5*P9)*P12
IF (P2.LT.0.) GO TO 70
P1=SS1*(AIX(K)-ESES)
P(K)=P1*P(K)+(1.-P1)*P3
GO TO 70                                         ES 1265
C     *** CONDENSED STATE                         ES 1270
C     P6 IS MECHANICAL PRESSURE TERM...          ES 1280
50    P6=ESCAPB*(ETA-1.)*2
P(K)=P1+P4+P5+P6
IF (P2.LT.0.) GO TO 60
C     *** USING COMBINATION OF CONDENSED AND EXPANDED EQUATIONS  ES 1290
C           OF STATE.
IF (P(K).LT.0.) P(K)=0.
P3=P(K)
GO TO 40                                         ES 1300
C     *** USING CONDENSED EQUATION OF STATE        ES 1310
60    IF (P(K).GE.0.) GO TO 90
C     *** IF MATERIAL IS EXPANDED OR J-INDEX OF CELL IS LESS      ES 1320
C           THAN N6, SET NEGATIVE PRESSURE TO ZERO. (N6 IS INPUT      ES 1330
C           PARAMETER)
IF (J.LE.N6.OR.ETA.LE.AMDM) GO TO 80
GO TO 90                                         ES 1340
C     *** SET NEGATIVE PRESSURES TO ZERO WHEN USING COMBINED      ES 1350
C           OR EXPANDED EQUATIONS OF STATE.                      ES 1360
70    IF (P(K).GE.0.) GO TO 90

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80 P(K)=0.
90 RETURN
END

ES 1490
ES 1500
ES 1510-

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SUBROUTINE EDIT ..... 10
***** ..... 20
DIMENSION AMX(2502),AIX(2502),U(2502) ,V(2502) ,P(2502) , 40
1 X(52) :XX(54) ,TAU(52) ,JPM(52) ,CRAD(52), 50
2 Y(102) ,YY(104) ,FLEFT(102),YAMC(102),SIGC(102), 60
3 GAMC(102), 70
4 PK(15), Z(150) , 80
5 XP(26,51),YP(26,51), 90
6 PL(204) ,UL(204) ,PR(204) , 100
7 RSN(52), RST(52), 110
8 CMXP(5) ,CMYP(5) ,IJ(5) ,JK(5) , 120
9 DX(52) ,DDX(54) ,DY(102) ,DDY(104) , 130
$ SNB(52) ,STB(52) ,UK(52,3) ,VK(52,3) ,RH0(52,3) 140
*** DIMENSIONED ARRAYS 150
*** Z-BLOCK IS SAVED ON TAPE. 160
COMMON Z 170
COMMON PK 180
COMMON YY, XX 190
COMMON DDX, DDY 200
COMMON AMX, AIX, U, V, P 210
COMMON TAU, JPM 220
COMMON UL, PL 230
COMMON XP, YP, CMXP, CMYP 240
*** NON-DIMENSIONED VARIABLES 250
COMMON AID,AMMV,AMMY,AMPY,AMUR,AMUT,AMVR, 260
1AMVT,DELEB,DELER,DELET,DELM,DTODX,DXYMIN,EAMMP,EAMPY, 270
2E,ERDUMP,I,I3,IWS,J,K,KA,KB, 280
3LL,MD,ME,MZT,NERR,NK,NPRINT, 290
4NR,NRZ,NULLE,PIDTS,SIEMIN,SNR,SINT,STR,SOLID, 300
5SUM,TESTRH,TWOP,URR,WS,WSA,WSB,WSC,WFLAGF, 310
6WFLAGL,WFLAGP 320
*** THE FOLLOWING EQUIVALENCES MAKE AVAILABLE 330
X(0), Y(0), DX(0), DY(0) 340
EQUIVALENCE (XX(2), X(1)), (YY(2), Y(1)) 350
EQUIVALENCE (DDX(2), DX(1)), (DDY(2), DY(1)) 360
*** SPECIAL EQUIVALENCES FOR PH2 ONLY 370
EQUIVALENCE (UL,FLEFT), (UL(103),YAMC), 400
1 (PL,GAMC,PR), (PL(103),SIGC) 410
*** SPECIAL EQUIVALENCES FOR PH3 ONLY 420
EQUIVALENCE (UL,RSN), 430
1 (PL,RST), (P,UK), 440
2 (P(157),VK), (P(313),SNB), 450
3 (P(365),STB), (P(417),RH0) 460
*** SPECIAL EQUIVALENCES FOR EDIT 470
EQUIVALENCE (PR(1), IJ), (PR(6), JK), (UL(103),CRAD) 480
*** Z-STORAGE EQUIVALENCES 490
EQUIVALENCE (Z( 1),PROB ),(Z( 2),CYCLE ), 500
58.

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1(Z(3),DT),(Z(4),NUMSP),(Z(5),NFRELP),(Z(6),NDUMP7),	590	
2(Z(7),ICSTOP),(Z(8),PIDY),(Z(9),TOPMU),(Z(10),RTMU),	600	
3(Z(11),STK1),(Z(12),NUMREZ),(Z(13),ETH),(Z(14),UN14),	610	
4(Z(15),RHINIT),(Z(16),PROJI),(Z(17),UN17),(Z(18),XMAX),	620	
5(Z(19),NZ),(Z(20),NREZ),(Z(21),AMDM),(Z(22),UVMAX),	630	
6(Z(23),UN23),(Z(24),DMIN),(Z(25),JSTR),(Z(26),DTNA),	640	
7(Z(27),CVIS),(Z(28),STK2),(Z(29),STEZ),(Z(30),NC),	650	
8(Z(31),UN31),(Z(32),NRC),(Z(33),IMAX),(Z(34),IMAXA),	660	
9(Z(35),JMAX),(Z(36),JMAXA),(Z(37),KMAX),(Z(38),KMAXA)	670	
EQUIVALENCE	680	
1(Z(39),BOTM),(Z(40),BOTMV),(Z(41),NUMSPT),(Z(42),CZERO),	690	
2(Z(43),NUMSCA),(Z(44),PRLIM),(Z(45),PRDELT),(Z(46),PRFACT)	700	
EQUIVALENCE	710	
1(Z(47),I1),(Z(48),I2),(Z(49),IPCYCL),(Z(50),TSTOP),	720	
2(Z(51),RHOFIL),(Z(52),TARGV),(Z(53),N3),(Z(54),IVARDY),	730	
3(Z(55),VT),(Z(56),N6),(Z(57),RTM),(Z(58),RTMV),	740	
4(Z(59),UN59),(Z(60),N10),(Z(61),N11),(Z(62),GAMMA),	750	
5(Z(63),TOPM),(Z(64),BOTMU),(Z(65),SN),(Z(66),TOPMV),	760	
6(Z(67),PRYBOT),(Z(68),PRYTOP),(Z(69),PRXRT),(Z(70),CYCPH3),	770	
7(Z(71),REZFCT),(Z(72),TARGI),(Z(73),PROJU),(Z(74),BBOUND),	780	
8(Z(75),EVAP),(Z(76),ECK),(Z(77),NECYCL),(Z(78),II),	790	
9(Z(79),JJ),(Z(80),NMP),(Z(81),Y2),(Z(82),EZPH1)	800	
EQUIVALENCE	810	
1(Z(83),IVARDX),(Z(84),T),(Z(85),NMPMAX),(Z(86),PMIN),	820	
2(Z(87),INTER),(Z(88),TAYBOT),(Z(89),TAYTOP),(Z(90),IEMAP),	830	
3(Z(91),MC),(Z(92),MR),(Z(93),MZ),(Z(94),MB)	840	
EQUIVALENCE	850	
1(Z(95),REZ),(Z(96),NODUMP),(Z(97),UN97),(Z(98),UN98),	860	
2(Z(99),UN99),(Z(100),EVAPM),(Z(101),EVAPEN),(Z(102),EVAPMU),	870	
3(Z(103),EVAPMV),(Z(104),EZPH2),(Z(105),SNL),(Z(106),STL),	880	
4(Z(107),TAXRT),(Z(108),IDNMAP),(Z(109),IPRMAP),(Z(110),ROEPS),	890	
5(Z(111),RHINI),(Z(112),VINI),(Z(113),FINAL),(Z(114),IVMAP),	900	
6(Z(115),RHOZ),(Z(116),ESA),(Z(117),ESEZ),(Z(118),ESB),	910	
7(Z(119),ESCAPA),(Z(120),ESESP),(Z(121),ESESQ),(Z(122),ESES),	920	
8(Z(123),ESALPH),(Z(124),ESBETA),(Z(125),ESCAPB),(Z(126),IUMAP),	930	
9(Z(127),SS1),(Z(128),SS2),(Z(129),UMIN),(Z(130),SS4)	940	
EQUIVALENCE	950	
1(Z(131),PRTIME),(Z(132),EOR),(Z(133),EOT),(Z(134),EOB),	960	
2(Z(135),EMOR),(Z(136),DXF),(Z(137),DYF),(Z(138),RHOMIN),	970	
3(Z(139),STAB),(Z(140),XIENRG),(Z(141),XKENRG),(Z(142),XTENRG),	980	
4(Z(143),STT),(Z(144),DTMIN),(Z(145),TRNSFC),(Z(146),EMOT),	990	
5(Z(147),JPROJ),(Z(148),CNAUT),(Z(149),BBAR),(Z(150),EMOB)	1000	
C	1010	
C	1020
G	1030
C	END OF COMMON	1040
C	1050
C	1060
C	1070
***: SPECIAL EQUIV. FOR EDIT		1080
EQUIVALENCE (PR(1),TIETAR),(PR(2),TKETAR),(PR(3),TETAR),	1090	
1 (PR(4),TARMAS),(PR(5),TARMV),(PR(6),TARMVP),	1100	
2 (PR(7),RAMOMA),(PR(8),PRAMOA),(PR(9),TIEPRO),	1110	
3 (PR(10),TKEPRO),(PR(11),TEPRO),(PR(12),PRMAS),	1120	
4 (PR(13),PRMV),(PR(14),PRMVP),(PR(15),RAMOMB),	1130	
5 (PR(16),PRAMOB)	1140	
DIMENSION PROPI(50)	1150	

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C           *** ERDUMP=1. WHEN ERROR CALLS EDIT FOR A TAPE DUMP ONLY    1160
C   IF (ERDUMP.GT.0.) GO TO 150                                         1162
C           *** ENERGY SUM (ESUM) AND RELATIVE ERROR IN SUM (RELERR)    1170
C   COMPUTED. ECK IS LARGEST ERROR COMPUTED AND ON PRINT                1172
C   CYCLES IS PRINTED AND COMPARED TO DMIN, MAXIMUM                   1174
C   ALLOWABLE ERROR.                                                 1176
C   ESUM=0.                                                       1178
C   DO 10 K=2,KMAX                                              1180
10  ESUM=ESUM+AMX(K)*(.5*(U(K)**2+V(K)**2)+AIX(K))                 1190
C   RELERR=(ESUM-ETH)/ETH                                         1200
C   IF (ABS(RELERR).LT.ABS(ECK)) GO TO 20                           1210
C   ECK=RELERR                                              1220
C   NECYCL=NC                                              1230
C   CONTINUE                                              1240
20  C           *** NPRINT = 1 WHEN EDIT IS CALLED TO DO AN INTERMEDIATE 1250
C   PRINT. SKIP TESTS ON TIME TO STOP, PRINT, REZONE, ETC.            1252
C   WHICH ALREADY HAVE BEEN DONE FOR THIS CYCLE.                     1254
C   IF (NPRINT.EQ.1) GO TO 190                                         1256
C   C           *** I3=1 SIGNALS A SHORT PRINT                         1260
C   I3=1                                                       1270
C   C           *** IF THIS IS FIRST CYCLE OF RUN, WFLAGF=1.             1280
C   IF (WFLAGF.GT.0.) GO TO 120                                         1290
C   C           *** IS THIS THE TIME OR CYCLE TO STOP EXECUTION        1300
C   IF (ICSTOP.LE.NC.AND.ICSTOP.GT.0) GO TO 30                         1305
C   IF (T*(1.+ROEPS).GE.TSTOP.AND.TSTOP.GT.0.) GO TO 30               1310
C   C           *** SHOULD THE GRID BE REZONED                         1320
C   IF ((REZ.NE.0..AND.REZFCT.NE.0..AND.NUMREZ.GT.0),OR.SS4.NE.0.) GO 1325
1TO 190                                         1330
C   GO TO 40                                              1340
C   C           *** SET WFLAGL=1. TO SAY THIS IS LAST CYCLE OF RUN 1350
30  WFLAGL=I.                                              1360
C   I3=I1                                              1370
C   NPRINT=1                                              1380
C   NUMSPT=NDUMP7                                         1390
C   NUMSP=0                                              1400
C   GO TO 190                                              1410
40  ASSIGN 140 TO LOCA                                         1420
C   ASSIGN 110 TO LOCB                                         1430
C   C           *** ARE WE PRINTING ON TIME OR CYCLE INTERVALS.       1440
C   IF (PRDELT.NE.0.) GO TO 50                                         1450
C   C           *** NO. BUT WILL NEXT CYCLE BYPASS THE PRINT TIME 1455
45  IF (IPCYCL.NE.0) GO TO 100                                         1460
C   GO TO 430                                              1470
C   C           *** PRINTING ON TIME. IS IT TIME TO PRINT           1480
50  IF (T*(1.+ROEPS).GE.PRTIME) GO TO 70                         1485
C   C           *** NO. BUT WILL NEXT CYCLE BYPASS THE PRINT TIME 1490
C   IF (PRTIME.GE.T+DT) GO TO 60                                         1495
C   DT=PRTIME-T                                         1500
C   DTNA=DT                                              1510
C   GO TO LOCA, (140,130)                                         1520
C   C           *** YES, IT IS TIME TO PRINT. NPRINT=1 FLAGS THIS AS A 1530
C   PRINT CYCLE.                                              1532
70  NPRINT=1                                              1534
C   C           *** AVOID TRUNCATION                                1540
C   T=PRTIME                                              1550
C   C           *** IS IT TIME TO RESCALE PRINT INTERVAL          1560
C   GO TO 190                                              1565

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IF (T*(1.+ROEPS).LT.PRLIM.OR.NUMSCA.LE.0) GO TO 80      1570
    *** CHANGE PRINT INTERVAL AND THE TIME FOR THE NEXT
    RESCALING.                                              1580
C
PRDELT=PRDELT*PRFACT                                     1585
PRLIM=PRLIM*PRFACT                                      1590
NUMSCA=NUMSCA-1                                         1600
C
    *** DEFINE TIME FOR NEXT PRINT.                         1610
80 PRTIME=T+PRDELT                                       1615
IWS=(PRTIME+.5*PRDELT)/PRDELT                           1620
WS=IWS                                                    1630
PRTIME=WS*PRDELT                                         1640
C
    *** WILL WE BYPASS TIME TO PRINT                      1650
    IF (PRTIME.GE.T+DT) GO TO 90                           1655
C
    *** YES, ADJUST DT                                    1660
    DT=PRTIME-T                                           1665
DTNA=DT                                                 1670
90 GO TO LOCB, (110,130)                                 1680
C
    *** PRINTING ON CYCLES. IS THIS A PRINT CYCLE        1690
100 IF (MOD(NC,IPCYCL).NE.0) GO TO LOCA, (140,130)       1695
C
    *** YES. NPRINT = 1 FLAGS THIS AS A PRINT CYCLE.     1700
NPRINT=1                                               1705
C
    *** IS THIS THE CYCLE TO RESCALE PRINT INTERVAL     1710
    IF (NC.LT.PRLIM.OR.NUMSCA.LE.0) GO TO LOCB, (110,130) 1715
C
    *** YES. MULTIPLY NUMBER OF CYCLES BETWEEN PRINTS BY PRFACT 1720
C
1730
IPCYCL=INT(PRFAC)*IPCYCL                               1740
PRLIM=PRFACT*PRLIM                                     1750
NUMSCA=NUMSCA-1                                         1760
GO TO LOCB, (110,130)                                 1770
C
    *** TEST FOR SHORT OR LONG PRINT                     1780
    *** NUMSP COUNTS NUMBER OF SHORT PRINTS SINCE LAST LONG 1790
    PRINT. NUMSPT COUNTS NUMBER OF CYCLES SINCE LAST
    TAPE DUMP.                                            1800
110 NUMSP=NUMSP+1                                         1802
NUMSPT=NUMSPT+1                                         1804
IF (NUMSP.NE.NFRELP) GO TO 190                          1806
NUMSP=0                                                 1810
C
    *** I3=I1 SIGNALS A LONG PRINT                      1820
120 I3=I1                                               1830
C
    *** PRINT OF RESTART CYCLE WILL BE SHORT IF PK(3).LT.-1. 1840
    IF (PK(3).LT.-1..AND.WFLAGF.GT.0.) I3=1             1850
GO TO 190                                               1860
C
    *** CHECK FOR ENERGY DISCREPANCY                   1865
130 IF (ABS(ECK).GT.DMIN) GO TO 440                   1870
C
    *** IF LAST CYCLE, REWIND TAPE                      1880
140 IF (WFLAGL.EQ.0.) GO TO 470                         1890
REWIND 7                                                1900
GO TO 470                                               1910
150 NUMSPT=0                                             1920
IF (NODUMP.NE.0) GO TO 170                            1930
BACKSPACE 7                                           1940
WS=555.0                                               1950
WRITE (7) WS,CYCLE,N3                                1960
WRITE (7) (Z(L),L=1,MZT)                             1970
WRITE (7) (U(K),V(K),AMX(K),AIX(K),P(K),K=1,KMAXA) 1980
WRITE (7) X(0),(X(K),TAU(K),JPM(K),K=1,IMAX)        1990
2000
2010
2020

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C      WRITE (7) (Y(K),K=0,JMAX)          2030
C          *** ARE TRACER POINTS BEING GENERATED 2035
C          IF (Y2.GT.(-1.)) GO TO 160        2040
C              *** YES. WRITE TRACER POINT COORDINATES (XP,YP) ON TAPE. 2045
C              WRITE (7) ((XP(I,J),YP(I,J),I=1,II),J=1,JJ) 2050
160      WRITE (7) (DX(I),I=1,IMAX)        2060
          WRITE (7) (DY(J),J=1,JMAX)        2070
          WS=666.0                         2080
          WRITE (7) WS,WS,WS                2090
          WRITE (6,550) NC                  2100
          IF (WFLAGL.EQ.0.) GO TO 170       2110
          END FILE 7                      2120
170      CONTINUE                         2130
          IF (ERDUMP.GT.0.) CALL EXIT       2140
          GO TO 280                         2150
180      N=2                             2160
          GO TO 220                         2170
C          *** INITIALIZE PR ARRAY, TEMPORARY STORAGE FOR ENERGY,MASS 2172
C          AND MOMENTUM TOTALS PRINTED OUT. 2174
190      DO 200 I=1,16                     2180
200      PR(I)=0.                         2190
C
C      RAMOMA=RADTAL MOMENTUM ABOVE JPROJ 2210
C      RAMOMB=RADTAL MOMENTUM BELOW JPROJ 2220
C      PRAMOA=POSITIVE RADIAL MOMENTUM ABOVE JPROJ 2230
C      PRAMOB=POSITIVE RADIAL MOMENTUM BELOW JPROJ 2240
C
C      IF (JPROJ.EQ.0) GO TO 180           2250
N=IMAX*JPROJ+1
DO 210 K=2,N
WS=AMX(K)
PRMAS=PRMAS+WS
TIEPRO=TIEPRO+WS*AIX(K)
TKEPRO=TKEPRO+.5*WS*(U(K)**2+V(K)**2)
WSA=WS*V(K)
PRMV=PRMV+WSA
IF (WSA.GT.0.) PRMVP=PRMVP+WSA
RAMOMB=RAMOMB+AMX(K)*U(K)
IF (U(K).GT.0.) PRAMOB=PRAMOB+AMX(K)*U(K)
210      CONTINUE                         2380
N=N+1
220      DO 230 K=N,KMAX                 2390
WS=AMX(K)
TARMAS=TARMAS+WS
TIETAR=TIETAR+WS*AIX(K)
TKETAR=TKETAR+.5*WS*(U(K)**2+V(K)**2)
WSA=WS*V(K)
TARMV=TARMV+WSA
IF (WSA.GT.0.) TARMVP=TARMVP+WSA
RAMOMA=RAMOMA+AMX(K)*U(K)
IF (U(K).GT.0.) PRAMOA=PRAMOA+AMX(K)*U(K)
230      CONTINUE                         2490
TETAR=TIETAR+TKETAR
TEPRO=TIEPRO+TKEPRO
DO 240 J=1,8
PR(J+16)=PR(J)+PR(J+8)
240      CONTINUE                         2550

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IF (IMAX.GT.1) GO TO 260                                2560
C
C
C
C
*** IF DOING A 1-D PROBLEM DIVIDE TOTALS BY NZ WHERE    2570
NZ=4***(NUMBER OF TIMES THE GRID HAS BEEN REZONED.)    2580
2585
2590
PROPI(1)=ETH/NZ                                         2600
PROPI(2)=ECK/NZ                                         2610
PROPI(4)=EZPH1/NZ                                       2620
PROPI(5)=EZPH2/NZ                                       2630
PROPI(6)=BBOUND/NZ                                      2640
DO 250 J=1,24                                           2650
250  PROPI(J+6)=PR(J)/NZ                               2660
PROPI(31)=BOTM/NZ                                       2670
PROPI(32)=RTM/NZ                                         2680
PROPI(33)=TOPM/NZ                                       2690
PROPI(34)=EVAPM/NZ                                      2700
PROPI(35)=EMOB/NZ                                       2710
PROPI(36)=EMOR/NZ                                       2720
PROPI(37)=EMOT/NZ                                       2730
PROPI(38)=EVAPEN/NZ                                     2740
PROPI(39)=BOTMU/NZ                                      2750
PROPI(40)=RTMU/NZ                                       2760
PROPI(41)=TOPMU/NZ                                      2770
PROPI(42)=EVAPMU/NZ                                     2780
PROPI(43)=BOTMV/NZ                                      2790
PROPI(44)=RTMV/NZ                                       2800
PROPI(45)=TOPMV/NZ                                      2810
PROPI(46)=EVAPMV/NZ                                     2820
PROPI(47)=EOB/NZ                                         2830
PROPI(48)=EOR/NZ                                         2840
PROPI(49)=EOT/NZ                                         2850
WRITE (6,530) PROB,T,NC,PROPI(1),PROPI(2),NECYCL,(PROPI(J),J=4:6) 2860
WRITE (6,540) (PROPI(J),J=7,49)                           2870
GO TO 270                                               2880
260  WRITE (6,530) PROB,T,NC,ETH,ECK,NECYCL,EZPH1,EZPH2,BBOUND 2890
     WRITE (6,540) ((PR(J),J=1,24),BOTM,RTM,TOPM,EVAPM,EMOB,EMOR,EMOT,E 2900
1VAPEN,BOTMU,RTMU,TOPMU,EVAPMU,BOTMV,RTMV,TOPMV,EVAPMV,EOB,EOR,EOT) 2910
270  WRITE (6,580) (JPM(I),I=1,I1)                         2920
C
C
*** ENERGY TOTALS STORED FOR LATER USE IN TRACER POINT 2930
C
PLOTS.                                                 2935
XIENRG=PR(17)                                         2940
XKENRG=PR(18)                                         2950
XTENRG=PR(19)                                         2960
C
*** IS THIS A TAPE DUMP OR REZONE CYCLE               2965
IF (NUMSPT.EQ.NDUMP7.OR.(REZ.NE.0..AND.REZFCT.NE.0..AND.NUMREZ.GT. ~ 2970
10)) GO TO 150                                         2980
C
*** ARE TRACER POINTS BEING GENERATED                2990
280  IF (Y2.GT.(-1.)) GO TO 305                         3000
C
*** YES, PRINT TRACER POINT COORDINATES IN CM.       3002
WRITE (6,590)                                         3005
N=0
DO 300 J=1,JJ                                         3010
DO 300 I=1,II                                         3020
IF (XP(I,J).LE.0..AND.YP(I,J).LE.0.) GO TO 300        3030
IP=INT(XP(I,J))                                       3040
JP=INT(YP(I,J))                                       3050
KK=JP*IMAX+IP+2                                       3060
                                         3070

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IF (AMX(KK).GT.0.) GO TO 290          3080
XP(I,J)=0.                            3090
YP(I,J)=0.                            3100
GO TO 300                            3110
290 N=N+1                            3120
CMXP(N)=X(IP)+DX(IP+1)*(XP(I,J)-INT(XP(I,J))) 3130
CMYP(N)=Y(JP)+DY(JP+1)*(YP(I,J)-INT(YP(I,J))) 3140
C
C      *** IJ, JK = THE I AND J OF THE CELL THE TRACER POINT 3150
C      ORIGINATED IN . (TRACER POINTS CHANGE POSITION IN 3160
C      XP AND YP ARRAYS WHEN THEY ARE WEDED OUT 3170
C      DURING REZONE.)
C
C      *** IJ, JK = THE I AND J OF THE CELL THE TRACER POINT 3180
C      ORIGINATED IN . (TRACER POINTS CHANGE POSITION IN 3190
C      XP AND YP ARRAYS WHEN THEY ARE WEDED OUT 3200
C
C      *** IJ, JK = THE I AND J OF THE CELL THE TRACER POINT 3210
C      ORIGINATED IN . (TRACER POINTS CHANGE POSITION IN 3220
C      XP AND YP ARRAYS WHEN THEY ARE WEDED OUT 3230
C      DURING REZONE.)
C
C      *** IJ, JK = THE I AND J OF THE CELL THE TRACER POINT 3240
C      ORIGINATED IN . (TRACER POINTS CHANGE POSITION IN 3250
C      XP AND YP ARRAYS WHEN THEY ARE WEDED OUT 3260
C      DURING REZONE.)
C
C      *** IJ, JK = THE I AND J OF THE CELL THE TRACER POINT 3270
C      ORIGINATED IN . (TRACER POINTS CHANGE POSITION IN 3280
C      XP AND YP ARRAYS WHEN THEY ARE WEDED OUT 3290
C      DURING REZONE.)
C
C      *** PRINT SYMBOLIC CONTOUR MAPS OF COMPRESSION, PRESSURE, 3292
C      VELOCITY, AND INTERNAL ENERGY UNLESS DOING A 1-D 3294
C      PROBLEM. 3296
CALL MAP
C      *** COMPUTE CRATER DEPTH AND VOLUME. AID SUMS DEPTH. 3300
AID = 0.                            3310
WRITE(6,490)                         3320
C      *** START AT AXIS 3325
DO 330 I=1,I1
CRAD(I) = .5*DX(I)+X(I-1)
PL(I) = 0.
UL(I) = 0.
DO 320 J=1,I2
K=(J-1)*IMAX + I + 1
C      *** WS IS COMPRESSION 3385
WS = AMX(K)/(TAU(I)*DY(J)*RHOZ)
IF(WS.LT.(.99)) GO TO 310
GO TO 325
310 AID = AID + 1.-WS
C      *** NOT AT BOTTOM OF CRATER YET 3425
320 CONTINUE
325 IAID = INT(AID)
C      *** UL(I) IS CM. DEPTH OF CRATER IN COLUMN I 3442
C      *** PL(I) IS CELL DEPTH OF CRATER IN COLUMN I 3444
UL(I) = Y(IAID) + DY(IAID+1)*(AID-FLOAT(IAID)) - Y(JPROJ)
IF(UL(I).GT.0..OR.UL(I).LT.0.) PL(I) = AID
AID = 0.
330 CONTINUE
C      *** PRINT CRATER DEPTHS 3485
DO 340 I=1,I1
IF(UL(I).LT.0..OR.UL(I).GT.0.) GO TO 335
GO TO 340
335 WRITE(6,495) I, PL(I), CRAD(I), UL(I)
340 CONTINUE
C      *** COMPUTE CRATER VOLUME AND VOLUME OF HEMISPHERE WITH 3530
3532

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C           RADIUS=UL(1). PRINT VOLUMES WHEN THEY ARE POSITIVE.      3534
WSB=0.
DO 345 I=1,I1
IF(UL(I).LT.0.) GO TO 350
C           *** WSB GIVES CRATER VOLUME                         3550
WSB = UL(I)*TAU(I)+WSB
345 CONTINUE
350 CONTINUE
C           *** PRINT CRATER VOLUME ONLY WHEN GREATER THAN ZERO   3560
IF(WSB.GT.0.) GO TO 355
GO TO 360
C           *** WSC GIVES VOLUME OF HEMISPHERE                      3565
355 WSC=2.0944*(UL(1))**3
WRITE(6,500) WSB, WSC
360 CONTINUE
C           *** SHORT PRINT MEAN I3=1 AND PROPERTIES ARE PRINTED ONLY 3570
C           FOR CELLS IN FIRST COLUMN. LONG PRINT MEANS I3=I1 AND    3580
C           PROPERTIES ARE PRINTED FOR ALL CELLS IN ACTIVE GRID.     3590
370 DO 420 I=1,I3
KSPACE=0
WFLAGP=1.
J=I2+1
K=I2*IMAX+I+1
DO 410 L=1,I2
J=J-1
K=K-IMAX
375 IF (AMX(K)) 450,400,380
380 IF (WFLAGP.EQ.0.) GO TO 390
WRITE (6,560) I,X(I),DX(I)
WFLAGP=0.
390 WS=AMX(K)/(TAU(I)*DY(J))
WSA=WS/RHOZ
WSC=P(K)
WRITE (6,520) J,U(K),V(K),WSC,AMX(K),WS,AIX(K),WSA,Y(J)
KSPACE=0
GO TO 410
400 KSPACE=KSPACE+1
IF (KSPACE.GT.1) GO TO 410
WRITE (6,570)
410 CONTINUE
420 CONTINUE
IF (NPRINT.EQ.1) GO TO 130
ASSIGN 130 TO LOCA
ASSIGN 130 TO LOCB
IF (PRDELT.NE.0.) GO TO 50
GO TO 100
C           *** PRINT DELTA NOT SPECIFIED IN INPUT                3960
430 NK=45
GO TO 460
C           *** ENERGY CHECK                                     3970
440 NK=130
GO TO 460
C           *** NEGATIVE MASS                                    3980
450 NK=375
460 NR=5
CALL ERROR
470 WFLAGP=0.

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C      WFLAGF=0.          4080
      *** SHOULD GRID BE REZONED ON THIS CYCLE    4085
      IF ((REZ.NE.0..AND.REZFCT.NE.0..AND.NUMREZ.GT.0).OR.SS4.NE.0.) GO 4090
1 TO 480
      RETURN          4100
480      CALL REZONE          4110
C      *** JUST CALL CDT TO RECALCULATE PRESSURES 4120
      TNOW=T          4130
      DTNOW=DT          4140
      KEZ=0.          4150
      SS4=0.          4160
      CALL CDT          4170
      T=TNOW          4180
      DT=DTNOW          4190
      DTNA=DT          4200
      NUMREZ=NUMREZ-1 4210
C      *** NREZ = NUMBER OF REZONES ALLOWED (INPUT VALUE OF NUMREZ) 4220
C      NUMREZ := NUMBER OF REZONES ALLOWED MINUS THE NUMBER 4230
C      OF REZONES PERFORMED SINCE T=0.          4240
C      NRZ=NREZ-NUMREZ          4250
C      *** NZ USED IN PRINTOUT OF TOTALS FOR 1-D PROBLEMS 4260
C      NZ=4.*NRZ          4270
C      NUMSPT=NDUMP7          4280
      GO TO 120          4285
C      FORMATS          4290
C      4300
C      4310
C      4320
C      4330
C      4340
C      4350
490      FORMAT (1H0,17X,35HDEPTH OF CRATER MEASURED FROM JPROJ//12X,1HI,5X 4360
      1,18H) OF CRATER BOTTOM,12X,1HR,11X,17HDEPTH IN CM. D(I)//) 4370
495      FORMAT (I13,9X,0PF6.1,13X,1PE10.4,9X,1PE10.4)          4380
500      FORMAT (/6X,13HCRATER VOLUME,11X,43HCRATER VOLUME BASED ON (2/3) 4390
      1* PI * D(1)**3/7X,1PE10.4,26X,1PE10.4)          4400
510      FORMAT (5(I4,I4,1P2E9.2))          4410
520      FORMAT (I4,1X,1P2E14.6,3E15.6,E14.6,E15.6,E14.6)          4420
530      FORMAT (8H1PROBLEM,6X,4HTIME,8X,5HCYCLE,3X,13HTOT.EN.THEOR.3X, 4430
      1         19HMAX,REL.ERROR-CYCLE,3X,18HIE SET TO ZERO-PH1,3X, 4440
      2         18HIE SET TO ZERO-PH2,3X,12HPLASTIC-WORK/1F8.4,2X,1PE13.7, 4450
      3         3X,I4,4X,1PE13.7,3X,1PE13.7,1X,I4,6X,1PE13.7,8X,1PE13.7,6X, 4460
      4         1PE13.7/)          4470
540      FORMAT (18X,2HIE,14X,2HKE,7X,13HTOT.EN. (SUM),7X,4HMASS,12X,2HMV,8 4480
      1X,12HMV(POSITIVE),8X,2HMU,8X,12HMU(POSITIVE)/11H J.GT.JPROJ,1P8E15 4490
      2.7/11H J.LE.JPROJ,1P8E15.7/14X,12H-----,3X,12H-----, 4500
      33X,12H-----,3X,12H-----,3X,12H-----,3X,12H-----,3X,12H--- 4510
      4-----,3X,12H-----,3X,12H-----,3X,7H TOTALS,4X,1P 4520
      58E15.7//9H BOUNDARY,9X,6HBOTTOM,9X,5HRIGHT,10X,3HTOP,8X,12H$EVAP0 4530
      6RATED$/9H MASS OUT,2X,1P4E15.7/11H ENERGY OUT,1P4E15.7/7H M$ OUT, 4540
      74X,1P4E15.7/7H MV OUT,4X,1P4E15.7//11H WORK DONE ,1P3E15.7//) 4550
550      FORMAT (1H0//21H TAPE 7 DUMP ON CYCLE15//)          4560
560      FORMAT (1H //4H I =I3,6X,6HR(I) =F12.3,6X,7HDR(I) =E14.7//3H J8X 4570
      1,1HU13X,1HV13X,3H P 12X,3HAMX12X,3HRH011X,3HAIX12X,4HCOMP11X,2H Z/ 4580
      2)          4590
570      FORMAT (1H0)          4600
580      FORMAT (//22H J OF PRESSURE-MAXIMUM/(25I5))          4610
590      FORMAT (//103H TRACER POINTS - INITIAL LOCATION IN CELL COORDINATES

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1 (I,J) - CURRENT LOCATION IN CM. COORDINATES (X,Y)// 5(4H I,3X, 4612
21HJ,5X,1HX,8X,1HY,3X)) 4614
END 4620-

SUBROUTINE MAP

DIMENSION AMX(2502),AIX(2502),U(2502),V(2502),P(2502),
 1 X(52),XX(54),TAU(52),JPM(52),
 2 Y(102),YY(104),FLEFT(102),YAMC(102),SIGC(102),
 3 GAMC(102),
 4 PK(15),Z(150),
 5 XP(26,51),YP(26,51),
 6 PL(204),UL(204),PR(204),
 7 RSN(52),RST(52),
 8 CMXP(5),CMYP(5),IJ(5),JK(5),
 9 DX(52),DDX(54),DY(102),DDY(104),
 \$ SNB(52),STB(52),UK(52,3),VK(52,3),RHO(52,3)

*** DIMENSIONED ARRAYS

*** Z-BLOCK IS SAVED ON TAPE.

COMMON Z
 COMMON PK
 COMMON YY, XX
 COMMON DDX, DDY
 COMMON AMX, AIX, U, V, P
 COMMON TAU, JPM
 COMMON UL, PL
 COMMON AP, YP, CMXP, CMYP

*** NON-DIMENSIONED VARIABLES

COMMON AID,AMMV,AMMY,AMPY,AMUR,AMUT,AMVR,
 1AMVT,DELEB,DELER,DELET,DELM,DTODX,DXYMIN,EAMMP,EAMPY,
 2E,ERDUMP,I,I3,IWS,J,K,KA,KB,
 3LL,MD,ME,MZT,NERR,NK,NPRINT,
 4NR,NRZ,NULLE,PIDTS,SIEMIN,SNR,SNT,STR,SOLID,
 5SUM,TESTRH,TWOP1,UUR,WS,WSA,WSB,WSC,WFLAGF,
 6WFLAGL,WFLAGP

*** THE FOLLOWING EQUIVALENCES MAKE AVAILABLE
 X(0), Y(0), DX(0), DY(0)

EQUIVALENCE (XX(2), X(1)), (YY(2), Y(1))
 EQUIVALENCE (DDX(2), DX(1)), (DDY(2), DY(1))

*** SPECIAL EQUIVALENCES FOR PH2 ONLY

EQUIVALENCE (UL,FLEFT), (UL(103),YAMC),
 1 (PL,GAMC,PR), (PL(103),SIGC)

*** SPECIAL EQUIVALENCES FOR PH3 ONLY

EQUIVALENCE (UL,RSN),
 1 (PL,RST), (P(157),VK), (P(313),SNB),
 2 (P(365),STB), (P(417),RHO),
 3

*** SPECIAL EQUIVALENCES FOR EDIT

EQUIVALENCE (PR(1), IJ), (PR(6), JK)

*** Z-STORAGE EQUIVALENCES

EQUIVALENCE (Z(1),PROB),(Z(2),CYCLE),

1(Z(3),DT),(Z(4),NUMEP),(Z(5),NFRELP),(Z(6),NDUMP7), MAP 590
 2(Z(7),ICSTOP),(Z(8),PIDY),(Z(9),TOPMU),(Z(10),RTMU), MAP 600
 3(Z(11),STK1),(Z(12),NUMREZ),(Z(13),ETH),(Z(14),UN14), MAP 610
 4(Z(15),RHINIT),(Z(16),PROJI),(Z(17),UN17),(Z(18),XMAX), MAP 620
 5(Z(19),NZ),(Z(20),NREZ),(Z(21),AMDM),(Z(22),UVMAX), MAP 630
 6(Z(23),UN23),(Z(24),DMIN),(Z(25),JSTR),(Z(26),DTNA), MAP 640
 7(Z(27),CVIS),(Z(28),STK2),(Z(29),STEZ),(Z(30),NC), MAP 650
 8(Z(31),UN31),(Z(32),NRC),(Z(33),IMAX),(Z(34),IMAXA), MAP 660
 9(Z(35),JMAX),(Z(36),JMAXA),(Z(37),KMAX),(Z(38),KMAXA) MAP 670
 EQUIVALENCE
 1(Z(39),BOTM),(Z(40),BOTMV),(Z(41),NUMSPT),(Z(42),CZERO), MAP 690
 2(Z(43),NUMSCA),(Z(44),PRLIM),(Z(45),PRDELT),(Z(46),PRFACT) MAP 700
 EQUIVALENCE
 1(Z(47),I1),(Z(48),I2),(Z(49),IFCYCL),(Z(50),TSTOP), MAP 720
 2(Z(51),RHOFIL),(Z(52),TARGV),(Z(53),N3),(Z(54),IARDY), MAP 730
 3(Z(55),VT),(Z(56),NG),(Z(57),RTM),(Z(58),RTMV), MAP 740
 4(Z(59),UN59),(Z(60),N10),(Z(61),N11),(Z(62),GAMMA), MAP 750
 5(Z(63),TOPM),(Z(64),BOTMU),(Z(65),SN),(Z(66),TOPMV), MAP 760
 6(Z(67),PRYBOT),(Z(68),PRYTOP),(Z(69),PRXRT),(Z(70),CYCPH3), MAP 770
 7(Z(71),REZFCT),(Z(72),TARG1),(Z(73),PROJU),(Z(74),BBOUND), MAP 780
 8(Z(75),EVAP),(Z(76),ECK),(Z(77),NECYCL),(Z(78),II), MAP 790
 9(Z(79),JJ),(Z(80),NMP),(Z(81),Y2),(Z(82),EZPH1) MAP 800
 EQUIVALENCE
 1(Z(83),VARDX),(Z(84),T),(Z(85),NMPMAX),(Z(86),PMIN), MAP 820
 2(Z(87),INTER),(Z(88),TAYBOT),(Z(89),TAYTOP),(Z(90),IEMAP), MAP 830
 3(Z(91),MC),(Z(92),MR),(Z(93),MZ),(Z(94),MB) MAP 840
 EQUIVALENCE
 1(Z(95),REZ),(Z(96),NODUMP),(Z(97),UN97),(Z(98),UN98), MAP 860
 2(Z(99),UN99),(Z(100),EVAPM),(Z(101),EVAFEN),(Z(102),EVAPMU), MAP 870
 3(Z(103),EVAPMV),(Z(104),EZPH2),(Z(105),SNL),(Z(106),STL), MAP 880
 4(Z(107),TAXRT),(Z(108),IDNMAP),(Z(109),IPRMAP),(Z(110),ROEPS), MAP 890
 5(Z(111),RHINI),(Z(112),VINI),(Z(113),FINAL),(Z(114),IVMAP), MAP 900
 6(Z(115),RHOZ),(Z(116),ESA),(Z(117),ESEZ),(Z(118),ESB), MAP 910
 7(Z(119),ESCAPA),(Z(120),ESESP),(Z(121),ESESQ),(Z(122),ESES), MAP 920
 8(Z(123),ESALPH),(Z(124),ESBETA),(Z(125),ESCAFBI),(Z(126),IUMAP) MAP 930
 9(Z(127),SSI),(Z(128),SS2),(Z(129),UMIN),(Z(130),SS4) MAP 940
 EQUIVALENCE
 1(Z(131),PRTIME),(Z(132),EOR),(Z(133),EOT),(Z(134),EOB), MAP 960
 2(Z(135),EMOR),(Z(136),DXF),(Z(137),DYF),(Z(138),RHOMIN), MAP 970
 3(Z(139),STAB),(Z(140),XIENRG),(Z(141),XKENRG),(Z(142),XTENRG), MAP 980
 4(Z(143),STT),(Z(144),DTMIN),(Z(145),TRNSFC),(Z(146),EMOT), MAP 990
 5(Z(147),JPROJ),(Z(148),CNAUT),(Z(149),BBAR),(Z(150),EMOB) MAP1000
 MAP1010
 MAP1020
 C C C C C
 END OF COMMON MAP1040
 MAP1050
 MAP1060
 MAP1070
 DIMENSION VALUE(40) MAP1080
 DIMENSION ALE(41) MAP1090
 DATA ALE/2H ,2H ,2H -2H A,2H B,2H C,2H D,2H E,2H F, MAP1100
 1 2H G,2H H,2H I,2H J,2H K,2H L,2H M,2H N,2H O, MAP1110
 2 2H P,2H Q,2H R,2H S,2H T,2H U,2H V,2H W,2H X, MAP1120
 3 2H Y,2H Z,2H +,2H *,2H 1,2H 2,2H 3,2H 4,2H 5, MAP1130
 4 2H 6,2H 7,2H 8,2H 9,2H 0/ MAP1140
 DIMENSION XUM(41) MAP1150

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DATA XUM/2H :2H-.,2H--:2H-A,2H-B,2H-C,2H-D,2H-E,2H-F,
1   2H-G,2H-H,2H-I,2H-J,2H-K,2H-L,2H-M,2H-N,2H-O,
2   2H-P,2H-Q,2H-R,2H-S,2H-T,2H-U,2H-V,2H-W,2H-X,
3   2H-Y,2H-Z,2H-+,2H-*,2H-1,2H-2,2H-3,2H-4,2H-5,
4   2H-6,2H-7,2H-8,2H-9,2H 0/ MAP1160
MAP1170
MAP1180
MAP1190
MAP1200
MAP1210
MAP1220
MAP1230
MAP1240
MAP1250
MAP1260
MAP1270
MAP1280
MAP1290
MAP1300
MAP1310
MAP1320
MAP1330
MAP1340
MAP1350
MAP1360
MAP1370
MAP1380
MAP1390
MAP1400
MAP1410
MAP1420
MAP1430
MAP1440
MAP1450
MAP1460
MAP1470
MAP1480
MAP1490
MAP1500
MAP1510
MAP1520
MAP1530
MAP1540
MAP1550
MAP1560
MAP1570
MAP1580
MAP1590
MAP1600
MAP1610
MAP1620
MAP1630
MAP1640
MAP1650
MAP1660
MAP1670
MAP1680
MAP1690
MAP1700
MAP1710
MAP1720
MAP1730
MAP1740
MAP1750

C
C      *** SEARCH FOR MINIMUM AND MAXIMUM COMPRESSIONS
C          TO SCALE COMPRESSION MAP
C
IDL=I1
JDL=I2
IF (NC.NE.0) GO TO 10
IDL=M1NO(IMAX,55)
JDL=JMAX
10 WSMAX=0.
WSMIN=10.
C
DO 20 J=1,JDL
K=(J-1)*IMAX+1
DO 20 I=1,IDL
K=K+1
WSA=AMX(K)/(TAU(I)*DY(J)*RHOZ)
IF (WSA.EQ.0.) GO TO 20
WSMAX=AMAX1(WSMAX,WSA)
WSMIN=A1N1(WSMIN,WSA)
20 CONTINUE
IF (WSMIN.LT.WSMAX) GO TO 30
WSMIN=0.

C
C      *** DEFINE LINEAR SCALE FACTOR AND PRINT KEY TO
C          COMPRESSION MAP.
C
30 DSCALE=(WSMAX-WSMIN)/FLOAT(IDNMAP)
IF ((AINT(DSCALE*100.)).LT.(DSCALE*100.)) GO TO 50
DSCALE=AINT(DSCALE*100.)/100.
GO TO 60
50 DSCALE=AINT(DSCALE*100.+1.)/100.
60 CONTINUE
DO 70 I=1, IDNMAP
VALUE(I)=WSMIN+FLOAT(I)*DSCALE
WRITE (6,860)
ILIM1=1
ILIM2=20
80 IF (IDNMAP.LT.ILIM2) ILIM2=IDNMAP
WRITE (6,870) (ALE(I+1),I=ILIM1,ILIM2)
WRITE (6,960) (VALUE(I),I=ILIM1,ILIM2)
IF (IDNMAP.EQ.ILIM2) GO TO 90
ILIM1=ILIM2+1
ILIM2=ILIM2+20
GO TO 80
90 CONTINUE

        WRITE (6,980)

C
J=JDL
100 K=(J-1)*IMAX+1
DO 150 I=1,IDL

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K=K+1 MAP1760
IF (AMX(K).GT.0.) GO TO 110 MAP1770
GO TO 130 MAP1780
110 WSA=AMX(K)/(TAU(I)*DY(J)) :0Z MAP1790
IF (WSA.GT.WSMIN) GO TO .20 MAP1800
C *** PRINT A DOT TO REPRESENT SMALLEST COMPRESSION. MAP1805
MA=2 MAP1810
GO TO 140 MAP1820
120 TMA=(WSA-WSMIN)/DSCALE+1. MAP1830
MA=TMA MAP1840
IF (WSA.GT.FLOAT(MA-1)*DSCALE+WSMIN) MA=MA+1 MAP1850
GO TO 140 MAP1860
C *** PRINT A BLANK FOR EMPTY CELLS. MAP1865
130 MA=1 MAP1870
140 PR(I)=ALE(MA) MAP1880
150 CONTINUE MAP1890
C *** PRINT J-VALUE ALONG Y-AXIS WHEN IT IS A MULTIPLE OF 5. MAP1895
IF (MOD(J,5).NE.0) GO TO 160 MAP1900
WRITE (6,880) J,(PR(I),I=1,IDL) MAP1910
GO TO 170 MAP1920
160 WRITE (6,890) (PR(I),I=1,IDL) MAP1930
170 J=J-1 MAP1940
IF (J.GT.0) GO TO 100 MAP1950
C *** PRINT AND LABEL X-AXIS OF MAP. MAP1960
PR(1)=ALE(30) MAP1970
WRITE (6,880) J,(PR(1),I=1,IDL) MAP1980
WRITE (6,900) (I,I=0,IDL,5) MAP1990
C *** SEARCH FOR MINIMUM AND MAXIMUM PRESSURES MAP2000
C TO SCALE PRESSURE MAP MAP2010
C MAP2020
C MAP2030
WSMAX=0. MAP2040
C MAP2050
DO 180 J=1,JDL MAP2060
DO 180 I=1,IDL MAP2070
K=(J-1)*IMAX+I+1 MAP2080
WSA=ABS(P(K)) MAP2090
IF (WSA.EQ.0.) GO TO 180 MAP2100
WSMAX=AMAX1(WSMAX,WSA) MAP2110
180 CONTINUE MAP2120
WSMIN=10.*PMIN MAP2130
WRITE (6,910) MAP2140
C *** PRINT KEY TO MAP ONLY IF THERE ARE NON-ZERO PRESSURES. MAP2145
IF (WSMAX.NE.0.) GO TO 190 MAP2150
J-JDL MAP2160
GO TO 260 MAP2170
C MAP2180
C *** DEFINE LOGARITHMIC SCALE FACTOR AND PRINT KEY TO MAP2220
C PRESSURE MAP. MAP2230
190 MAXEXP=INT ALOG10(WSMAX) MAP2240
MINEXP=INT ALOG10(WSMIN) MAP2250
PSCLE=FLOAT(MAXEXP-MINEXP+1)/FLOAT(IPRMAP) MAP2260
IF ((AINT(PSCLE*1000.)).LT.(PSCLE*1000.)) GO TO 210 MAP2270
PSCLE=AINT(PSCLE*1000.)/1000. MAP2280
GO TO 220 MAP2290
210 PSCLE=AINT(PSCLE*1000.+.)/1000. MAP2300
220 CONTINUE MAP2310

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230 DO 230 I=1,IPRMAP MAP2320
    VALUE(I)=10.**(MINEXP+FLOAT(I)*PSCLE)
    ILIM1=1 MAP2330
    ILIM2=10 MAP2340
240 IF (IPRMAP.LT.ILIM2) ILIM2=IPRMAP MAP2350
    WRITE (6,920) (ALE(I+3),I=ILIM1,ILIM2) MAP2360
    WRITE (6,970) (VALUE(I),I=ILIM1,ILIM2) MAP2370
    IF (IPRMAP.EQ.ILIM2) GO TO 250 MAP2380
    ILIM1=ILIM2+1 MAP2390
    ILIM2=ILIM2+10 MAP2400
    GO TO 240 MAP2410
250 CONTINUE MAP2420
    WRITE (6,980) MAP2430
C MAP2440
    J=JDL MAP2450
260 K=(J-1)*IMAX+1 MAP2460
C MAP2470
    DO 320 I=1,IDL MAP2480
    K=K+1 MAP2490
    IF (AMX(K).GT.0.) GO TO 270 MAP2500
C *** PRINT A BLANK FOR EMPTY CELLS. MAP2510
    MA=1 MAP2520
    GO TO 310 MAP2530
270 IF (P(K).NE.0.) GO TO 280 MAP2540
C *** PRINT A ZERO FOR NONEMPTY CELLS WITH ZERO PRESSURE. MAP2545
    MA=41 MAP2550
    GO TO 310 MAP2560
280 FLOTMA=( ALOG10(ABS(P(K)))-FLOAT(MINEXP))/PSCLE+3. MAP2570
    INTMA=INT(FLOTMA) MAP2580
    IF (FLOTMA.GT.FLOAT(INTMA)) GO TO 290 MAP2590
    MA=INTMA MAP2600
    GO TO 300 MAP2610
290 MA=INTMA+1 MAP2620
C *** DO NOT USE DOT AND DASH IN PRESSURE MAP. MAP2625
300 IF (MA.LE.3) MA=4 MAP2630
310 CONTINUE MAP2640
    PR(I)=ALE(MA) MAP2650
C *** USE XUM ARRAY OF SYMBOLS FOR NEGATIVE PRESSURES. MAP2655
320 IF (P(K).LT.0.) PR(I)=XUM(MA) MAP2660
C
    IF (MOD(J,5).NE.0) GO TO 330 MAP2670
    WRITE (6,880) J,(PR(I),I=1,IDL) MAP2680
    GO TO 340 MAP2690
330 WRITE (6,890) (PR(I),I=1,IDL) MAP2700
340 J=J-1 MAP2710
    IF (J.GT.0) GO TO 260 MAP2720
C *** PRINT AND LABEL X-AXIS OF MAP. MAP2730
    PR(1)=ALE(30) MAP2740
    WRITE (6,880) J,(PR(1),I=1,IDL) MAP2750
    WRITE (6,900) (I,I=0,IDL,5) MAP2760
C
C *** SEARCH FOR MINIMUM AND MAXIMUM RADIAL MAP2770
C VELOCITIES TO DEFINE SCALE FACTOR OF MAP2780
C RADIAL VELOCITY MAP MAP2790
C
    WSMAX=0. MAP2800
C MAP2810
MAP2820
MAP2830
MAP2840

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DO 350 J=1,JDL          MAP2850
DO 350 I=1:IDL          MAP2860
K=(J-1)*IMAX+I+1        MAP2870
WSA=ABS(U(K))           MAP2880
IF (WSA.EQ.0.) GO TO 350 MAP2890
WSMAX=AMAX1(WSMAX,WSA)   MAP2900
CONTINUE                 MAP2910
WSMIN=10.*UMIN          MAP2920
WRITE (6,930)             MAP2930
C                         *** PRINT KEY TO MAP ONLY IF THERE ARE NON-ZERO VALUES.
IF (WSMAX.NE.0.) GO TO 360 MAP2940
J=JDL                   MAP2950
GO TO 430                MAP2960
C
C
C                         *** USCLE IS LOGARITHMIC SCALE FACTOR OF RADIAL VELOCITY
C                         MAP.
360 MAXEXP=INT ALOG10(WSMAX)    MAP3020
MINEXP=INT ALOG10(WSMIN)    MAP3030
USCLE=FLOAT(MAXEXP-MINEXP+1)/FLOAT(IUMAP) MAP3040
IF ((AINT(USCLE*1000.)).LT.(USCLE*1000.)) GO TO 380 MAP3050
USCLE=AINT(USCLE*1000.)/1000.               MAP3060
GO TO 390                  MAP3070
380 USCLE=AINT(USCLE*1000.+1.)/1000.         MAP3080
390 CONTINUE                  MAP3090
C                         *** PRINT KEY TO MAP.
DO 400 I=1,IUMAP          MAP3100
400 VALUE(I)=10.**(MINEXP+FLOAT(I)*USCLE)    MAP3110
ILIM1=I                   MAP3120
ILIM2=10                  MAP3125
410 IF (IUMAP.LT.ILIM2) ILIM2=IUMAP          MAP3130
WRITE (6,920) (ALE(I:3),I=ILIM1,ILIM2)      MAP3140
WRITE (6,970) (VALUE(I),I=ILIM1,ILIM2)      MAP3150
IF (IUMAP.EQ.ILIM2) GO TO 420              MAP3160
ILIM1=ILIM2+1              MAP3170
ILIM2=ILIM2+10             MAP3180
GO TO 410                  MAP3190
420 CONTINUE                  MAP3200
WRITE (6,980)                MAP3210
C
J=JDL                     MAP3220
430 K=(J-1)*IMAX+1          MAP3230
C
DO 490 I=1:IDL            MAP3240
K=K+1                     MAP3250
IF (AMX(K).GT.0.) GO TO 440 MAP3260
C                         *** EMPTY CELL.
MA=1                      MAP3270
GO TO 480                  MAP3280
440 IF (U(K).NE.0.) GO TO 450 MAP3290
C                         *** ZERO RADIAL VELOCITY.
MA=41                     MAP3300
GO TO 480                  MAP3310
450 FLOTMA=(ALOG10(ABS(U(K)))-FLOAT(MINEXP))/USCLE+3. MAP3320
INTMA=INT(FLOTMA)          MAP3330
IF (FLOTMA.GT.FLOAT(INTMA)) GO TO 460 MAP3340
MA=INTMA                  MAP3350
MAP3360
MAP3370
MAP3380
MAP3390
MAP3400
MAP3410

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        GO TO 470
400    MA=INTMA+1
C      *** DO NOT USE DOT OR DASH IN RADIAL VELOCITY MAP.
470    IF (MA.LE.3) MA=4
480    CONTINUE
        PR(I)=ALE(MA)
C      *** USE XUM ARRAY FOR NEGATIVE RADIAL VELOCITIES.
490    IF (U(K).LT.0.) PR(I)=XUM(MA)
C      *** PRINT J-VALUE ALONG Y-AXIS WHEN IT IS A MULTIPLE
C          OF 5.
        IF (MOD(J,5).NE.0) GO TO 500
        WRITE (6,880) J,(PR(I),I=1,IDL)
        GO TO 510
500    WRITE (6,890) (PR(I),I=1,IDL)
510    J=J-1
        IF (J.GT.0) GO TO 430
C      *** PRINT AND LABEL X-AXIS OF MAP.
        PR(1)=ALE(30)
        WRITE (6,880) J,(PR(1),I=1,IDL)
        WRITE (6,900) (I,I=0,IDL,5)

C      *** SEARCH FOR MINIMUM AND MAXIMUM AXIAL
C          VELOCITES TO DEFINE SCALE FACTOR OF
C          AXIAL VELOCITY MAP
C
        WSMAX=0.
C
        DO 520 J=1,JDL
        DO 520 I=1,IDL
        K=(J-1)*IMAX+I+1
        WSA=ABS(V(K))
        IF (WSA.EQ.0.) GO TO 520
        WSMAX=AMAX1(WSMAX,WSA)
520    CONTINUE
        WSMIN=10.*UMIN
        WRITE (6,940)
C      *** PRINT KEY TO MAP ONLY IF THERE ARE NON-ZERO VALUES.
        IF (WSMAX.NE.0.) GO TO 530
        J=JDL
        GO TO 600
C
C      *** VSCL IS LOGARITHMIC SCALE FACTOR FOR AXIAL VELOCITY
C          MAP.
530    MAXEXP=INT ALOG10(WSMAX)
        MINEXP=INT ALOG10(WSMIN)
        VSCL=FLOAT(MAXEXP-MINEXP+1)/FLOAT(IVMAP)
        IF ((AINT(VSCL*1000.)).LT.(VSCL*1000.)) GO TO 550
        VSCL=AINT(VSCL*1000.)/1000.
        GO TO 560
550    VSCL=AINT(VSCL*1000.+1.)/1000.
560    CONTINUE
C      *** PRINT KEY TO AXIAL VELOCITY MAP.
        DO 570 I=1,IVMAP
        VALUE(I)=10.**(MINEXP+FLOAT(I)*VSCL)
        ILIM1=1
        ILIM2=10

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580 IF (IVMAP.LT.ILIM2) ILIM2=IVMAP
      WRITE (6,920) (ALE(I+3),I=ILIM1,ILIM2)
      WRITE (6,970) (VALUE(I),I=ILIM1,ILIM2)
      IF (IVMAP.EQ.ILIM2) GO TO 590
      ILIM1=ILIM2+1
      ILIM2=ILIM2+10
      GO TO 580
  590 CONTINUE
      WRITE (6,980)
C
      J=JDL
  600 K=(J-1)*IMAX+1
C
      DO 660 I=1,IDL
      K=K+1
      IF (AMX(K).GT.0.) GO TO 610
C           *** EMPTY CELL.
      MA=1
      GO TO 650
  610 IF (V(K).NE.0.) GO TO 620
C           *** ZERO AXIAL VELOCITY.
      MA=41
      GO TO 650
  620 FLOTMA=( ALOG10(ABS(V(K)))-FLOAT(MINEXP))/VSCL+E3.
      INTMA=INT(FLOTMA)
      IF (FLOTMA.GT.FLOAT(INTMA)) GO TO 630
      MA=INTMA
      GO TO 640
  630 MA=INTMA+1
C           *** DO NOT USE DOT OR DASH IN AXIAL VELOCITY MAP.
      640 IF (MA.LE.3) MA=4
  650 CONTINUE
      PR(I)=ALE(MA)
C           *** USE XUM ARRAY FOR NEGATIVE AXIAL VELOCITIES.
  660 IF (V(K).LT.0.) PR(I)=XUM(MA)
C           *** PRINT J-VALUE ALONG Y-AXIS WHEN IT IS A MULTIPLE OF 5.
      IF (MOD(J,5).NE.0) GO TO 670
      WRITE (6,880) J,(PR(I),I=1,IDL)
      GO TO 680
  670 WRITE (6,890) (PR(I),I=1,IDL)
  680 J=J-1
      IF (J.GT.0) GO TO 600
C           *** PRINT AND LABEL X-AXIS OF MAP.
      PR(1)=ALE(30)
      WRITE (6,880) J,(PR(1),I=1,IDL)
      WRITE (6,900) (I,I=0,IDL,5)
C
C           *** SEARCH FOR MINIMUM AND MAXIMUM SPECIFIC INTERNAL
C           ENERGIES TO DEFINE SCALE FACTOR OF ENERGY MAP
C
      WSMAX=0.
C
      DO 690 J=1,JDL
      DO 690 I=1,IDL
      K=(J-1)*IMAX+I+1
      WSA=ABS(AIX(K))
      IF (WSA.EQ.0.) GO TO 690

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690   WSMAX=AMAX1(WSMAX,WSA)
       CONTINUE
       WSMIN=10.*SIEMIN
       WRITE (6,950)
C           *** PRINT KEY TO MAP ONLY IF THERE ARE NON-ZERO VALUES.
       IF (WSMAX.NE.0.) GO TO 700
       J=JDL
       GO TO 770
C
C
C           *** ESCLE IS LOGARITHMIC SCALE FACTOR FOR INTERNAL ENERGY
C           MAP.
700   MAXEXP=INT ALOG10(WSMAX)
       MINEXP=INT ALOG10(WSMIN)
       ESCLE=FLOAT(MAXEXP-MINEXP+1)/FLOAT(IEMAP)
       IF ((AINT(ESCLE*1000.)).LT.(ESCLE*1000.)) GO TO 720
       ESCLE=AINT(ESCLE*1000.)/1000.
       GO TO 730
720   ESCLE=AINT(ESCLE*1000.+1.)/1000.
       *** PRINT KEY TO INTERNAL ENERGY MAP.
730   CONTINUE
       DO 740 I=1,IEMAP
740   VALUE(I)=10.**(MINEXP+FLOAT(I)*ESCLE)
       ILIM1=1
       ILIM2=10
750   IF (IEMAP.LT.ILIM2) ILIM2=IEMAP
       WRITE (6,920) (ALE(I+3),I=ILIM1,ILIM2)
       WRITE (6,970) (VALUE(I),I=ILIM1,ILIM2)
       IF (IEMAP.EQ.ILIM2) GO TO 760
       ILIM1=ILIM2+1
       ILIM2=ILIM2+10
       GO TO 750
760   CONTINUE
       WRITE (6,980)
C
       J=JDL
770   K=(J-1)*IMAX+1
C
       DO 830 I=1,IDL
       K=K+1
       IF (AMX(K).GT.0.) GO TO 780
C           *** EMPTY CELL.
       MA=1
       GO TO 820
780   IF (AIX(K).NE.0.) GO TO 790
C           *** ZERO INTERNAL ENERGY.
       MA=41
       GO TO 820
790   FLOTMA=(ALOG10(ADS(AIX(K)))-FLOAT(MINEXP))/ESCLE+3.
       INTMA=INT(FLOTMA)
       IF (FLOTMA.GT.FLOAT(INTMA)) GO TO 800
       MA=INTMA
       GO TO 810
800   MA=INTMA+1
C           *** DO NOT USE DOT AND DASH IN INTERNAL ENERGY MAP.
810   IF (MA.LE.3) MA=4
820   CONTINUE

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MAP4500
MAP4510
MAP4520
MAP4530
MAP4535
MAP4540
MAP4550
MAP4560
MAP4570
MAP4610
MAP4620
MAP4630
MAP4640
MAP4650
MAP4660
MAP4670
MAP4680
MAP4690
MAP4700
MAP4705
MAP4710
MAP4720
MAP4730
MAP4740
MAP4750
MAP4760
MAP4770
MAP4780
MAP4790
MAP4800
MAP4810
MAP4820
MAP4830
MAP4840
MAP4850
MAP4860
MAP4870
MAP4880
MAP4890
MAP4900
MAP4910
MAP4915
MAP4920
MAP4930
MAP4940
MAP4945
MAP4950
MAP4960
MAP4970
MAP4980
MAP4990
MAP5000
MAP5010
MAP5020
MAP5025
MAP5030
MAP5040

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830 PR(I)=ALE(MA) MAP5050
C IF (AIX(K).LT.0.) PR(I)=XUM(MA) MAP5060
C *** PRINT J-VALUE ALONG Y-AXIS WHEN IT IS A MULTIPLE OF 5. MAP5070
IF (MOD(J,5).NE.0) GO TO 840 MAP5080
WRITE (6,880) J,(PR(I),I=1,IDL)
GO TO 850 MAP5090
840 WRITE (6,890) (PR(I),I=1,IDL) MAP5100
850 J=J-1 MAP5110
IF (J.GT.0) GO TO 770 MAP5120
C *** PRINT AND LABEL X-AXIS OF MAP. MAP5130
PR(1)=ALE(30) MAP5140
WRITE (6,880) J,(PR(1),I=1,IDL) MAP5150
WRITE (6,900) (I,I=0,IDL,5) MAP5160
C C
RETURN MAP5170
C C
*** FORMATS MAP5180
800 FORMAT (1H1,4X,15HCOMPRESSION //) MAP5190
810 FORMAT (16H SYMBOL ,20(3X,A2)) MAP5200
880 FORMAT (I10,2H I,54A2) MAP5210
890 FORMAT (10X,2H I,54A2) MAP5215
900 FORMAT (I12,10I10//) MAP5220
910 FORMAT (1H1,4X,15HPRESSURE //) MAP5230
920 FORMAT (16H SYMBOL ,10(3X,A2,5X)) MAP5240
930 FORMAT (1H1,4X,15HRADIAL VELOCITY//) MAP5250
940 FORMAT (1H1,4X,15HAXIAL VELOCITY //) MAP5260
950 FORMAT (1H1,4X,15HINTERNAL ENERGY//) MAP5270
960 FORMAT (16H MAXIMUM VALUE ,20(F5.2)) MAP5280
970 FORMAT (16H MAXIMUM VALUE ,1P10E10.2) MAP5290
980 FORMAT (//) MAP5300
END MAP5310
MAP5320
MAP5330
MAP5340
MAP5350-

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SUBROUTINE PH1 PH1 10
 PH1 20
 PH1 30
 PH1 40
 DIMENSION AMX(2502),AIX(2502),U(2502),V(2502),P(2502),
 1 X(52),XX(54),TAU(52),JPM(52),
 2 Y(102),YY(104),FLEFT(102),YAMC(102),SIGC(102),
 3 GAMC(102),
 4 PK(15),Z(150),
 5 XP(26,51),YP(26,51),
 6 PL(204),UL(204),PR(204),
 7 RSN(52),RST(52),
 8 CMXP(5),CMYP(5),IJ(5),JK(5),
 9 DX(52),DDX(54),DY(102),DDY(104),
 \$ SNB(52),STB(52),UK(52,3),VK(52,3),RHO(52,3)
 *** DIMENSIONED ARRAYS PH1 120
 *** Z-BLOCK IS SAVED ON TAPE. PH1 130
 COMMON Z PH1 140
 COMMON PK PH1 150
 COMMON YY,XX PH1 160
 COMMON DDX,DY PH1 170
 COMMON AMX,AIX,U,V,P PH1 180
 COMMON TAU,JPM PH1 190
 COMMON UL,PL PH1 200
 COMMON XP,YP,CMXP,CMYP PH1 210
 *** NON-DIMENSIONED VARIABLES PH1 220
 COMMON AID,AMMV,AMMY,AMPY,AMUR,AMUT,AMVR,
 1AMVT,DELEB,DELER,DELET,DELM,DTODX,DXYMIN,EAMMP,EAMPY,
 2E,ERDUMP,I,13,IWS,J,K,KA,KB,
 3LL,MD,ME,MZT,NERR,NK,NPRINT,
 4NR,NRZ,NULLE,PIDTS,SIEMIN,SNR,SNT,STR,SOLID,
 5SUM,TESTRH,TWOP,I,URR,WS,WSA,WSB,WSC,WFLAGF,
 6WFLAGL,WFLAGP PH1 230
 *** THE FOLLOWING EQUIVALENCES MAKE AVAILABLE PH1 240
 X(0),Y(0),DX(0),DY(0) PH1 250
 EQUIVALENCE (XX(2),X(1)),(YY(2),Y(1)) PH1 260
 EQUIVALENCE (DDX(2),DX(1)),(DDY(2),DY(1)) PH1 270
 *** SPECIAL EQUIVALENCES FOR PH2 ONLY PH1 280
 EQUIVALENCE (UL,FLEFT),(UL(103),YAMC),
 1 (PL,GAMC,PR),(PL(103),SIGC) PH1 290
 *** SPECIAL EQUIVALENCES FOR PH3 ONLY PH1 300
 EQUIVALENCE (UL,RSN),
 1 (PL,RST),(P,UK), PH1 310
 2 (P(157),VK),(P(313),SNB), PH1 320
 3 (P(365),STB),(P(417),RHO) PH1 330
 *** SPECIAL EQUIVALENCES FOR EDIT PH1 340
 EQUIVALENCE (PR(1),IJ),(PR(6),JK) PH1 350
 *** Z-STORAGE EQUIVALENCES PH1 360
 EQUIVALENCE (Z(1),PROB),(Z(2),CYCLE),PH1 370
 PH1 380
 PH1 390
 PH1 400
 PH1 410
 PH1 420
 PH1 430
 PH1 440
 PH1 450
 PH1 460
 PH1 470
 PH1 480
 PH1 490
 PH1 500
 PH1 510
 PH1 520
 PH1 530
 PH1 540
 PH1 550
 PH1 560
 PH1 570
 PH1 580

1(Z(3),WT),(Z(4),NUMSP),(Z(5),NFRRELPS),(Z(6),NDUMP7), PH1 590
 2(Z(7),ICSTOP),(Z(8),PIDY),(Z(9),TOPMU),(Z(10),RTMU), PH1 600
 3(Z(11),STK1),(Z(12),NUMREZ),(Z(13),ETH),(Z(14),UN14), PH1 610
 4(Z(15),RHINIT),(Z(16),PROJI),(Z(17),UN17),(Z(18),XMAX), PH1 620
 5(Z(19),NZ),(Z(20),NREZ),(Z(21),AMDM),(Z(22),UVMAX), PH1 630
 6(Z(23),UN23),(Z(24),DMIN),(Z(25),JSTR),(Z(26),DTNA), PH1 640
 7(Z(27),CVIS),(Z(28),STK2),(Z(29),STEZ),(Z(30),NC), PH1 650
 8(Z(31),UN31),(Z(32),NRC),(Z(33),IMAX),(Z(34),IMAXA), PH1 660
 9(Z(35),JMAX),(Z(36),JMAXA),(Z(37),KMAX),(Z(38),KMAXA) PH1 670
 EQUIVALENCE
 1(Z(39),BOTM),(Z(40),BOTMV),(Z(41),NUMSPT),(Z(42),CZERO), PH1 690
 2(Z(43),NUMSCA),(Z(44),PRLIM),(Z(45),PRDELT),(Z(46),PRFACT) PH1 700
 EQUIVALENCE
 1(Z(47),II),(Z(48),I2),(Z(49),IPCYCL),(Z(50),TSTOP), PH1 720
 2(Z(51),RHOFIL),(Z(52),TARGV),(Z(53),N3),(Z(54),IVARDY), PH1 730
 3(Z(55),VT),(Z(56),N6),(Z(57),RTM),(Z(58),RTMV), PH1 740
 4(Z(59),UN59),(Z(60),N10),(Z(61),N11),(Z(62),GAMMA), PH1 750
 5(Z(63),TOPM),(Z(64),BOTMU),(Z(65),SN),(Z(66),TOPMV), PH1 760
 6(Z(67),PRYBOT),(Z(68),PRYTOP),(Z(69),PRXRT),(Z(70),CYCPH3), PH1 770
 7(Z(71),REZFCT),(Z(72),TARGI),(Z(73),PROJU),(Z(74),BBOUND), PH1 780
 8(Z(75),EVAP),(Z(76),ECK),(Z(77),NECYCL),(Z(78),II), PH1 790
 9(Z(79),JJ),(Z(80),NMP),(Z(81),Y2),(Z(82),EZPH1) PH1 800
 EQUIVALENCE
 1(Z(83),IVARDX),(Z(84),T),(Z(85),NMPMAX),(Z(86),PMIN), PH1 820
 2(Z(87),INTER),(Z(88),TAYBOT),(Z(89),TAYTOP),(Z(90),IEMAP), PH1 830
 3(Z(91),MC),(Z(92),MR),(Z(93),MZ),(Z(94),MB) PH1 840
 EQUIVALENCE
 1(Z(95),REZ),(Z(96),NODUMP),(Z(97),UN97),(Z(98),UN98), PH1 860
 2(Z(99),UN99),(Z(100),EVAPM),(Z(101),EVAPEN),(Z(102),EVAPMU), PH1 870
 3(Z(103),EVAPMV),(Z(104),EZPH2),(Z(105),SNL),(Z(106),STL), PH1 880
 4(Z(107),TAXRT),(Z(108),IDNMAP),(Z(109),IPRMAP),(Z(110),ROEPS), PH1 890
 5(Z(111),RHINI),(Z(112),VINI),(Z(113),FINAL),(Z(114),IVMAP), PH1 900
 6(Z(115),RHOZ),(Z(116),ESA),(Z(117),ESEZ),(Z(118),ESB), PH1 910
 7(Z(119),ESCAPA),(Z(120),ESESP),(Z(121),ESESQ),(Z(122),ESES), PH1 920
 8(Z(123),ESALPH),(Z(124),ESBETA),(Z(125),ESCAPB),(Z(126),IUMAP), PH1 930
 9(Z(127),SS1),(Z(128),SS2),(Z(129),UMIN),(Z(130),SS4) PH1 940
 EQUIVALENCE
 1(Z(131),PRTIME),(Z(132),EOR),(Z(133),EOT),(Z(134),EOB), PH1 960
 2(Z(135),EMOR),(Z(136),DXF),(Z(137),DYF),(Z(138),RHOMIN), PH1 970
 3(Z(139),STAB),(Z(140),XIENRG),(Z(141),XKENRG),(Z(142),XTENRG), PH1 980
 4(Z(143),STT),(Z(144),DTMIN),(Z(145),TRNSFC),(Z(146),EMOT), PH1 990
 5(Z(147),JPROJ),(Z(148),CNAUT),(Z(149),BBAR),(Z(150),EMOB) PH11000
 PH11010
 PH11020
 PH11030
 PH11040
 PH11050
 PH11060
 *** PH1 COMPUTES THE EFFECT OF THE PRESSURE GRADIENTS ON
 UPDATING THE VELOCITIES AND INTERNAL ENERGIES. PH11062
 *** NRT AND NRC ARE USED TO ADVANCE THE ACTIVE GRID. PH11064
 *** NRT AND NRC ARE USED TO ADVANCE THE ACTIVE GRID. PH11070
 NRT=0 PH11075
 NRC=0 PH11080
 *** VEL=1. FLAGS FIRST PASS. ON SECOND PASS, VEL = 0. PH11090
 VEL=1.0 PH11095
 PH11100

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C *** RC = DISTANCE FROM AXIS TO CENTER OF CELL K.
C RR = DISTANCE FROM AXIS TO CENTER OF CELL K+1.          PH11102
1U   RC=DX(1)/2.0                                         PH11104
      RR=RC+(DX(1)+DX(2))/2.0                           PH11110
      K=2                                                 PH11120
C *** FOR ALL CELLS IN COLUMN NEXT TO AXIS, SET PRESSURE    PH11130
C AT LEFT SIDE OF CELL = PRESSURE IN CELL, AND SET          PH11132
C RADIAL VELOCITY AT LEFT SIDE OF CELL = 0.                  PH11134
C DO 20 J=1,JMAX                                           PH11136
C PL(J)=P(K)                                              PH11140
C UL(J)=0.0                                                PH11150
2U   K=K+IMAX                                             PH11160
      DO 140 I=1,I1                                         PH11170
      K=I+1
C *** DEFINE PRESSURE AND AXIAL VELOCITY AT BOTTOM          PH11180
C BOUNDARY OF GRID.                                         PH11190
C VBLO=V(K)                                              PH11192
C PBLO=P(K)                                              PH11194
C *** IF BOTTOM BOUNDARY OF GRID IS REFLECTIVE, SET        PH11200
C AXIAL VELOCITY AT THAT BOUNDARY = 0.                      PH11210
C IF (CVIS.GT.(-.5)) VBLO=0.                                PH11212
C TAUUTS=TAU(I)*DT                                         PH11214
C DO 130 J=1,I2                                         PH11220
C N=K+IMAX                                              PH11230
C PIDTS=1.0/(PIDY*DT*DY(J))                               PH11240
C IF (AMX(K).LE.0.) GO TO 30                            PH11250
C IF (I.LT.IMAX) GO TO 50                                PH11260
C *** FOR ALL CELLS IN LAST COLUMN OF GRID, SET PRESSURE   PH11270
C AT RIGHT OF CELL = PRESSURE IN CELL. COMPUTE             PH11280
C ENERGY LOST ACROSS RIGHT BOUNDARY AND SUBTRACT IT       PH11282
C FROM ETH, THEORETICAL ENERGY TOTAL.                      PH11284
C PRR=P(K)                                              PH11286
C E=PRR*U(K)/PIDTS*X(I)                                 PH11288
C ETH=ETH-E                                         PH11290
C EOR=EOR-E                                         PH11300
C GO TO 40                                              PH11310
C *** CELL K IS EMPTY                                  PH11320
3U   PL(J)=0.                                              PH11330
      UL(J)=U(K+1)*RR                                     PH11335
      PBLO=0.                                              PH11340
      VBLO=V(N)                                            PH11350
      GO TO 130                                           PH11360
4U   URR=RC*U(K)                                         PH11370
      GO TO 70                                              PH11380
C *** IF CELL ON RIGHT IS EMPTY SET SPECIAL P AND U     PH11390
5U   IF (AMX(K+1).GT.0.) GO TO 60                         PH11400
      PRR=0.                                              PH11410
      URRE=U(K)*RC                                         PH11420
      GO TO 70                                              PH11430
6U   PRR=(P(K)+P(K+1))/2.                                PH11440
      URR=(U(K)*RC+U(K+1)*RR)/2.                          PH11450
7U   IF (J.LT.JMAX) GO TO 80                            PH11460
C *** FOR ALL CELLS IN TOP ROW OF GRID, SET PRESSURE AND   PH11470
C AXIAL VELOCITY AT TOP OF CELL = PRESSURE AND AXIAL        PH11480
C VELOCITY IN CELL. COMPUTE ENERGY LOST ACROSS TOP        PH11482
C BOUNDARY.                                               PH11484
C PABOVE=P(K)                                         PH11486
                                          PH11486
                                          PH11490

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C      E=PABOVE*V(K)/2.*TAUDTS          PH11500
ETH=ETH-E          PH11510
EOT=EOT-E          PH11520
VABOVE=V(K)          PH11530
GO TO 110          PH11540
C      *** IF CELL ABOVE IS EMPTY SET SPECIAL P AND V     PH11550
80    IF (AMX(N).GT.0.) GO TO 90          PH11560
PABOVE=0.          PH11570
VABOVE=V(K)          PH11580
GO TO 100          PH11590
90    PABOVE=(P(K)+P(N))/2.          PH11600
VABOVE=(V(K)+V(N))/2.          PH11610
100   IF (J.GT.1) GO TO 110          PH11620
C      *** IF BOTTOM BOUNDARY OF GRID IS REFLECTIVE, ADD TO ETH     PH11622
C      THE ENERGY GENERATED BY PRESSURE AT THAT BOUNDARY.       PH11624
IF (CVIS.GT.-.5) GO TO 110          PH11630
E=PBL0*V(K)/2.*TAUDTS          PH11640
ETH=ETH+E          PH11650
FOB=ENB+E          PH11660
110   IF (VEL.EQ.0.) GO TO 120          PH11670
C      *** COMPUTE UPDATED VELOCITIES ON FIRST PASS (VEL = 1.)     PH11675
V(K)=V(K)+(PBLO-PABOVE)*TAUDTS/(AMX(K))          PH11680
U(K)=U(K)+(PL(J)-PRR)/(AMX(K))*RC/PIDTS*2.0          PH11690
120   CONTINUE          PH11700
C      *** AIX(X) CHANGED ON BASIS OF GRADIENTS COMPUTED IN FIRST     PH11702
C      PASS. ON SECOND PASS AIX(K) CHANGED AGAIN ON BASIS      PH11704
C      OF GRADIENTS CACULATED FROM THE UPDATED VELOCITIES.      PH11706
WS-(VBLO-VABOVE)*TAUDTS/2.          PH11710
WS=(UL(J)-URR)/PIDTS+WS          PH11720
WSA=AIX(K)+WS*P(K)/AMX(K)          PH11730
AIX(K)=WSA          PH11740
VBLO=VABOVE          PH11750
PL(J)=PRR          PH11760
UL(J)=URR          PH11770
PBLO=PABOVE          PH11780
C      *** RC, N, RR REDEFINED FOR NEXT CELL IN ROW J.          PH11785
130   K=N          PH11790
RC=RR          PH11800
140   RR=(X(I+1)+X(I+2))/2.0          PH11810
IF (VEL.EQ.0.) GO TO 150          PH11820
VEL=0.0          PH11830
GO TO 10          PH11840
150   DO 190 I=1,I1          PH11850
K=I+1          PH11860
DO 180 J=1,I2          PH11870
C      *** SN = 0 (INPUT PARAMETER) SETS NEGATIVE INTERNAL      PH11872
C      ENERGIES TO ZERO.          PH11874
IF (AIX(K).GE.0..OR.SN.GT.0.) GO TO 170          PH11880
E=AIX(K)*AMX(K)          PH11890
ETH=ETH-E          PH11900
EZPH1=EZPH1-E          PH11910
IF (INTER.EQ.0) GO TO 160          PH11920
C      *** PRINT PROPERTIES OF CELLS WHOSE NEGATIVE ENERGY IS      PH11922
C      SET TO ZERO WHEN DOING INTERMEDIATE PRINTS (INTER.GT.0).    PH11924
WRITE (6,240) I,J,AMX(K),AIX(K),U(K),V(K)          PH11930
160   AIX(K)=0.0          PH11940
170   IF (I.NE.I1) GO TO 180          PH11950

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C      *** ENLARGE ACTIVE GRID IN I-DIRECTION IF A CELL IN THE I1 PH11952
C      COLUMN HAS NONZERO VELOCITY OR ENERGY.                      PH11954
180    IF (U(K).NE.0..OR.V(K).NE.0..OR.AIX(K).NE.0.) NRC=1          PH11960
      K=K+IMAX                                         PH11970
      LL=K-2*IMAX                                         PH11980
C      *** ENLARGE ACTIVE GRID IN J-DIRECTION IF A CELL IN THE I2 PH11982
C      ROW HAS NONZERO VELOCITY OR ENERGY.                      PH11984
190    IF (U(LL).NE.0..OR.V(LL).NE.0..OR.AIX(LL).NE.0.) NRT=1          PH11990
      CONTINUE                                         PH12000
      I1=I1+NRC                                         PH12010
      I2=I2+NRT                                         PH12020
C      *** DONT ALLOW ACTIVE GRID TO EXCEED IMAX BY JMAX GRID. PH12025
      IF (I1-IMAX) 210,210,200                         PH12030
200    I1=IMAX                                         PH12040
210    IF (I2-JMAX) 230,230,220                         PH12050
220    I2=JMAX                                         PH12060
230    RETURN                                         PH12070
C
240    FORMAT (4H PH1,2I4,4H M=,1PE15.8,6H SIE=,1PE15.8,4H U=,1PE..5.8,PH12090
      14H V=,1PE15.8,18H SIE SET TO ZERO)                  PH12100
      END                                              PH12110-

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SUBROUTINE PH3 PH3 10
 PH3 20
 PH3 30
 PH3 40
 PH3 50
 PH3 60
 PH3 70
 PH3 80
 PH3 90
 PH3 100
 PH3 110
 PH3 120
 PH3 130
 PH3 140
 PH3 150
 PH3 160
 PH3 170
 PH3 180
 PH3 190
 PH3 200
 PH3 210
 PH3 220
 PH3 230
 PH3 240
 PH3 250
 PH3 260
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 PH3 290
 PH3 300
 PH3 310
 PH3 320
 PH3 330
 PH3 340
 PH3 350
 PH3 360
 PH3 370
 PH3 380
 PH3 390
 PH3 400
 PH3 410
 PH3 420
 PH3 430
 PH3 440
 PH3 450
 PH3 460
 PH3 470
 PH3 480
 PH3 490
 PH3 500
 PH3 510
 PH3 520
 PH3 530
 PH3 540
 PH3 550
 PH3 560
 PH3 570
 PH3 580

C C

DIMENSION AMX(2502),AIX(2502),U(2502),V(2502),P(2502),
 1 X(52),XX(54),TAU(52),JPM(52),
 2 Y(102),YY(104),FLEFT(102),YAMC(102),SIGC(102),
 3 GAMC(102),
 4 PK(15),Z(150),
 5 XP(26,51),YP(26,51),
 6 PL(204),UL(204),PR(204),
 7 RSN(52),RST(52),
 8 CMXP(5),CMYP(5),IJ(5),JK(5),
 9 DX(52),DDX(54),DY(102),DDY(104),
 S SNB(52),STB(52),UK(52,3),VK(52,3),RHO(52,3)

C C

*** DIMENSIONED ARRAYS
 *** Z-BLOCK IS SAVED ON TAPE.

COMMON Z
 COMMON PK
 COMMON YY, XX
 COMMON DDX, DDY
 COMMON AMX, AIX, U, V, P
 COMMON TAU, JPM
 COMMON UL, PL
 COMMON XP, YP, CMXP, CMYP

C
 *** NON-DIMENSIONED VARIABLES

COMMON AIO,AMMV,AMMY,AMPY,AMUR,AMUT,AMVR,
 1AMVT,DELEB,DELER,DELET,DELM,DTODX,DXYMIN,EAMMP,EAMPY,
 2E,ERDUMP,I,I3,IWS,J,K,KA,KB,
 3LL,MD,ME,MZT,NERR,NK,NPRINT,
 4NR,NRZ,NULLE,PIOTS,SIEMIN,SNR,SNT,STR,SOLID,
 5SUM,TESTRH,TWOP,URR,WS,WSA,WSB,WSC,WFLAGF,
 6WFLAGL,WFLAGP

C C

*** THE FOLLOWING EQUIVALENCES MAKE AVAILABLE
 X(0), Y(0), DX(0), DY(0)

C C

EQUIVALENCE (XX(2), X(1)), (YY(2), Y(1))
 EQUIVALENCE (DDX(2), DX(1)), (DDY(2), DY(1))

C C

*** SPECIAL EQUIVALENCES FOR PH2 ONLY

C C

EQUIVALENCE (UL,FLEFT), (UL(103),YAMC),
 1 (PL,GAMC,PR), (PL(103),SIGC)

C C

*** SPECIAL EQUIVALENCES FOR PH3 ONLY

C C

EQUIVALENCE (UL,RSN),
 1 (PL,RST), (P,UK),
 2 (P(157),VK), (P(313),SNB),
 3 (P(365),STB), (P(417),RHO)

C C

*** SPECIAL EQUIVALENCES FOR EDIT

C C

EQUIVALENCE (PR(1), IJ), (PR(0), JK)

C C

*** Z-STORAGE EQUIVALENCES

C C

EQUIVALENCE (Z(1),PROB),(Z(2),CYCLE), PH3 580

1(Z(5),UT),(Z(4),NUMSP),(Z(5),NFRELP),(Z(6),NDUMP7), PH3 590
 2(Z(7),ICSTOP),(Z(8),PIDY),(Z(9),TOPMU),(Z(10),RTMU), PH3 600
 3(Z(11),STK1),(Z(12),NUMREZ),(Z(13),ETH),(Z(14),UN14), PH3 610
 4(Z(15),RHINIT),(Z(16),PROJI),(Z(17),UN17),(Z(18),XMAX), PH3 620
 5(Z(19),NZ),(Z(20),NREZ),(Z(21),AMDM),(Z(22),UVMAX), PH3 630
 6(Z(23),UN23),(Z(24),DMIN),(Z(25),JSTR),(Z(26),DTNA), PH3 640
 7(Z(27),CVIS),(Z(28),STK2),(Z(29),STEZ),(Z(30),NC), PH3 650
 8(Z(31),UN31),(Z(32),NRC),(Z(33),IMAX),(Z(34),IMAXA), PH3 660
 9(Z(35),JMAX),(Z(36),JMAXA),(Z(37),KMAX),(Z(38),KMAXA) PH3 670
 EQUIVALENCE PH3 680
 1(Z(39),BUTM),(Z(40),BOTMV),(Z(41),NUMSPT),(Z(42),CZERO), PH3 690
 2(Z(43),NUMSCA),(Z(44),PRLIM),(Z(45),PRDELT),(Z(46),PRFACT) PH3 700
 EQUIVALENCE PH3 710
 1(Z(47),I1),(Z(48),I2),(Z(49),IPCYCL),(Z(50),TSTOP), PH3 720
 2(Z(51),RHOFIL),(Z(52),TARGV),(Z(53),N3),(Z(54),IVARDY), PH3 730
 3(Z(55),VT),(Z(56),N6),(Z(57),RTM),(Z(58),RTMV), PH3 740
 4(Z(59),UN59),(Z(60),N10),(Z(61),N11),(Z(62),GAMMA), PH3 750
 5(Z(63),TOPM),(Z(64),BOTMU),(Z(65),SN),(Z(66),TOPMV), PH3 760
 6(Z(67),PRYBOT),(Z(68),PRYTOP),(Z(69),PRXRT),(Z(70),CYCPH3), PH3 770
 7(Z(71),REZFCT),(Z(72),TARGI),(Z(73),FROJU),(Z(74),BBOUND), PH3 780
 8(Z(75),EVAP),(Z(76),ECK),(Z(77),NECYCL),(Z(78),II), PH3 790
 9(Z(79),JJ),(Z(80),NMP),(Z(81),Y2),(Z(82),EZPH1) PH3 800
 EQUIVALENCE PH3 810
 1(Z(83),IVARUX),(Z(84),T),(Z(85),NMPMAX),(Z(86),PMIN), PH3 820
 2(Z(87),INTER),(Z(88),TAYBOT),(Z(89),TAYTOP),(Z(90),IEMAP), PH3 830
 3(Z(91),MC),(Z(92),MR),(Z(93),MZ),(Z(94),MB) PH3 840
 EQUIVALENCE PH3 850
 1(Z(95),REZ),(Z(96),NODUMP),(Z(97),UN97),(Z(98),UN98), PH3 860
 2(Z(99),UN99),(Z(100),EVAPM),(Z(101),EVAPEN),(Z(102),EVAPMU), PH3 870
 3(Z(103),EVAPMV),(Z(104),EZPH2),(Z(105),SNL),(Z(106),STL), PH3 880
 4(Z(107),TAXRT),(Z(108),IDNMAP),(Z(109),IPRMAP),(Z(110),ROEPS), PH3 890
 5(Z(111),RHINI),(Z(112),VINI),(Z(113),FINAL),(Z(114),IVMAP), PH3 900
 6(Z(115),RHOZ),(Z(116),ESA),(Z(117),ESEZ),(Z(118),ESB), PH3 910
 7(Z(119),ESCAPA),(Z(120),EGESP),(Z(121),ESESQ),(Z(122),ESES), PH3 920
 8(Z(123),ESALPH),(Z(124),ESBETA),(Z(125),ESCAPB),(Z(126),IUMAP), PH3 930
 9(Z(127),SS1),(Z(128),SS2),(Z(129),UMIN),(Z(130),SS4) PH3 940
 EQUIVALENCE PH3 950
 1(Z(131),PRT1ME),(Z(132),EOR),(Z(133),EOT),(Z(134),EOB), PH3 960
 2(Z(135),EMOR),(Z(136),DXF),(Z(137),DYF),(Z(138),RHOMIN), PH3 970
 3(Z(139),STAB),(Z(140),XIENRG),(Z(141),XKENRG),(Z(142),XTENRG), PH3 980
 4(Z(143),STT),(Z(144),DTMIN),(Z(145),TRNSFC),(Z(146),EMOT), PH3 990
 5(Z(147),JPROJ),(Z(148),CNAUT),(Z(149),BBAR),(Z(150),EMOB) PH31000
 PH31010
 ***** PH31020
 END OF COMMON PH31030
 PH31040
 PH31050
 ***** PH31060
 DX(0)=-DX(1) PH31070
 DY(0)=-DY(1) PH31080
 PH31090
 C *** TURN ON R-P TREATMENT WHEN ACTIVE-GRID REACHES JSTR PH31100
 IF (I2.LT.JSTR) GO TO 400 PH31110
 *** TURN OFF JSTR PH31120
 JSTR=0 PH31130
 PW=0. PH31140
 C *** USE P-STORAGE FOR U,V,SIE BEING CALC. PH31150

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DO 10 K=2,KMAX          PH31160
10 P(K)=0.               PH31170
C     *** CALCULATE SUBCYCLE DT      PH31180
C     ICP3 = INT(CYCPH)
C     *** CALCULATE FACTOR FOR VARIABLE DT      PH31190
C     N=ICP3*(ICP3+1)      PH31200
C     DTFACT=2./FLOAT(N)      PH31210
C     *** LOOP THRU SUBCYCLES      PH31220
C     DO 380 NN=1,ICP3      PH31230
C     *** DECREASING DT      PH31240
C     WS=1CP3-NN+1      PH31250
C     DTSTR=WS*DTFACT*dt      PH31260
C
C     *** INITIALIZE UK,VK FOR ROW1,2 AND BORDER BELOW      PH31270
C     *** NOTE THAT THESE ARE STORED WITH AN EXTRA CELL TO      PH31280
C     RIGHT AND LEFT OF MESH. SO K = 2 IS AXIS CELL.      PH31290
C
C     VFACT=-1.      PH31300
C     *** IF REFLECTIVE,PUT NEG. V IN BORDER CELLS      PH31310
C     IF (CVIS.LT.0.) VFACT=1.      PH31320
C     *** BUT IF TRANS., USE V      PH31330
NKB=1      PH31340
NK=2      PH31350
NKA=3      PH31360
C     *** SET LIMITS USED IN PH3      PH31370
M=I1+1      PH31380
LL=I1-1      PH31390
DO 20 K=2,M      PH31400
L=K+IMAX      PH31410
I=K-1      PH31420
C     *** SET VALUES ADJOINING BOTTOM ROW      PH31430
RHO(K,NK)=AMX(K)/(TAU(I)*DY(1))      PH31440
RHO(K,NKB)=RHO(K,NK)      PH31450
RHO(K,NKA)=AMX(L)/(TAU(I)*DY(2))      PH31460
UK(K,NK)=U(K)      PH31470
UK(K,NKB)=U(K)      PH31480
UK(K,NKA)=U(L)      PH31490
VK(K,NK)=V(K)      PH31500
VK(K,NKB)=V(K)*VFACT      PH31510
VK(K,NKA)=V(L)      PH31520
C     *** BORDER CELL TO LEFT      PH31530
DO 30 N=1,3      PH31540
RHO(1,N)=RHO(2,N)      PH31550
UK(1,N)=UK(2,N)      PH31560
VK(1,N)=VK(2,N)      PH31570
C     *** SNB AND STB HAVE BEEN SET TO 0. BY SETTING ALL      PH31580
C     P STORAGE TO 0.      PH31590
C     *** SET NORMAL STRESSES ON BOTTOM IF REFLECTIVE      PH31600
C     IF (CVIS.LT.0.) GO TO 100      PH31610
C     IF (IMAX.GT.1) GO TO 40      PH31620
C     ***IMAX=1      PH31630
WSA=1.-AIX(2)/STEZ      PH31640
IF (WSA.LT.0) WSA=0.      PH31650
WSB=AMX(2)/(TAU(1)*DY(1)*RHOZ)-1.      PH31660
STRENG=(CZERO+WSB*(STK1+WSB*STK2))*WSA      PH31670
IF (STRENG.LT.0.) STRENG=0.      PH31680
SNB(2)=STRENG*SQRT(2)*ABS(V(2))/V(2)      PH31690
PH31700
PH31710
PH31720

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GO TO 100
C
      ***PUT IWS = RIGHT BOUNDARY OF JPM ARRAY
40    IWS=1
      DO 50 I=1,IMAX
      IF (JPM(I).EQ.0) GO TO 60
      IWS=IWS+1
50    CONTINUE
C
60    DO 90 K=2,IWS
      WSA=.5*DX(K)+DX(K-1)+.5*DX(K-2)
      DUODX=(U(K+1)-U(K-1))/WSA
      DVODX=(V(K+1)-V(K-1))/WSA
      DVODY=2*V(K)/DY(1)
      UOX=2*U(K)/(X(K-1)+X(K-2))
      WSA=DUODX+DVODY+UOX
      TH03=WSA/3.
      WS=DUODX**2+DVODY**2+UOX**2+.5*(DVODX**2)-TH03*WSA
      IF (WS.LE.0.) GO TO 70
      WSA=1.-AIX(K)/STEZ
      IF (WSA.LT.0.) WSA=0.
      WSB=AMX(K)/(TAU(K-1)*DY(1)*RHOZ)-1.
      STRENG=(CZERO+WSB*(STK1+WSB*STK2))*WSA
      IF (STRENG.LT.0.) STRENG=0.
      B=STRENG*SQRT(2./WS)
      GO TO 80
70    B=0.
80    SNB(K)=B*(DVODY-TH03)
90    CONTINUE
100   L=I2-1
C      *** DO ROWS
      DO 370 J=1,L
      K=(J-1)*IMAX+2
C      *** STRESS AT AXIS =0.
      SNL=0.
      STL=0.
C      *** LOOP ON CELLS ACROSS ROW
      DO 330 I=1,LL
      IK=I+1
C      *** IF NOT SOLID, SKIP STRESS CALCULATION
      IF (RHO(IK,NK).LT.SOLID) GO TO 170
C      *** IF ABOVE JPM(I)+1 WE ARE DONE WITH THIS ROW UNLESS ALSO
C          BELOW JPM(I-1)
      JFLAG=0
      IF (J.LE.JPM(I)+1) GO TO 110
      IF (I.EQ.1) GO TO 340
      IF (J.GT.JPM(I-1)) GO TO 340
      JFLAG=1
C      *** CALCULATE STRENGTH
110   WSA=1.-AIX(K)/STEZ
      IF (WSA.LT.0.) GO TO 170
      WSB=RHO(IK,NK)/RHOZ-1.
      STRENG=(CZERO+WSB*(STK1+WSB*STK2))*WSA
      IF (STRENG.LT.0.) GO TO 170
C
C
C
      ****
      *** HOOP STRESS***
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C .....PH32300
C HOOP=0. PH32310
C IF (J.EQ.JPM(I)+1.OR.JFLAG.EQ.1) GO TO 170 PH32320
C     *** SKIP HOOP AND RT CALC IF 1-D PH32330
C IF (IMAX.EQ.1) GO TO 140 PH32340
C     *** DIFFERENCES ARE CENTERED AT CELL-CENTER PH32350
C UOX=UK(IK,NK)/(X(I)+X(I-1))*2. PH32360
C WS=1./(.5*DX(I+1)+DX(I)+.5*DX(I-1)) PH32370
C DUODX=(UK(IK+1,NK)-UK(IK-1,NK))*WS PH32380
C DVODX=(VK(IK+1,NK)-VK(IK-1,NK))*WS PH32390
C WS=1./(.5*DY(J+1)+DY(J)+.5*DY(J-1)) PH32400
C DUODY=(UK(IK,NKA)-UK(IK,NKB))*WS PH32410
C DVODY=(VK(IK,NKA)-VK(IK,NKB))*WS PH32420
C ASSIGN 120 TO LOCA PH32430
C GO TO 240 PH32440
C     *** CALCULATED TH03,B PH32450
120  HOOP=B*(UOX-TH03) PH32460
C .....PH32470
C .....*** END OF HOOP CALC. PH32480
C .....PH32490
C     *** IF THE CELL ON RIGHT IS NOT SOLID, STRESSES ARE ZERO PH32500
C IF (RHO(IK+1,NK).LT.SOLID.OR.IK.EQ.LL) GO TO 140 PH32510
C     *** DIFFERENCES ARE CENTERED AT RIGHT EDGE OF CELL PH32520
C WS=2./(DX(I)+DX(I+1)) PH32530
C DUODX=(UK(IK+1,NK)-UK(IK,NK))*WS PH32540
C DVODX=(VK(IK+1,NK)-VK(IK,NK))*WS PH32550
C WS=1./((DY(J+1)+2.*DY(J)+DY(J-1)) PH32560
C DUODY=(UK(IK,NKA)+UK(IK+1,NKA)-UK(IK,NKB)-UK(IK+1,NKB))*WS PH32570
C DVODY=(VK(IK,NKA)+VK(IK+1,NKA)-VK(IK,NKB)-VK(IK+1,NKB))*WS PH32580
C UOX=(UK(IK+1,NK)+UK(IK,NK))/X(I)*.5 PH32590
C
C ASSIGN 130 TO LOCA PH32600
C     *** CALC. TH03 AND B PH32610
C GO TO 240 PH32620
130  SNR=B*(DUODX-TH03) PH32630
C STR=B*(DUODY+DVODX)*.5 PH32640
C GO TO 150 PH32650
140  SNR=0. PH32660
C STR=0. PH32670
C     *** IF THE CELL ABOVE IS NOT SOLID, STRESSES ABOVE ARE PH32690
150  IF (RHO(IK,NKA).LT.SOLID.OR.J.EQ.L) GO TO 180 PH32700
C
C     *** DIFFERENCES ARE CENTERED AT TOP EDGE OF CELL PH32710
C WS=2./(DY(J+1)+DY(J)) PH32720
C DUODY=(UK(IK,NKA)-UK(IK,NK))*WS PH32730
C DVODY=(VK(IK,NKA)-VK(IK,NK))*WS PH32740
C WS=1./(DX(I+1)+2.*DX(I)+DX(I-1)) PH32750
C DUODX=(UK(IK+1,NK)+UK(IK+1,NKA)-UK(IK-1,NK)-UK(IK-1,NKA))*WS PH32760
C DVODX=(VK(IK+1,NK)+VK(IK+1,NKA)-VK(IK-1,NK)-VK(IK-1,NKA))*WS PH32770
C UOX=(UK(IK,NKA)+UK(IK,NK))/(X(I)+X(I-1)) PH32780
C
C ASSIGN 160 TO LOCA ~ 2790
C GO TO 240 . H32800
160  SNT=B*(DVODY-TH03) PH32810
C STT=B*(DUODY+DVODX)*.5 PH32820
C GO TO 190 PH32830
170  SNR=0. PH32840
C STR=0. PH32850
C

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C           END OF TH03 AND S CALCULATION          PH33430
C
C
280   IF (INTER.NE.99) GO TO 330                 PH33440
      E=0.                                         PH33450
      DO 290 LJD=2,KMAX                         PH33460
      E=E+AMX(LJD)*(.5*(U(LJD)**2+V(LJD)**2)+AIX(LJD)) PH33470
290   CONTINUE                                     PH33480
      WRITE (6,440) I,J,E                         PH33490
      DO 300 LJD=2,IK                           PH33500
      UBAR=.5*(UK(LJD,NK)+UK(LJD,NKA))          PH33510
      VBAR=.5*(VK(LJD,NK)+VK(LJD,NKA))          PH33520
300   E=E-TAU(LJD-1)*(UBAR*STB(LJD)+VBAR*SNB(LJD))*DTSTR PH33530
      IKK=IK+1                                    PH33540
      DO 310 LJD=IKK,I1                          PH33550
      IF (J.GT.JPM(LJD-2)) GO TO 320            PH33560
      UBAR=.5*(UK(LJD,NK)+UK(LJD,NKB))          PH33570
      VBAR=.5*(VK(LJD,NK)+VK(LJD,NKB))          PH33580
310   E=E-TAU(LJD-1)*(UBAR*STB(LJD)+VBAR*SNB(LJD))*DTSTR PH33590
320   UBAR=.5*(UK(IK+1,NK)+UK(IK,NK))          PH33600
      VBAR=.5*(VK(IK+1,NK)+VK(IK,NK))          PH33610
      E=E-TWOP1*DY(J)*X(I)*(UBAR*SNL+VBAR*STL)*DTSTR PH33620
      WRITE (6,440) I,J,E                         PH33630
      PW=PW+DELI*AMX(K)                         PH33640
      WRITE (6,450) PW                           PH33650
330   K=K+1                                       PH33660
C           *** END OF LOOP ON I                  PH33670
C
340   IF (J.EQ.L) GO TO 370                      PH33680
      NKA=NKA+1                                  PH33690
      NK=NK+1                                    PH33700
      NKB=NKB+1                                  PH33710
      IF (NKA.GT.3) NKA=1                        PH33720
      IF (NK.GT.3) NK=1                         PH33730
      IF (NKB.GT.3) NKB=1                        PH33740
      K=(J+1)*IMAX+2                           PH33750
      DO 350 I=1,I1                            PH33760
      IK=I+1                                     PH33770
      UK(IK,NKA)=U(K)                         PH33780
      VK(IK,NKA)=V(K)                         PH33790
      RHO(IK,NKA)=AMX(K)/(TAU(I)*DY(J+1))    PH33800
      K=K+1                                     PH33810
350   C           *** END LOOP                  PH33820
      IF (IMAX.NE.1) GO TO 360                PH33830
      UK(3,NKA)=UK(2,NKA)                      PH33840
      VK(3,NKA)=VK(2,NKA)                      PH33850
      RHO(3,NKA)=RHO(2,NKA)                    PH33860
      C
360   UK(1,NKA)=UK(2,NKA)                      PH33870
      VK(1,NKA)=VK(2,NKA)                      PH33880
      RHO(1,NKA)=RHO(2,NKA)                    PH33890
      C           *** END OF J-LOOP             PH33900
370   CONTINUE                                     PH33910
      C           *** END OF RIGID-PLASTIC CALCULATION FOR ONE DTSTR PH33920
380   CONTINUE                                     PH33930
      DO 390 K=2,KMAX                         PH33940
      P(K)=0.                                     PH33950
390

```

400 RETURN PH34000
C PH34010
410 FORMAT (/6I5,/7H HOOP=,1PE12.6,7H SNL =,1PE12.6,7H STL =,1PE12.PH34020
1o,7H SNR =,1PE12.6,7H STR =,1PE12.6,/7HSTRENG=,1PE12.6,7H SNB =PH34030
2,1PE12.0,7H STB =,1PE12.6,7H SNT =,1PE12.6,7H STT =,1PE12.6/) PH34040
420 FORMAT (/3I5,/7H DELU=,1PE12.6,7H DELV=,1PE12.6,7H DELI=,1PE12.PH34050
16/) PH34060
430 FORMAT (7H DUODX=,1PE12.0,7H DVODY=,1. E12.6,7H UOX =,1PE12.6,7H TPH34070
1E03 =,1PE12.0,/7H DUODY=,1PE12.6,7H DVODX=,1PE12.6,7H WS =,1PE12PH34080
2.0.7H B =,1PE12.6,I7) PH34090
440 FORMAT (4X,2HI=I2,4X,2HJ=I2,4X,2HE=1PE13.7) PH34100
450 FORMAT (4X,3HPW=1PE12.6) PH34110
END PH34120-

SUBROUTINE PH2 PH2 10
 PH2 20
 PH2 30
 PH2 40
 PH2 50
 PH2 60
 PH2 70
 PH2 80
 PH2 90
 PH2 100
 PH2 110
 PH2 120
 PH2 130
 PH2 140
 PH2 150
 PH2 160
 PH2 170
 PH2 180
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 PH2 210
 PH2 220
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 PH2 370
 PH2 380
 PH2 390
 PH2 400
 PH2 410
 PH2 420
 PH2 430
 PH2 440
 PH2 450
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 PH2 480
 PH2 490
 PH2 500
 PH2 510
 PH2 520
 PH2 530
 PH2 540
 PH2 550
 PH2 560
 PH2 570
 PH2 580

C C
 DIMENSION AMX(2502),AIX(2502),U(2502) ,V(2502) ,P(2502) ,
 1 X(52) ,XX(54) ,TAU(52) ,JPM(52) ,
 2 Y(102) ,YY(104) ,FLEFT(102), YAMC(102), SIGC(102),
 3 GAMC(102),
 4 PK(15), Z(150) ,
 5 XP(26,51),YP(26,51),
 6 PL(204) ,UL(204) ,PR(204) ,
 7 RSN(52), RST(52),
 8 CMXP(5) ,CMYP(5) ,IJ(5) ,JK(5) ,
 9 DX(52) ,DDX(54) ,DY(102) ,DDY(104) ,
 5 SNB(52) ,STB(52) ,UK(52,3) ,VK(52,3) ,RHO(52,3)

C C
 *** DIMENSIONED ARRAYS
 *** Z-BLOCK IS SAVED ON TAPE.

COMMON Z
 COMMON PK
 COMMON YY, XX
 COMMON DDX, DDY
 COMMON AMX, AIX, U, V, P
 COMMON TAU, JPM
 COMMON UL, PL
 COMMON XP, YP, CMXP, CMYP

C C
 *** NON-DIMENSIONED VARIABLES

COMMON AID,AMMV,AMMY,AMPY,AMUR,AMUT,AMVR,
 1 AMVT,DELES,DELER,DELET,DELM,DTODX,DAYMIN,EAMMP,EAMPY,
 2 ERDUMP,I,I3,IWS,J,K,KA,KB,
 3 LL,MD,ME,MZT,NERR,NK,NPRINT,
 4 NR,NRZ,NU,LE,PIOTS,SIEMIN,SNR,SNT,STR,SOLID,
 5 SUM,TESTRH,TWUPI,URR,WS,WSA,WSB,WSC,WFLAGF,
 6 WFLAGL,WFLAGP

C C
 *** THE FOLLOWING EQUIVALENCES MAKE AVAILABLE
 X(0), Y(0), DX(0), DY(0)

C C
 EQUIVALENCE (XX(2), X(1)), (YY(2), Y(1))
 EQUIVALENCE (DDX(2), DX(1)), (DDY(2), DY(1))

C C
 *** SPECIAL EQUIVALENCES FOR PH2 ONLY

C C
 EQUIVALENCE (UL,FLEFT), (UL(103),YAMC),
 1 (PL,GAMC,PR), (PL(103),SIGC)

C C
 *** SPECIAL EQUIVALENCES FOR PH3 ONLY

C C
 EQUIVALENCE (UL,RSN),
 1 (PL,RST), (P,UK),
 2 (P(157),VK), (P(313),SNB),
 3 (P(365),STB), (P(417),RHO)

C C
 *** SPECIAL EQUIVALENCES FOR EDIT

C C
 EQUIVALENCE (PR(1), IJ), (PR(6), JK)

C C
 *** Z-STORAGE EQUIVALENCES

C C
 EQUIVALENCE (Z(1),PROB),(Z(2),CYCLE),(Z(3),RHO)

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1(Z( 3),DT ),(Z( 4),NUMSP ),(Z( 5),NFRELP),(Z( 6),NDUMP7), PH2 590
2(Z( 7),ICSTOP),(Z( 8),PIDY ),(Z( 9),TOPMU ),(Z(10),RTMU ), PH2 600
3(Z(11),STK1 ),(Z(12),NUMREZ),(Z(13),ETH ),(Z(14),UN14 ), PH2 610
4(Z(15),RMINIT),(Z(16),PROJI ),(Z(17),UN17 ),(Z(18),XMAX ), PH2 620
5(Z(19),NZ ),(Z(20),NREZ ),(Z(21),AMDM ),(Z(22),UVMAX ), PH2 630
6(Z(23),UN23 ),(Z(24),DMIN ),(Z(25),JSTR ),(Z(26),DTNA ), PH2 640
7(Z(27),CVIS ),(Z(28),STK2 ),(Z(29),STEZ ),(Z(30),NC ), PH2 650
8(Z(31),UN31 ),(Z(32),NRC ),(Z(33),IMAX ),(Z(34),IMAXA ), PH2 660
9(Z(35),JMAX ),(Z(36),JMAXA ),(Z(37),KMAX ),(Z(38),KMAXA ) PH2 670
EQUIVALENCE
1(Z(39),BOTM ),(Z(40),BOTMV ),(Z(41),NUMSPT),(Z(42),CZERO ), PH2 690
2(Z(43),NUMSCA),(Z(44),PRLIM ),(Z(45),PRDELT),(Z(46),PRFACT) PH2 700
EQUIVALENCE
1(Z(47),I1 ),(Z(48),I2 ),(Z(49),IPCYCL),(Z(50),TSTOP ), PH2 720
2(Z(51),RHOF1L),(Z(52),TARGV ),(Z(53),N3 ),(Z(54),IVARDY), PH2 730
3(Z(55),VT ),(Z(56),N6 ),(Z(57),RTM ),(Z(58),RTMV ), PH2 740
4(Z(59),UN59 ),(Z(60),N10 ),(Z(61),N11 ),(Z(62),GAMMA ), PH2 750
5(Z(63),TOPM ),(Z(64),BOTMU ),(Z(65),SN ),(Z(66),TOPMV ), PH2 760
6(Z(67),PRYBOT),(Z(68),PRYTOP ),(Z(69),PRXRT ),(Z(70),CYCPH3), PH2 770
7(Z(71),REZFCT),(Z(72),TARGI ),(Z(73),PROJU ),(Z(74),BBOUND), PH2 780
8(Z(75),EVAP ),(Z(76),ECK ),(Z(77),NECYCL),(Z(78),II ), PH2 790
9(Z(79),JJ ),(Z(80),NMP ),(Z(81),Y2 ),(Z(82),EZPH1 ) PH2 800
EQUIVALENCE
1(Z(83),IVARDX),(Z(84),T ),(Z(85),NMPMAX),(Z(86),PMIN ), PH2 820
2(Z(87),INTER ),(Z(88),TAYBOT),(Z(89),TAYTOP),(Z(90),IEMAP ), PH2 830
3(Z(91),MC ),(Z(92),MR ),(Z(93),MZ ),(Z(94),MB ) PH2 840
EQUIVALENCE
1(Z(95),REZ ),(Z(96),NODUMP),(Z(97),UN97 ),(Z(98),UN98 ), PH2 860
2(Z(99),UN99 ),(Z(100),EVAPM ),(Z(101),EVAPEN),(Z(102),EVAPMU ), PH2 870
3(Z(103),EVAPMV),(Z(104),EZPH2 ),(Z(105),SNL ),(Z(106),STL ), PH2 880
4(Z(107),TAXRT ),(Z(108),IDNMAP),(Z(109),IPRMAP),(Z(110),ROEPS ), PH2 890
5(Z(111),RHINI ),(Z(112),VINI ),(Z(113),FINAL ),(Z(114),IVMAP ), PH2 900
6(Z(115),RHOZ ),(Z(116),ESA ),(Z(117),ESEZ ),(Z(118),ESB ), PH2 910
7(Z(119),ESCAPA),(Z(120),ESESP ),(Z(121),SESSEQ ),(Z(122),ESES ), PH2 920
8(Z(123),ESALPH),(Z(124),ESBETA ),(Z(125),ESCAPB),(Z(126),IUMAP ), PH2 930
9(Z(127),SS1 ),(Z(128),SS2 ),(Z(129),UMIN ),(Z(130),SS4 ) PH2 940
EQUIVALENCE
1(Z(131),PRTIME),(Z(132),EOR ),(Z(133),EOT ),(Z(134),EOB ), PH2 960
2(Z(135),EMOR ),(Z(136),DXF ),(Z(137),DYF ),(Z(138),RHOMIN), PH2 970
3(Z(139),STAB),(Z(140),XIENRG),(Z(141),XKENRG),(Z(142),XTENRG), PH2 980
4(Z(143),STT ),(Z(144),DTMIN ),(Z(145),TRNSFC),(Z(146),EMOT ), PH2 990
5(Z(147),JPROJ ),(Z(148),CNAUT ),(Z(149),BBAR ),(Z(150),EMOS ) PH21000
PH21010
C *** SPECIAL EQUIVALENCE FOR PH2
C EQUIVALENCE (WSOUT,UOTK) PH21012
C ..... PH21014
C ..... PH21020
C ..... PH21030
C END OF COMMON PH21040
C ..... PH21050
C ..... PH21060
C ..... PH21070
C SUME=0. PH21090
C *** ARE TRACER POINTS BEING GENERATED PH21095
C IF (Y2.GT.(-1.)) GO TO 260 PH21100
C *** YES. CALCULATE NEW POSITIONS OF POINTS IN ACTIVE GRID. PH21105
C DO 250 J=1,JJ PH21110

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DO 250 I=1,II
IF (XP(I,J).LE.0.) GO TO 250
IX=XP(I,J)
IY=YP(I,J)
IF (IX.GT.I1) GO TO 250
IF (IY.GT.I2) GO TO 250
K=IY*IMAX+IX+2
      *** SKIP CALCULATION IF POINT IS IN EMPTY CELL
      (AHEAD OF THE MASS IT REPRESENTS).
IF (AMX(K).EQ.0.) GO TO 250
      *** FRX AND FRY GIVE LOCATION OF TRACER POINT IN
      CELL(IX+1,IY+1).
FRX=XP(I,J)-AINT(XP(I,J))
FRY=YP(I,J)-AINT(YP(I,J))

      *** IWS=1 FLAGS TRACER POINTS IN CELLS ON RIGHT OR
      LEFT BOUNDARY OF GRID.
      IWS=2 FLAGS TRACER POINTS IN CELLS ON TOP OR
      BOTTOM BOUNDARY OF GRID.
      IWS=0 FLAGS TRACER POINTS IN CELLS WHICH ARE NOT
      ON A GRID BOUNDARY.

IWS=0
      *** SEE IF TRACER POINT IS IN A BOUNDARY CELL.
IF (IX.LT.1) GO TO 130
IF (IX.GT.IMAX-2) GO TO 110
IF (IY.LT.1) GO TO 160
IF (IY.GT.JMAX-2) GO TO 140
      *** NOT IN BOUNDARY CELL. IS POINT ON LEFT SIDE OF CELL
IF (FRX.LT.-.5) GO TO 40
      *** POINT IS ON RIGHT SIDE OF CELL. IS CELL ON RIGHT EMPTY
IF (AMX(K+1).EQ.0.) GO TO 30
      *** RADIAL COMPONENT BASED ON AVERAGE OF RADIAL VELOCITIES
      OF CELL K AND CELL ON RIGHT OR LEFT.
UEFF=(FRX-.5)*U(K+1)+(1.5-FRX)*U(K)
GO TO 50
      *** CELL ON RIGHT OR LEFT EMPTY-USE RADIAL COMPONENT
      OF CELL K.
UEFF=U(K)
GO TO 50
      *** POINT IS ON LEFT SIDE OF CELL. IS CELL ON LEFT EMPTY
IF (AMX(K-1).EQ.0.) GO TO 30
      *** RADIAL COMPONENT BASED ON AVERAGE OF TWO CELLS.
UEFF=(.5-FRX)*U(K-1)+(.5+FRX)*U(K)
      *** WHEN IWS = 2 AXIAL COMPONENT OF CELL HAS ALREADY BEEN
      CALCULATED.
IF (IWS.GT.1) GO TO 100
      *** IS POINT IN BOTTOM HALF OF CELL
IF (FRY.LT..5) GO TO 90
      *** POINT IS IN TOP HALF. IS CELL ABOVE EMPTY
KA=K+IMAX
IF (AMX(KA).EQ.0.) GO TO 80
      *** AXIAL COMPONENT BASED ON AVERAGE OF AXIAL VELOCITIES
      OF CELL K AND CELL ABOVE OR BELOW.
VEFF=(FRY-.5)*V(KA)+(1.5-FRY)*V(K)
GO TO 100
      *** CELL ABOVE OR BELOW IS EMPTY. USE AXIAL COMPONENT OF
      CELL K.

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50 VEFF=V(K) PH21440
60 TO 100 PH21450
70 KA=K-IMAX PH21460
80 IF (AMX(KA).EQ.0.) GO TO 80 PH21470
90 VEFF=(.5-FRY)*V(KA)+(.5+FRY)*V(K) PH21480
C     *** IX+1 IS I-INDEX AND IY+1 IS J-INDEX OF CELL TRACER PH21482
C     POINT IS IN. COMPUTE NEW LOCATION OF TRACER PTNT. PH21484
100 DTODX=DT/DX(IX+1) PH21490
    XP(I,J)=XP(I,J)+UEFF*DTODX PH21500
    DTODY=DT/DY(IY+1) PH21510
    YP(I,J)=YP(I,J)+VEFF*DTODY PH21520
C     ***IWS.LT.1 MEANS TRACER POINT WAS NOT IN BOUNDARY CELL PH21522
C     BEFORE BEING MOVED, AND ITS NEW POSITION NEED NOT PH21524
C     BE CHECKED - GO TO END OF LOOP. PH21526
IF (IWS.LT.1) GO TO 250 PH21530
GO TO 200 PH21540
C     *** POINT IN CELL ON RIGHT BOUNDARY. PH21542
110 IF (FRX.LT.-.5) GO TO 40 PH21550
IWS=1 PH21560
UEFF=U(K) PH21570
C     *** IS POINT IN CELL ON BOTTOM BOUNDARY PH21575
120 IF (IY.LT.1) GO TO 170 PH21580
C     *** IS POINT IN CELL ON TOP BOUNDARY PH21585
IF (IY.GT.JMAX-2) GO TO 190 PH21590
GO TO 60 PH21600
C     *** POINT IN CELL ON AXIS. PH21605
130 IF (FRX.GT..5) GO TO 20 PH21610
IWS=1 PH21620
UEFF=2.*FRX*U(K) PH21630
GO TO 120 PH21640
C     *** POINT IN CELL ON TOP BOUNDARY. PH21645
140 IF (FRY.LT..5) GO TO 10 PH21650
IWS=2 PH21660
150 VEFF=V(K) PH21670
GO TO 10 PH21680
C     *** POINT IN CELL ON BOTTOM BOUNDARY. RADIAL COMPONENT PH21682
C     HAS NOT BEEN COMPUTED. PH21684
160 IF (FRY.GT..5) GO TO 10 PH21690
IWS=2 PH21700
IF (CVIS.LT.0.) GO TO 150 PH21710
UEFF=2.*FRY*V(K) PH21720
GO TO 10 PH21730
C     *** POINT IN CELL ON BOTTOM BOUNDARY. AXIAL COMPONENT PH21732
C     HAS BEEN COMPUTED. PH21734
170 IF (FRY.GT..5) GO TO 70 PH21740
C     *** COMPUTE AXIAL COMPONENT ON BASIS OF BOTTOM BOUNDARY PH21742
C     CONDITION. PH21744
IF (CVIS.LT.0.) GO TO 180 PH21750
C     *** REFLECTIVE. PH21755
UEFF=2.*FRY*V(K) PH21760
GO TO 100 PH21770
C     *** TRANSMITTIVE. PH21775
180 VEFF=V(K) PH21780
GO TO 100 PH21790
C     *** POINT IN CELL ON TOP BOUNDARY. PH21795
190 IF (FRY.LT..5) GO TO 90 PH21800
GO TO 180 PH21810

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C     *** SPECIAL TESTS FOR TRACER POINTS WHICH WERE IN          PH21812
C     BOUNDARY CELLS BEFORE BEING MOVED.                         PH21814
C     *** IF POINT MOVED BELOW GRID, TEST ON BOTTOM BOUNDARY    PH21816
C     CONDITION, IF REFLECTIVE MOVE POINT BACK INTO GRID,       PH21818
C     IF TRANSMITTIVE SET X-COORDINATE TO -1.                  PH21819
200   IF (YP(I,J).LT.0.) GO TO 220                                PH21820
C     *** IF POINT CROSSED TOP BOUNDARY SET ITS X-COORDINATE PH21822
C     TO -1.                                                       PH21824
.     IF (INT(YP(I,J)).LT.JMAX) GO TO 230                          PH21830
210   XP(I,J)=-1.                                                 PH21840
      GO TO 250                                                 PH21850
220   IF (CVIS.LT.0.) GO TO 210                                  PH21860
C     *** REFLECTIVE.                                         PH21865
      YP(I,J)=-YP(I,J)                                         PH21870
C     *** ADJUST X-COORDINATE IF ITS CALCULATED POSITION IS PH21872
C     NEGATIVE.                                                 PH21874
230   IF (XP(I,J).LT.0.) GO TO 240                                PH21880
C     *** IF POINT CROSSED RIGHT BOUNDARY SET ITS X-COORDINATE PH21882
C     TO -1.                                                       PH21884
      IF (INT(XP(I,J)).LT.IMAX) GO TO 250                      PH21890
      GO TO 210                                                 PH21900
240   XP(I,J)=-XP(I,J)                                         PH21910
C     *** END OF LOOP FOR TRACER POINT MOVEMENT.                PH21915
250   CONTINUE                                                 PH21920
C
C     *** SET TO ZERO ACTIVE GRID AND REZONE FLAGS.             PH21925
260   NRT=0                                                     PH21930
NRC=0                                                     PH21940
REZ=0.0                                                   PH21950
PIDTS=1.0/(PIDY*DT)                                     PH21960
TWOPDT=2./PIDTS                                         PH21970
K=2                                                       PH21980
. C     *** CALCULATE FLUXES ON LEFT SIDE OF CELLS IN AXIS COLUMN. PH21985
DO 310 J=1,JMAX                                         PH21990
IF (AMX(K).LE.0.) GO TO 270                           PH22000
IF (U(K).LT.0.) GO TO 280                           PH22010
270   FLEFT(J)=0.                                         PH22020
      GO TO 300                                         PH22030
280   GAMC(J)=AMX(K)*U(K)*DT/DX(1)                   PH22040
      IF ((GAMC(J)+AMX(K)).GE.0.) GO TO 290           PH22050
      GAMC(J)=-AMX(K)                                 PH22060
290   FLEFT(J)=2.*GAMC(J)*U(K)/SS2                  PH22070
300   GAMC(J)=0.                                         PH22080
      YAMC(J)=0.                                         PH22090
      SIGC(J)=0.                                         PH22100
310   K=K+IMAX                                         PH22110
C     *** DO LOOP IN I-DIRECTION - MOVE UP COLUMNS - SPECIAL PH22112
C     TREATMENT FOR FLUXES AT BOTTOM BOUNDARY OCCURS BEFORE PH22114
C     J-LOOP BEGINS.                                     PH22116
DO 1150 I=1-I1                                         PH22120
J=1                                                       PH22130
K=I+1                                                 PH22140
315   IF(AMX(K)) 1220, 330, 320                      PH22150
320   IF (-V(K).GT.UMIN) GO TO 340                  PH22160
330   AMMV=0.0                                         PH22170
      GO TO 390                                         PH22180
340   AMMY=AMX(K)*V(K)*DT/DY(J)                     PH22190

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      IF (AMMY+AMX(K)) 350,360,360          PH22200
350  AMMY=-AMX(K)                      PH22210
360  IF (CVIS) 370,380,380          PH22220
C     *** BOTTOM BOUNDARY IS TRANSMITTIVE, MATERIAL IS MOVING    P422230
C     OUT, REMOVE ITS ENERGY FROM ETH.          PH22240
370  AMMU=AMMY*U(K)          PH22250
A MMV=AMMY*V(K)          PH22260
DELEB=AIX(K)+(U(K)**2+V(K)**2)/2.0        PH22270
DELES=AMMY*DELEB          PH22280
EMOB=EMOB-DELEB          PH22290
ETH=ETH+DELEB          PH22300
BOTM=BOTM-AMMY          PH22310
BOTMV=BOTMV-AMMV          PH22320
BOTMU=BOTMU-AMMU          PH22330
GO TO 400          PH22340
C     *** BOTTOM BOUNDARY IS REFLECTIVE, NET MOMENTUM CHANGE    PH22350
C     IN Z DIRECTION IS 2*MV/SS2.          PH22360
380  IF (V(K).GE.0.) GO TO 330          PH22370
AMMV=2.*AMMY*V(K)/SS2          PH22380
390  AMMY=0.0          PH22390
AMMU=0.          PH22400
DELEB=0.0          PH22410
C     *** BEGIN DO LOOP IN J(Z) DIRECTION.          PH22420
400  DO 1140 J=1,I2          PH22430
MSLAVE=0          PH22440
NSLAVE=0          PH22450
IF (J.EQ.JMAX) GO TO 420          PH22460
C           NOT AT TOP OF MESH          PH22470
C           L IS INDEX OF CELL ABOVE K          PH22480
L=K+IMAX          PH22490
C           IS CELL K EMPTY          PH22500
IF (AMX(K).GT.0.) GO TO 540          PH22510
C           IF CELL ABOVE IS ALSO EMPTY THEN FLUX=0 OR          PH22520
C           IF FLUX WOULD BE OUT OF EMPTY CELL, THEN FLUX=0.          PH22530
IF (AMX(L).EQ.0..OR.V(L).GE.0.) GO TO 430          PH22540
C           CELL ABOVE NOT EMPTY. MASS MOVING IN DIRECTION OF          PH22550
C           CELL K WHICH IS EMPTY.          PH22560
C           IS CELL ABOVE COLD AND SOLID          PH22570
IF (AIX(L).GT.ESESQ.OR.AMX(L)/(TAU(I)*DY(J+1)).GE.RHOZ) GO TO 410          PH22580
C           COLD, BUT NOT UP TO NORMAL DENSITY          PH22590
C           IS NEXT CELL ABOVE C OLD          PH22600
IF ((J+1).EQ.JMAX) GO TO 410          PH22610
LA=L+IMAX          PH22620
IF (AIX(LA).LT.ESESQ.AND.AMX(LA)/(TAU(I)*DY(J+1)).GT.SOLID) GO TO 1430          PH22630
C           CELL ABOVE IS HOT. DO NOT HOLD BACK.          PH22640
410  M=L          PH22650
V ABOVE=V(L)          PH22660
WL,F=DY(J+1)          PH22670
GO TO 460          PH22680
C           TOP OF MESH. IS MASS MOVING OUT.          PH22690
420  IF (V(K).GT.0.) GO TO 440          PH22700
C           SET FLUX TERMS TO ZERO.          PH22710
430  AMPY=0.          PH22720
GO TO 590          PH22730
C           MASS MOVING OUT OF TOP BOUNDARY          PH22740
440  VABOVE=V(K)          PH22750
C                                     PH22760

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450 WDYF=DY(J) PH22770
C M=K PH22780
C CALCULATE MASS FLUX AT TOP OF CELL PH22790
460 IF (ABS(VABOVE).LE.UMIN) GO TO 430 PH22800
UVMAX=TRNSFC*DY(J)/DT PH22810
IF (ABS(VABOVE).LT.UVMAX) GO TO 480 PH22820
IF (VABOVE.GT.0.) GO TO 470 PH22830
VABOVE=-UVMAX PH22840
GO TO 480 PH22850
470 VABOVE=UVMAX PH22860
480 AMPY=AMX(M)*VABOVE*DT/WDYF PH22870
IF (MSLAVE.NE.0) GO TO 500 PH22880
490 EAMPY=.5*(U(M)**2+V(M)**2)+AIX(M) PH22890
UAMPY=U(M) PH22900
VAMPY=V(M) PH22910
GO TO 590 PH22920
500 IF (VABOVE.GT.0.) GO TO 510 PH22930
M=L PH22940
GO TO 490 PH22950
510 M=K PH22960
GO TO 490 PH22970
520 WSA=.5*(V(K)+V(L)) PH22980
WSB=1.0+(V(L)-V(K))*DT/((DY(J+1)+DY(J))/2.0) PH22990
WDYF=(DY(J)+DY(J+1))/2. PH23000
VABOVE=WSA/WSB PH23010
IF (MSLAVE.NE.0) GO TO 460 PH23020
IF (VABOVE) 530,430,450 PH23030
530 M=L PH23040
GO TO 460 PH23050
.C CELL K IS NOT EMPTY. HOW ABOUT CELL ABOVE K. PH23060
540 IF (AMX(L).GT.0.) GO TO 550 PH23070
C CELL ABOVE IS EMPTY. IS FLUX INTO IT. PH23080
IF (V(K).LE.0.) GO TO 430 PH23090
C FLUX TOWARD EMPTY CELL PH23100
IF (J.EQ.1) GO TO 440 PH23110
C SHOULD MASS BE HELD UP UNTIL CELL IS FULL PH23120
LB=K-IMAX PH23130
IF (AIX(LB).GT.ESESQ.OR.AIX(K).GT.ESESQ.OR.AMX(LB)/(TAU(I)*DY(J-1)) PH23140
1).LT.SOLID.OR.AMX(K)/(TAU(I)*DY(J)).GT.SOLID) GO TO 440 PH23150
GO TO 430 PH23160
550 IF (V(K).GT.0..AND.V(L).LT.0.) GO TO 560 PH23170
IF ((J+1).EQ.JMAX) GO TO 580 PH23180
LA=L+IMAX PH23190
IF (AMX(LA).GT.0..OR.V(K).GE.0..OR.V(L).GE.0.) GO TO 570 PH23200
C K AND L NOT EMPTY BUT CELL ABOVE L IS EMPTY PH23210
TEST FOR SLAVING L TO K PH23220
IF (AMX(L)/(TAU(I)*DY(J+1)).GE.RHOZ.OR.AIX(K).GT.ESESQ.OR.AIX(L).GPH23230
IT.ESESQ) GO TO 520 PH23240
C YES, SLAVE L TO K PH23250
MSLAVE=L PH23260
M=K PH23270
GO TO 520 PH23280
C *** $SREFLECTIVES$ TREATMENT PH23290
560 VMK=V(K)*AMY(K) PH23300
VML=V(L)*AMX(L) PH23310
WSA=VMK+VML PH23320
AMPY=WSA*DT/((DY(J)+DY(J+1))/2.0) PH23330

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VAMPY=(VMK*V(K)+VML*V(L))/WSA PH23340
UAMPY=(VMK*U(K)+VML*U(L))/WSA PH23350
SAVEK=AIX(K)+.5*(U(K)**2+V(K)**2) PH23360
EAMPY=(VMK*SAVEK+VML*(AIX(L)+.5*(U(L)**2+V(L)**2)))/WSA PH23370
GO TO 590 PH23380
570 IF (J.EQ.1) GO TO 520 PH23390
580 LB=K-IMAX PH23400
C IF (AMX(LB).NE.0..OR.V(L).LE.0..OR.U(K).LE.0.) GO TO 520 PH23410
C SHOULD K BE SLAVED TO L PH23420
C IF (AMX(K)/(TAU(I)*DY(J)).GE.RHOZ.OR.AIX(L).GE.ESESQ.OR.AIX(K).GT.1ESESQ) GO TO 520 PH23430
C YES. SLAVE K TO L. PH23440
C MSLAVE=K PH23450
C MEL PH23460
C GO TO 520 PH23470
C *** CHECK FOR ONE-D PH23480
590 IF (ASS(AMPY).LT.ROEPS*AMX(K).AND.ABS(AMPY).LT.ROEPS*AMX(K+IMAX)) 1AMPY=0. PH23490
IF (IMAX.EQ.1) GO TO 620 PH23500
IF (I.EQ.IMAX) GO TO 610 PH23510
C NOT AT RIGHT BOUNDARY PH23520
C IS CELL K.EMPTY PH23530
C IF (AMX(K).GT.0.) GO TO 730 PH23540
C SET FLUX=0 IF CELL ON RIGHT IS EMPTY PH23550
C OR IF VELOCITY IS AWAY FROM EMPTY CELL K PH23560
C IF (AMX(K+1).EQ.0..OR.U(K+1).GE.0.) GO TO 620 PH23570
C CELL TO RIGHT IS NOT EMPTY. SHALL WE LET MASS MOVE PH23580
C INTO CELL K WHICH IS EMPTY. PH23590
C IF (AIX(K+1).GT.ESESQ.OR.AMX(K+1)/(TAU(I+1)*DY(J)).GT.RHOZ) GO TO 1600 PH23600
1600 COLD AND NOT UP TO NORMAL DENSITY PH23610
C IS NEXT CELL TO RIGHT COLD PH23620
C IF ((I+1).EQ.IMAX) GO TO 600 PH23630
C IF (AIX(K+2).LT.ESESQ.AND.AMX(K+2)/(TAU(I+2)*DY(J)).GT.SOLID) GO TO 10 620 TPH23640
C ***CELL ON RIGHT IS HOT. DO NOT HOLD BACK PH23650
600 M=K+1 PH23660
URR=U(M) PH23670
N=I+1 PH23680
GO TO 650 PH23690
C RIGHT EDGE OF MESH PH23700
610 IF (U(K).GT.0.) GO TO 630 PH23710
C NO MASS COMES IN FROM OUTSIDE PH23720
C SET FLUX TERMS TO ZERO PH23730
620 AXMP=0. PH23740
GO TO 790 PH23750
C MASS MOVING OUT OF RIGHT EDGE PH23760
630 URR=U(K) PH23770
640 N=I PH23780
M=K PH23790
C CALCULATE MASS FLUX AT RIGHT OF CELL PH23800
650 IF (ABS(URR).LE.UMIN) GO TO 620 PH23810
UVMAX=TRNSFC*DX(I)/DT PH23820
IF (ABS(URR).LT.UVMAX) GO TO 670 PH23830
IF (URR.GT.0.) GO TO 660 PH23840
URR=-UVMAX PH23850

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      GO TO 670                                PH23900
600  URR=UVMAX                                PH23910
670  AMMP=AMX(M)/TAU(N)*TWO PDT*X(I)*URR    PH23920
      C          SET SPECIFIC ENERGY + MOMENTUM
      IF (NSLAVE.NE.0) GO TO 690                PH23930
      EAMMP=.5*(U(M)**2+V(M)**2)+AIX(M)       PH23940
      UAMMP=U(M)                                PH23950
      VAMMP=V(M)                                PH23960
      GO TO 790                                PH23970
690  IF (URR.GT.0.) GO TO 700                PH23980
      M=K+1                                    PH23990
      GO TO 680                                PH24000
700  M=K                                    PH24010
      GO TO 680                                PH24020
710  WSA=.5*(U(K)+U(K+1))                   PH24030
      WSB=1.+(U(K+1)-U(K))*DT/((DX(I+1)+DX(I))/2.0) PH24040
      URR=WSA/WSB                               PH24050
      IF (NSLAVE.NE.0) GO TO 650                PH24060
      IF (URR) 720,620,640                      PH24070
      M=K+1                                    PH24080
      N=I+1                                    PH24090
      GO TO 650                                PH24100
      C          CELL K IS NOT EMPTY           PH24110
730  IF (AMX(K+1).GT.0.) GO TO 750          PH24120
      C          CELL ON RIGHT OF K IS EMPTY   PH24130
      IF (U(K).LE.0.) GO TO 620                PH24140
      C          SHOULD MASS GO INTO EMPTY CELL PH24150
      IF (I.EQ.1) GO TO 740                  PH24160
      IF (AIX(K-1).GT.ESESQ.OR.AIX(K).GT.ESESQ.OR.AMX(K-1)/(TAU(I-1)*DY(PH24180
      1J)),LT.SOLID.OR.AMX(K)/(TAU(I)*DY(J)).GT.SOLID) GO TO 630
      GO TO 620                                PH24190
740  IF (AIX(K).GE.ESESQ.OR.AMX(K)/(TAU(I)*DY(J)).GE.RHOZ) GO TO 630
      GO TO 620                                PH24200
750  IF (U(K).GT.0..AND.U(K+1).LT.0.) GO TO 760
      IF ((I+1).EQ.IMAX) (J TO 780
      IF (AMX(K+2).GT.0..OR.U(K).GE.0..OR.U(K+1).GE.0.) GO TO 770
      C          K AND K+1 NOT EMPTY BUT CELL K+2
      C          IS EMPTY. TEST FOR SLAVING K+1 TO K
      IF (AIX(K).GE.ESESQ.OR.AIX(K+1).GE.ESESQ.OR.AMX(K+1)/(TAU(I)*DY(J)PH24280
      1).GE.RHOZ) GO TO 710                  PH24290
      C          YES, SLAVE K+1 TO K            PH24300
      NSLAVE=K+1                                PH24310
      N=I                                    PH24320
      M=K                                    PH24330
      GO TO 710                                PH24340
      C          *** $SREFLECTIVE$ TREATMENT   PH24350
760  UMK=U(K)*AMX(K)                          PH24360
      UMKP=U(K+1)*AMX(K+1)                     PH24370
      WSA=TWO PDT*X(I)                         PH24380
      UOTK=UMK/TAU(I)                          PH24390
      UOTKP=UMKP/TAU(I+1)                      PH24400
      SB=UOTK+UOTKP                           PH24410
      MM=WSB*WSA                               PH24420
      UAMMP=(UOTK*U(K)+UOTKP*U(K+1))/WSB     PH24430
      VAMMP=(UOTK*V(K)+UOTKP*V(K+1))/WSB     PH24440
      SAVEK=AIX(K)+.5*(U(K)**2+V(K)**2)       PH24450
      EAMMP=(UOTK*SAVEK+UOTKP*(AIX(K+1)+.5*(U(K+1)**2+V(K+1)**2)))/WSB PH24460

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GO TO 790 PH24470
770 IF (I.EQ.1) GO TO 710 PH24480
780 IF (AMX(K-1).NE.0..OR.U(K+1).LE.0..OR.U(K).LE.0.) GO TO 710 PH24490
C SHOULD K BE SLAVED TO K+1 PH24500
IF (AIX(K).GE.ESESQ.OR.AIX(K+1).GE.ESESQ.OR.AMX(K)/(TAU(I)*DY(J)).PH24510
1GE.RHOZ) GO TO 710 PH24520
C YES, SLAVE K TO K+1 PH24530
NSLAVE=K PH24540
N=I+1 PH24550
M=K+1 PH24560
GO TO 710 PH24570
C WILL K BECOME MORE THAN EMPTY PH24580
790 IF (ABS(AMMP).LT.AMX(K)*ROEPS.AND.ABS(AMMP).LT,ROEPS*AMX(K+1)) AMMPH24590
1P=0. PH24600
WSOUT=0. PH24610
WSA=0. PH24620
WSB=0. PH24630
IF (AMMP.GT.0.) GO TO 830 PH24640
WSA=-AMMP PH24650
800 -F (AMPY.GT.0.) GO TO 840 PH24660
WSA=WSA-AMPY PH24670
810 IF (GAMC(J).LT.0.) GO TO 850 PH24680
WSA=..SA+GAMC(J) PH24690
820 IF (AMMY.LT.0.) GO TO 860 PH24700
WSA=WSA+AMMY PH24710
GO TO 870 PH24720
830 WSB=AMMP PH24730
GO TO 880 PH24740
840 WSB=WSB+AMPY PH24750
GO TO 810 PH24760
850 WSOUT=-GAMC(J) PH24770
GO TO 820 PH24780
860 WSOUT=WSOUT-AMMY PH24790
870 DELM=WSA-WSB-WSOUT PH24800
IF (AMX(K)+DELM.GE.0.) GO TO 970 PH24810
C *** INTERMEDIATE PRINT FOR CELLS OVER-EMPTYING. PH24815
IF (INTER.EQ.0) GO TO 880 PH24820
WRITE (6,1290) I,J,AMX(K),DELM,AMMY,GAMC(J),AMPY,AMMP PH24830
880 IF (WSOUT.GT.AMX(K)) GO TO 920 PH24840
C *** OTHERWISE, MAKE WSB PLUS WSOUT EXACTLY PH24850
C *** EQUAL TO AMX(K) PH24860
WS=AMX(K)-WSOUT PH24870
IF (AMMP.GT.0.) GO TO 900 PH24880
AMPY=WS PH24890
890 DELM=WSA-WSOUT-AMMP-AMPY PH24900
C *** INTERMEDIATE PRINT FOR OVER-EMPTIED CELL AFTER PH24902
C *** R'GHT AND/OR TOP FLUXES ADJUSTED. PH24904
IF (INTER.EQ.0) GO TO 970 PH24906
WRITE (6,1350) AMX(K),DELM,AMMY,GAMC(J),AMPY,AMMP PH24908
GO TO 970 PH24910
900 IF (AMPY.GT.0.) GO TO 910 PH24920
AMMP=WS PH24930
GO TO 890 PH24940
910 AMMP=WS/(AMMP+AMPY)*AMMP PH24950
AMPY=WS-AMMP PH24960
GO TO 890 PH24970
C *** CELL OVER-EMPTIED DOWN OR LEFT. PUT IT BACK. PH24980

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920 IF (AMMP.LT.0.) GO TO 930 PH24990
    AMMP=0.
    AMUR=0.
    AMVR=0.
    DELER=0.
930 IF (AMPY.LT.0.) GO TO 940 PH25000
    AMPY=0.
    AMUT=0.
    AMVT=0.
    DELET=0.
940 MASS=AMX(K) PH25010
    UMOM=MASS*U(K)
    VMOM=MASS*V(K)
    ENGY=MASS*(.5*U(K)**2+.5*V(K)**2+AIX(K))
    MASS=MASS-AMMP
    UMOM=UMOM-AMMP*U(K+1)
    VMOM=VMOM-AMMP*V(K+1)
    ENGY=ENGY-AMMP*(.5*U(K+1)**2+.5*V(K+1)**2+AIX(K+1))
    MASS=MASS-AMPY
    UMOM=UMOM-AMPY*U(L)
    VMOM=VMOM-AMPY*V(L)
    ENGY=ENGY-AMPY*(.5*U(L)**2+.5*V(L)**2+AIX(L))
    MASS=MASS+AMMY
    UMOM=UMOM+AMMU
    VMOM=VMOM+AMMV
    ENGY=ENGY+DELEB
    MASS=MASS+GAMC(J)
    UMOM=UMOM+FLEFT(J)
    VMOM=VMOM+YAMC(J)
    ENGY=ENGY+SIGC(J)
    WSA=-AMIN1(0.,GAMC(J))/WSOUT
    WSB=-AMIN1(0.,AMMY)/WSOUT
    LB=K-IMAX
    IF (LB.LT.0) WSA=1.
    IF (LB.LT.0) GO TO 950
    IF (AMMY.EQ.0..OR.WSB.EQ.0.) GO TO 950
    WSC=AMX(LB)+WSB*MASS
    WSD=AIX(LB)+.5*(U(LB)**2+V(LB)**2)
    U(LB)=(AMX(LB)*U(LB)+WSB*UMOM)/WSC
    V(LB)=(AMX(LB)*V(LB)+WSB*VMOM)/WSC
    AIX(LB)=(AMX(LB)*WSD+WSB*ENGY)/WSC-.5*(U(LB)**2+V(LB)**2)
    AMX(LB)=WSC
950 IF (GAMC(J).EQ.0..OR.WSA.EQ.0.) GO TO 960
    WSC=AMX(K-1)+WSA*MASS
    WSD=AIX(K-1)+.5*(U(K-1)**2+V(K-1)**2)
    U(K-1)=(AMX(K-1)*U(K-1)+WSA*UMOM)/WSC
    V(K-1)=(AMX(K-1)*V(K-1)+WSA*VMOM)/WSC
    AIX(K-1)=(AMX(K-1)*WSD+WSA*ENGY)/WSC-.5*(U(K-1)**2+V(K-1)**2)
    AMX(K-1)=WSC
C           *** INTERMEDIATE PRINT FOR OVER-EMPTIED CELLS AFTER
C           MASS PUT BACK.
960 IF (INTER.EQ.0) GO TO 1100
    WRITE(6,1360) AMX(K), DELM, AMMY, GAMC(J), AMPY, AMMP
    GO TO 1100
970 IF (AMPY.EQ.0.) GO TO 960
C           CALCULATE ENERGY AND MOMENTUM FLUX AT TOP
    AMUT=AMPY*UAMPY

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AMVT=AMPY*VAMPY PH25540
DELET=AMPY*EAMPY PH25550
C IS THIS AT TOP BOUNDARY PH25560
IF (J.NE.JMAX) GO TO 990 PH25570
C YES, TOP. ADJUST ENERGY. PH25580
ETH=ETH-DELET PH25590
EMOT=EMOT+DELET PH25600
TOPM=TOPM+AMPY PH25610
TOPMV=TOPMV+AMVT PH25620
TOPMU=TOPMU+AMUT PH25630
C IS AMPY LARGE ENOUGH TO TRIGGER REZONE PH25640
IF (AMPY/(TAU(I)*DY(J)).GE.VT) REZ=1. PH25650
GO TO 990 PH25660
C AMPY=0. SET MOMENTUM AND ENERGY FLUX=0. PH25670
980 AMUT=0. PH25680
AMVT=0. PH25690
DELET=0. PH25700
990 IF (AMMP.EQ.0.) GO TO 1000 PH25710
C CALCULATE ENERGY + MOMENTUM FLUX AT RIGHT PH25720
AMUR=AMMP*UAMMP PH25730
AMVR=AMMP*VAMMP PH25740
DELER=AMMP*EAMMP PH25750
C IS THIS AT RIGHT BOUNDARY PH25760
IF (I.NE.IMAX) GO TO 1010 PH25770
C YES, RIGHT. ADJUST ENERGY. PH25780
ETH=ETH-DELER PH25790
EMOR=EMOR+DELER PH25800
RTM=RTM+AMMP PH25810
RTMV=RTMV+AMVR PH25820
RTMU=RTMU+AMUR PH25830
C IS AMMP LARGE ENOUGH TO TRIGGER REZONE PH25840
IF (AMMP/(TAU(I)*DY(J)).GE.VT) REZ=1. PH25850
GO TO 1010 PH25860
C AMMP=0. SET MOMENTUM AND ENERGY FLUX=0. PH25870
1000 AMUR=0. PH25880
AMVR=0. PH25890
DELER=0. PH25900
C REPARTITION ENERGY + MOMENTUM PH25910
1010 IF (DELM.EQ.0.) GO TO 1080 PH25920
1020 WSA=.5*(U(K)**2+V(K)**2) PH25930
SIGMU=-AMUT-AMUR+AMMU+FLEFT(J) PH25940
SIGMV=-AMVT-AMVR+AMMV+YAMC(J) PH25950
WS=DELM+AMX(K) PH25960
IF (WS.LE.0.) GO TO 1070 PH25970
UNEW=(SIGMU+AMX(K)*U(K))/WS PH25980
DELU=UNEW-U(K) PH25990
IF (ABS(DELU).LT.UMIN) GO TO 1030 PH26000
U(K)=UNEW PH26010
1030 VNEW=(SIGMV+AMX(K)*V(K))/WS PH26020
DELV=VNEW-V(K) PH26030
IF (ABS(DELV).LT.UMIN) GO TO 1040 PH26040
V(K)=VNEW PH26050
1040 WSB=-DELET-DELER+DELEB+SIGC(J) PH26060
SIENEW=((AIX(K)+WSA)*AMX(K)+WSB)/WS-.5*(U(K)**2+V(K)**2) PH26070
DELI=SIENEW-AIX(K) PH26080
IF (ABS(DELI).GT.SIEMIN) GO TO 1050 PH26090
C *** SUMS ENERGY FLUXES TOO SMALL TO USE. SUME IS PH26092

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C SUBTRACTED FROM ETH AT THE END OF THIS ROUTINE. PH26094
 SUME=SUME+DELI*WS PH26100
 GO TO 1060 PH26110
 1050 AIX(K)=SIENEW PH26120
 1060 AMX(K)=WS PH26130
 GO TO 1090 PH26140
 1070 AMX(K)=0. PH26150
 AIX(K)=0. PH26160
 U(K)=0. PH26170
 V(K)=0. PH26180
 GO TO 1100 PH26190

C DELM=0. BUT IS THERE INDIVIDUAL FLOW PH26200
 1080 IF (AMMP.NE.0.) GO TO 1020 PH26210
 IF (AMPY.NE.0.) GO TO 1020 PH26220
 IF (AMMY.NE.0.) GO TO 1020 PH26230
 IF (GAMC(J).NE.0.) GO TO 1020 PH26240
 1090 IF (I.NE.I1) GO TO 1100 PH26250
 IF (U(K).NE.0..OR.V(K).NE.0..OR.AIX(K).NE.0.) NRC=1 PH26260

C *** SPECIAL INTERMEDIATE PRINT FOR CHECKING ENERGY PH26262
 C CONSERVATION - PRINTS ONLY IF INTER = 7 IN INPUT DECK. PH26264

1100 IF (INTER.NE.7) GO TO 1130 PH26270
 ENERGY=DELER+DELET-SIGC(J) PH26280
 DO 1110 NN=1,JMAX PH26290
 ENERGY=ENERGY+SIGC(NN) PH26300
 1110 CONTINUE PH26310
 DO 1120 LJD=2,KMAX PH26320
 ENERGY=ENERGY+AMX(LJD)*(AIX(LJD)+.5*(U(LJD)**2+V(LJD)**2)) PH26330

1120 CONTINUE PH26340
 WRITE (6,1300) I,J,ENERGY PH26350
 WRITE (6,1310) AMPY,AMMP,AMMY,GAMC(J) PH26360
 WRITE (6,1320) DELET,DELER,DELEB,SIGC(J) PH26370

1130 CONTINUE PH26380
 GAMC(J)=AMMP PH26390
 FLEFT(J)=AMUR PH26400
 YAMC(J)=AMVR PH26410
 SIGC(J)=DELER PH26420
 AMMY=AMPY PH26430
 AMMU=AMUT PH26440
 AMMV=AMVT PH26450
 DELEB=DELET PH26460

C *** END OF J-LOOP. PH26465

C 1140 K=K+IMAX PH26470
 LL=K-IMAX PH26480
 IF (U(LL).NE.0..OR.V(LL).NE.0..OR.AIX(LL).NE.0.) NRT=1 PH26490

C *** END OF I-LOOP. PH26495

C 1150 CONTINUE PH26500
 C *** ADVANCE ACTIVE GRID. PH26505
 I1=I1+NRC PH26510
 I2=I2+NRT PH26520
 IF (IMAX-I1) 1160,1170,1180 PH26530

1160 I1=IMAX PH26540
 1170 CONTINUE PH26550
 1180 IF (JMAX-I2) 1190,1200,1210 PH26560

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1190 I2=JMAX PH26570
1200 CONTINUE PH26580
1210 GO TO 1230 PH26590
C *** NEGATIVE MASS PH26600
1220 NK=315 PH26610
NR=9 PH26620
CALL ERROR PH26630
1230 SUM=0.0 PH26640
C *** EVAPORATE LOW-DENSE CELLS ON BASIS OF EVAP, INPUT PH26642
C PARAMETER. PH26644
DO 1260 I=1,I1 PH26650
K=I+1 PH26660
DO 1270 J=1,I2 PH26670
IF (AMX(K).EQ.0.) GO TO 1270 PH26680
IF (AMX(K)/(TAU(1)*DY(J)).GT.EVAP*RHIN) GO TO 1250 PH26690
WS=(U(K)**2+V(K)**2)/2.0 PH26700
EVAPM=EVAPM+AMX(K) PH26710
WS=AMX(K)*(AIX(K)+WS) PH26720
EVAPEN=EVAPEN+WS PH26730
ETH=ETH-WS PH26740
EVAPMU=EVAPMU+AMX(K)*U(K) PH26750
EVAPMV=EVAPMV+AMX(K)*V(K) PH26760
C *** INTERMEDIATE PRINT FOR CELLS EVAPORATED. PH26765
IF (INTER.EQ.0) GO TO 1240 PH26770
WRITE(6,1340) I,J,AMX(K),AIX(K),U(K),V(K) PH26780
1240 AMX(K)=0.0 PH26790
AIX(K)=0.0 PH26800
P(K)=0.0 PH26810
U(K)=0.0 PH26820
V(K)=0.0 PH26830
GO TO 1270 PH26840
C *** SET NEGATIVE INTERNAL ENERGIES TO ZERO WHEN SN=0. PH26842
C (INPUT PARAMETER). PH26844
1250 IF (AIX(K).GE.0..OR.SN.GT.0.) GO TO 1270 PH26850
C *** SUM SUMS NEGATIVE INTERNAL ENERGY SET TO ZERO. PH26855
SUM=SUM+AIX(K)*AMX(K) PH26860
C *** INTERMEDIATE PRINT FOR CELLS WHOSE NEGATIVE PH26862
C INTERNAL ENERGY IS SET TO ZERO. PH26864
IF (INTER.EQ.0) GO TO 1260 PH26870
WRITE (6,1330) I,J,AMX(K),AIX(K),U(K),V(K) PH26880
1260 AIX(K)=0. PH26890
1270 K=K+IMAX PH26900
1280 CONTINUE PH26910
C *** ETH = THEORETICAL ENERGY SUM, USED IN EDIT FOR PH26912
C ENERGY CHECK. PH26914
C *** EZPH2 = ENERC. SET TO ZERO IN PH2 SINCE TIME=0. PH26916
C *** SUM = NEGAT1 : INTERNAL ENERGY SET TO ZERO ON THIS PH26917
C CYCLE. PH26918
C *** SUME = SUM OF THE ENERGY FLUXES IGNORED ON THIS CYCLE. PH26919
ETH=ETH-SUM-SUME PH26920
EZPH2=EZPH2-SUME-SUM PH26930
RETURN PH26940
C
1290 FORMAT (5H NEGM,I3,I4,4H M=,1PE14.7,6H DELM=,1PE14.7,6H BOT=,1PEPH26960
114.7,7H LEFT=,1PE14.7,6H TOP=,1PE14.7,5H RT=,1PE14.7) PH26970
1300 FORMAT (5H I= I3,6X,5H J= I3,6X,9H ENERGY=1PE15.8) PH26980
1310 FORMAT (7H AMPY=1PE15.8,6X,6H AMMP=1PE15.8,6X,6H AMMY=1PE15.8,9H PH26990

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1GAMC(J)=1PE15.8) PH27000
1320 FORMAT (7H DELET=1PE15.8,6X,6HDELER=1PE15.8,6X,6HDELEB=1PE15.8,9H PH27010
1SIGC(J)=1PE15.8) PH27020
1330 FORMAT (4H PH2,2I4,4H M=,1PE15.8,6H SIE=,1PE15.8,4H U=,1PE15.8, PH27030
14H V=,1PE15.8,18H SIE SET TO ZERO) PH27040
1340 FORMAT (4H PH2,2I4,4H M=,1PE15.8,6H SIE=,1PE15.8,4H U=,1PE15.8, PH27042
14H V=,1PE15.8,19H CELL EVAPORATED) PH27044
1350 FORMAT (12H ADJUST FLUX,4H M=,1PE14.7,6H DELM=,1PE14.7,6H BOT=, PH27045
11PE14.7,7H LEFT=,1PE14.7,6H TOP=,1PE14.7,5H RT=,1PE14.7) PH27046
1360 FORMAT (12H ADJUST MASS,4H M=,1PE14.7,6H DELM=,1PE14.7,6H BOT=, PH27047
11PE14.7,7H LEFT=,1PE14.7,6H TOP=,1PE14.7,5H RT=,1PE14.7) PH27048
END PH27050-

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SUBROUTINE REZONE ..... REZ 10
..... REZ 20
..... REZ 30
DIMENSION AMX(2502),AIX(2502),U(2502) ,V(2502) ,P(2502) , REZ 40
1 X(52) ,XX(54) ,TAU(52) ,JPM(52) , REZ 50
2 Y(102) ,YY(104) ,FLEFT(102),YAMC(102),SIGC(102), REZ 60
3 GAMC(102), REZ 70
4 PK(15), Z(150) , REZ 80
5 XP(26,51),YP(26,51), REZ 90
6 PL(204) ,UL(204) ,PR(204) , REZ 100
7 RSN(52), RST(52), REZ 110
8 CMXP(5) ,CMYP(5) ,IJ(5) ,JK(5) , REZ 120
9 DX(52) ,DDX(54) ,DY(102) ,DDY(104) , REZ 130
$ SNB(52) ,STB(52) ,UK(52,3) ,VK(52,3) ,RH0(52,3) REZ 140
*** DIMENSIONED ARRAYS REZ 150
*** Z-BLOCK IS SAVED ON TAPE. REZ 160
COMMON Z REZ 170
COMMON PK REZ 180
COMMON YY, XX REZ 190
COMMON DDX, DDY REZ 200
COMMON AMX, AIX, U, V, P REZ 210
COMMON TAU, JPM REZ 220
COMMON UL, PL REZ 230
COMMON XP, YP, CMXP, CMYP REZ 240
*** NON-DIMENSIONED VARIABLES REZ 250
COMMON AID ,AMMV ,AMMY ,AMPY ,AMUR ,AMUT ,AMVR , REZ 260
1AMVT ,DELEB ,DELER ,DELET ,DELM ,DTODX ,DXYMIN ,EAMMP ,EAMPY , REZ 270
2E ,ERDUMP ,I ,I3 ,IWS ,J ,K ,KA ,KB , REZ 280
3LL ,MD ,ME ,MZT ,NERR ,NK ,NPRINT , REZ 290
4NR ,NRZ ,NULLE ,PIDTS ,SIEMIN ,SNR ,SNT ,STR ,SOLID , REZ 300
5SUM ,TESTRH ,TWOP ,URR ,WS ,WSA ,WSB ,WSC ,WFLAGF , REZ 310
6WFLAGL ,WFLAGP REZ 320
*** THE FOLLOWING EQUIVALENCES MAKE AVAILABLE REZ 330
X(0), Y(0), DX(0), DY(0) REZ 340
REZ 350
REZ 360
EQUIVALENCE (XX(2), X(1)), (YY(2), Y(1)) REZ 370
EQUIVALENCE (DDX(2), DX(1)), (DDY(2), DY(1)) REZ 380
*** SPECIAL EQUIVALENCES FOR PH2 ONLY REZ 390
REZ 400
REZ 410
EQUIVALENCE (UL,FLEFT), (UL(103),YAMC), REZ 420
1 (PL,GAMC,PR), (PL(103),SIGC) REZ 430
REZ 440
*** SPECIAL EQUIVALENCES FOR PH3 ONLY REZ 450
REZ 460
EQUIVALENCE (UL,RSN), REZ 470
1 (PL,RST), (P,UK), REZ 480
2 (P(157),VK), (P(313),SNB), REZ 490
3 (P(365),STB), (P(417),RH0) REZ 500
REZ 510
*** SPECIAL EQUIVALENCES FOR EDIT REZ 520
REZ 530
EQUIVALENCE (PR(1), IJ), (PR(6), JK) REZ 540
REZ 550
*** Z-STORAGE EQUIVALENCES REZ 560
REZ 570
EQUIVALENCE (Z( 1),PROB ),(Z( 2),CYCLE ), REZ 580

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1(Z(3),DT),(Z(4),NUMSP),(Z(5),NFRELP),(Z(6),NDUMP7), REZ 590
 2(Z(7),ICSTOP),(Z(8),PIDY),(Z(9),TOPMU),(Z(10),RTMU), REZ 600
 3(Z(11),STK1),(Z(12),NUMREZ),(Z(13),ETH),(Z(14),UN14), REZ 610
 4(Z(15),RHINIT),(Z(16),PROJI),(Z(17),UN17),(Z(18),XMAX), REZ 620
 5(Z(19),NZ),(Z(20),NREZ),(Z(21),AMDM),(Z(22),UVMAX), REZ 630
 6(Z(23),UN23),(Z(24),DMIN),(Z(25),JSTR),(Z(26),DTNA), REZ 640
 7(Z(27),CVIS),(Z(28),STK2),(Z(29),STEZ),(Z(30),NC), REZ 650
 8(Z(31),UN31),(Z(32),NRC),(Z(33),IMAX),(Z(34),JMAXA), REZ 660
 9(Z(35),JMAX),(Z(36),JMAXA),(Z(37),KMAX),(Z(38),KMAXA) REZ 670
 EQUIVALENCE . REZ 680
 1(Z(39),BOTM),(Z(40),BOTMV),(Z(41),NUMSPT),(Z(42),CZERO), REZ 690
 2(Z(43),NUMSCA),(Z(44),PRLIM),(Z(45),PRDELT),(Z(46),PRFACT) REZ 700
 EQUIVALENCE REZ 710
 1(Z(47),I1),(Z(48),I2),(Z(49),IPCYCL),(Z(50),TSTOP), REZ 720
 2(Z(51),RHOFILE),(Z(52),TARGV),(Z(53),N3),(Z(54),IVARDY), REZ 730
 3(Z(55),VT),(Z(56),N6),(Z(57),RTM),(Z(58),RTMV), REZ 740
 4(Z(59),UN59),(Z(60),N10),(Z(61),N11),(Z(62),GAMMA), REZ 750
 5(Z(63),TOPM),(Z(64),BOTMU),(Z(65),SN),(Z(66),TOPMV), REZ 760
 6(Z(67),PRYBOT),(Z(68),PRYTOP),(Z(69),PRXRT),(Z(70),CYCPH3), REZ 770
 7(Z(71),REZFCT),(Z(72),TARGI),(Z(73),PROJU),(Z(74),BBOUND), REZ 780
 8(Z(75),EVAP),(Z(76),ECK),(Z(77),NECYCL),(Z(78),II), REZ 790
 9(Z(79),JJ),(Z(80),NMP),(Z(81),Y2),(Z(82),EZPH1) REZ 800
 EQUIVALENCE REZ 810
 1(Z(83),IVARDX),(Z(84),T),(Z(85),NMPMAX),(Z(86),PMIN), REZ 820
 2(Z(87),INTER),(Z(88),TAYBOT),(Z(89),TAYTOP),(Z(90),IEMAP), REZ 830
 3(Z(91),MC),(Z(92),MR),(Z(93),MZ),(Z(94),MB) REZ 840
 EQUIVALENCE REZ 850
 1(Z(95),REZ),(Z(96),NODUMP),(Z(97),UN97),(Z(98),UN98), REZ 860
 2(Z(99),UN99),(Z(100),EVAPM),(Z(101),EVAPEN),(Z(102),EVAPMU), REZ 870
 3(Z(103),EVAPMV),(Z(104),EZPH2),(Z(105),SNL),(Z(106),STL), REZ 880
 4(Z(107),TAXRT),(Z(108),IDNMAP),(Z(109),IPRMAP),(Z(110),RCEPS), REZ 890
 5(Z(111),RHINI),(Z(112),VINI),(Z(113),FINAL),(Z(114),IVMAP), REZ 900
 6(Z(115),RHOZ),(Z(116),ESA),(Z(117),ESEZ),(Z(118),ESB), REZ 910
 7(Z(119),ESCAPA),(Z(120),ESESP),(Z(121),ESESQ),(Z(122),ESES), REZ 920
 8(Z(123),ESALPH),(Z(124),ESBETA),(Z(125),ESCAPB),(Z(126),IUMAP), REZ 930
 9(Z(127),SS1),(Z(128),SS2),(Z(129),UMIN),(Z(130),SS4) REZ 940
 EQUIVALENCE REZ 950
 1(Z(131),FRTIME),(Z(132),EOR),(Z(133),EOT),(Z(134),EOB), REZ 960
 2(Z(135),EMOR),(Z(136),DXF),(Z(137),DYF),(Z(138),RHOMIN), REZ 970
 3(Z(139),STAB),(Z(140),XIENRG),(Z(141),XKENRG),(Z(142),XTENRG), REZ 980
 4(Z(143),STT),(Z(144),DTMIN),(Z(145),TRNSFC),(Z(146),EMOT), REZ 990
 5(Z(147),JPROJ),(Z(148),CNAUT),(Z(149),BBAR),(Z(150),EMOB) REZ1000
 REZ1010
 REZ1020
 END OF COMMON REZ1030
 REZ1040
 REZ1050
 REZ1060
 *** INITIALIZE P-STORAGE. CDT CALLED AGAIN AND PRESSURES REZ1072
 RECALCULATED AFTER GRID REZONED AND BEFORF PH1,PH3 REZ1074
 AND PH2 ARE CALLED. REZ1076
 DO 10 K=2,KMAX REZ1080
 P(K)=0. REZ1090
 CONTINUE REZ1100
 NJMAX=JMAX/2 REZ1110

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IF (IMAX.EQ.1) GO TO 20 REZ1120
NIMAX=IMAX/2 REZ1130
GO TO 70 REZ1140
C *** 1-D REZ1145
.20 IMAX=2 REZ1150
NIMAX=1 REZ1160
K=2 REZ1170
L=2*JMAX+2 REZ1180
C *** STORE PROPERTIES TEMPORARILY IN UNUSED PART OF ARRAYS. REZ1185
DO 30 J=1,JMAX REZ1190
AMX(L)=AMX(K) REZ1200
U(L)=U(K) REZ1210
V(L)=V(K) REZ1220
AIX(L)=AIX(K) REZ1230
K=K+1 REZ1240
L=L+1 REZ1250
CONTINUE REZ1260
K=2 REZ1270
L=2*JMAX+2 REZ1280
C *** ADD ANOTHER COLUMN OF CELLS. EACH CELL IN NEW COLUMN REZ1282
C WILL HAVE SAME VELOCITIES AND SIE AND 3 TIMES THE REZ1284
C MASS OF AXIS CELL. REZ1286
DO 50 J=1,JMAX REZ1290
DO 40 I=1,2 REZ1300
AMX(K)=AMX(L) REZ1310
U(K)=U(L) REZ1320
V(K)=V(L) REZ1330
AIX(K)=AIX(L) REZ1340
K=K+1 REZ1350
AMX(L)=3.*AMX(L) REZ1360
CONTINUE REZ1370
50 L=L+1 REZ1380
L=2*JMAX+1 REZ1390
C *** ADJUST ETH BY ADDING ENERGY OF CELLS IN NEW COLUMN. REZ1395
DO 60 K=3,L,2 REZ1400
ETH=ETH+AMX(K)*(AIX(K)+(V(K)**2)/2.) REZ1410
CONTINUE REZ1420
60 DO 120 J=1,NJMAX REZ1430
K=(J-1)*NIMAX+2 REZ1440
L=(J-1)*2*IMAX+2 REZ1450
DO 110 I=1,NIMAX REZ1460
M=L+IMAX REZ1470
C *** SUM MASS OF FOUR CELLS TO BE MADE INTO ONE CELL. REZ1475
WSA=AMX(L)+AMX(M)+AMX(L+1)+AMX(M+1) REZ1480
IF (WSA.EQ.0.) GO TO 80 REZ1490
C *** SUM KINETIC ENERGY OF FOUR CELLS. REZ1495
WSB=AMX(L)*(U(L)**2+V(L)**2)+AMX(M)*(U(M)**2+V(M)**2)+AMX(L+1)*(U(1L+1)**2+V(L+1)**2)+AMX(M+1)*(U(M+1)**2+V(M+1)**2) REZ1500
REZ1510
C *** COMPUTE VELOCITIES OF NEW CELL FROM VELOCITIES OF REZ1512
C THE FOUR CELLS. REZ1514
U(K)=(U(L)*AMX(L)+U(M)*AMX(M)+U(L+1)*AMX(L+1)+U(M+1)*AMX(M+1))/WSA REZ1520
V(K)=(V(L)*AMX(L)+V(M)*AMX(M)+V(L+1)*AMX(L+1)+V(M+1)*AMX(M+1))/WSA REZ1530
C *** COMPUTE INTERNAL ENERGY OF NEW CELL. REZ1535
AIX(K)=AIX(L)*AMX(L)+AIX(M)*AMX(M)+AIX(L+1)*AMX(L+1)+AMX(M+1)*AIX(1M+1) REZ1540
REZ1550
AMX(K)=WSA REZ1560
WS=U(K)**2+V(K)**2 REZ1570

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C E=AIX(K)+WSB/2.0 REZ1580
*** COMPUTE SIE OF NEW CELL.
AIX(K)=E/AMX(K)-.5*WS REZ1585
IF (K-2) 100,100,90 REZ1590
C *** NEW CELL EMPTY. REZ1600
80 AMX(K)=0. REZ1605
AIX(K)=0. REZ1610
U(K)=0. REZ1620
V(K)=0. REZ1630
C *** INITIALIZE STORAGE OF CELL QUANTIES OF OLD GRID. REZ1640
90 AMX(L)=0.0 REZ1650
U(L)=0.0 REZ1660
V(L)=0.0 REZ1670
AIX(L)=0.0 REZ1680
AMX(M)=0.0 REZ1690
U(M)=0.0 REZ1700
V(M)=0.0 REZ1710
AIX(M)=0.0 REZ1720
AMX(L+1)=0.0 REZ1730
U(L+1)=0.0 REZ1740
V(L+1)=0.0 REZ1750
AIX(L+1)=0.0 REZ1760
AMX(M+1)=0.0 REZ1770
U(M+1)=0.0 REZ1780
V(M+1)=0.0 REZ1790
AIX(M+1)=0.0 REZ1800
100 K=K+1 REZ1810
L=L+2 REZ1820
C *** END OF I-LOOP REZ1830
110 CONTINUE REZ1835
C *** END OF J-LOOP REZ1840
120 CONTINUE REZ1845
C *** OLD PART OF ENLARGED GRID HAS NOW BEEN REZONED. REZ1850
C PROPERTIES OF NEW PART OF GRID WILL BE ASSIGNED REZ1852
C BELOW. REZ1854
C REZ1856
C *** CALCULATE NEW DY'S UP TO EDGE OF OLD GRID BY REZ1860
C COMBINING THE OLD DY'S . CALCULATE NEW Y'S FROM REZ1862
C THE NEW DY'S. REZ1864
DO 130 J=1,NJMAX REZ1870
DY(J)=DY(2*j-1)+DY(2*j) REZ1880
Y(J)=Y(J-1)+DY(J) REZ1890
130 CONTINUE REZ1900
C *** ASSIGN THE VALUE OF THE LAST DY CALCULATED ABOVE REZ1902
C TO ALL CELLS ABOVE THE OLD GRID. REZ1904
NJMAX1=NJMAX+1 REZ1910
DO 140 J=NJMAX1,JMAX REZ1920
DY(J)=DY(NJMAX) REZ1930
Y(J)=Y(J-1)+DY(J) REZ1940
140 CONTINUE REZ1950
C *** IMAX IS SET TO 2 IF DOING A 1-D PROBLEM REZ1955
IF (IMAX.EQ.2) DX(2)=DX(1) REZ1960
DX(1)=DX(1)+DX(2) REZ1970
X(1)=DX(1) REZ1980
WS=X(1)**2 REZ1990
TAU(1)=PIDY*WS REZ2000
C *** ARE YOU DOING A 1-D PROBLEM REZ2005

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IF (IMAX.EQ.2) GO TO 300 REZ2010
*** CALCULATE NEW DX'S OUT TO EDGE OF OLD GRID BY REZ2012
    COMBINING OLD DX'S. CALCULATE NEW X'S AND CELL-FACE REZ2014
    AREAS FROM THE NEW DX'S. REZ2016
DO 150 I=2,NIMAX REZ2020
DX(I)=DX(2*I-1)+DX(2*I)
X(I)=X(I-1)+DX(I)
WSA=X(I)**2 REZ2040
TAU(I)=PIDY*(WSA-WS) REZ2050
WS=WSA REZ2060
CONTINUE REZ2070
150 *** ASSIGN THE VALUE OF THE LAST DX CALCULATED ABOVE REZ2080
    TO ALL CELLS TO THE RIGHT OF THE OLD GRID. REZ2082
NIMAX1=NIMAX+1 REZ2090
DO 160 I=NIMAX1,IMAX REZ2100
DX(I)=DX(NIMAX) REZ2110
X(I)=X(I-1)+DX(I) REZ2120
WSA=X(I)**2 REZ2130
TAU(I)=PIDY*(WSA-WS) REZ2140
WS=WSA REZ2150
160 CONTINUE REZ2160
C REZ2170
C *** INITIALIZE CELL BOUNDARIES REZ2180
C REZ2190
JPB=0 REZ2200
JPA=0 REZ2210
JTB=0 REZ2220
JTA=0 REZ2230
IPRT=0 REZ2240
ITRT=0 REZ2250
REZ2260
C IF (PRYTOP.LE.Y(NJMAX).AND.PRXRT.LE.X(NIMAX).AND.TAYTOP.LE.Y(NJMAX) REZ2270
1).AND.TAXRT.LE.X(NIMAX)) GO TO 300 REZ2280
C REZ2290
C *** COMPUTE JPB, JPA - BOTTOM AND TOP CELL BOUNDARIES OF REZ2300
C PROJECTILE REZ2310
C REZ2320
IF (PRYBOT.LT.0..OR.(PRYTOP.LE.Y(NJMAX).AND.PRXRT.LE.X(NIMAX))) GO REZ2330
1 TO 230 REZ2340
J=0 REZ2350
IF (PRYBOT.EQ.0.) GO TO 180 REZ2360
DYSUM=0. REZ2370
DO 170 J=1,JMAX REZ2380
DYSUM=DYSUM+DY(J) REZ2390
IF (PRYBOT.GE.DYSUM-.5*DY(J).AND.PRYBOT.LT.DYSUM+.5*DY(J+1)) GO TO REZ2400
1 180 REZ2410
170 CONTINUE REZ2420
GO TO 230 REZ2430
180 JPB=MIND(J+1,JMAX) REZ2440
DO 190 J=JPB,JMAX REZ2450
DYSUM=DYSUM+DY(J) REZ2460
IF (PRYTOP.GE.DYSUM-.5*DY(J).AND.PRYTOP.LT.DYSUM+.5*DY(J+1)) GO TO REZ2470
1 200 REZ2480
190 CONTINUE REZ2490
200 JPA=J REZ2500
C REZ2510
C *** COMPUTE IPRT - RIGHT CELL BOUNDARY OF PROJECTILE REZ2520

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C
DXSUM=0.
DO 210 I=1,IMAX
DXSUM=DXSUM+DX(I)
IF (PRXRT.GE.DXSUM-.5*DX(I).AND.PRXRT.LT.DXSUM+.5*DX(I+1)) GO TO 2REZ2570
120
CONTINUE
IPRT=I
C
*** COMPUTE JTB, JTA - BOTTOM AND TOP CELL BOUNDARIES OF TARGET
C
230 IF (TAYBOT.LT.0..OR.(TAYTOP.LE.Y(NJMAX).AND.TAXRT.LE.X(NIMAX))) GO TO REZ2650
1 TO 300
J=0
IF (TAYBOT.EQ.0.) GO TO 250
DYSUM=0.
DO 240 J=1,JMAX
DYSUM=DYSUM+DY(J)
IF (TAYBOT.GE.DYSUM-.5*DY(J).AND.TAYBOT.LT.DYSUM+.5*DY(J+1)) GO TO REZ2720
1 250
CONTINUE
GO TO 300
250 JTB=MINO(J+1,JMAX)
DO 260 J=JTB,JMAX
DYSUM=DYSUM+DY(J)
IF (TAYTOP.GE.DYSUM-.5*DY(J).AND.TAYTOP.LT.DYSUM+.5*DY(J+1)) GO TO REZ2790
1 270
CONTINUE
JTA=J
C
*** COMPUTE ITRT - RIGHT CELL BOUNDARY OF TARGET
C
DXSUM=0.
DO 280 I=1,IMAX
DXSUM=DXSUM+DX(I)
IF (TAXRT.GE.DXSUM-.5*DX(I).AND.TAXRT.LT.DXSUM+.5*DX(I+1)) GO TO 2REZ2890
190
CONTINUE
ITRT=I
300 CONTINUE
C
*** REDEFINE IMAX AND JMAX FOR ORDERING THE K ARRAYS BELOW.
IMAX=NIMAX
JFILB=JPA+1
JFILA=JTB-1
JMAX=NJMAX
I1=I1/2
I2=I2/2
C
*** IS THIS A 1-D PROBLEM
IF (IMAX.GT.1) GO TO 320
C
*** YES.ADD TARGET MATERIAL
JMP1=JMAX+1
JMAX=2*JMAX
DO 310 J=JMP1,JMAX
K=J+1
AMX(K)=RHINIT*TAU(1)*DY(J)

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IF (TARGI.GT.0.) I2=J REZ3060
AIX(K)=TARGI REZ3070
ETH=ETH+AMX(K)*AIX(K) REZ3080
310 CONTINUE REZ3090
JPROJ=JPROJ/2 REZ3100
I1=1 REZ3110
GO TO 520 REZ3120
C *** PREPARE TO SHUFFLE K ARRAYS SUCH AS TO PRESERVE REZ3130
C K=(J-1)*IMAX+I+1, THEN ADD MATERIAL TO NEW PART REZ3140
C OF GRID. REZ3145
320 DO 360 N=1,JMAX REZ3150
J=JMAX+1-N REZ3160
K=(J-1)*IMAX+I+IMAX REZ3170
L=(J-1)*(IMAX+IMAX)+1+IMAX REZ3180
DO 350 I=1,IMAX REZ3190
AMX(L)=AMX(K) REZ3200
AIX(L)=AIX(K) REZ3210
U(L)=U(K) F_Z3220
V(L)=V(K) REZ3230
IF (J-1) 340,340,330 REZ3240
330 AMX(K)=0.0 REZ3250
AIX(K)=0.0 REZ3260
V(K)=0.0 REZ3270
U(K)=0.0 REZ3280
340 K=K-1 REZ3290
L=L-1 REZ3300
350 CONTINUE REZ3310
360 CONTINUE REZ3320
C *** REDEFINE IMAX,JMAX SO THEY WILL REPRESENT NUMBER REZ3322
C OF COLUMNS AND ROWS IN NEW GRID (SAME AS IN OLD GRID). REZ3324
IMAX=NIMAX*2 REZ3330
JMAX=NJMAX*2 REZ3340
IL=NIMAX+1 REZ3350
JL=NJMAX+1 REZ3360
IF (PRYTOP.LE.Y(NJMAX).AND.PRXRT.LE.X(NIMAX).AND.TAYTOP.LE.Y(NJMAX) REZ3370
1).AND.TAXRT.LE.X(NIMAX) GO TO 510 REZ338G
C *** ADD APPROPRIATE MATERIAL REZ3390
C IN CELLS ABOVE (BUT NOT TO THE RIGHT OF) OLD GRID. REZ3395
DO 430 I=1,NIMAX REZ3400
K=(JL-1)*IMAX+I+1 REZ3410
DO 420 J=JL,JMAX REZ3420
IF (PRYBOT.LT.0.) GO TO 370 REZ3430
IF (J.GE.JPB.AND.J.LE.JPA.AND.I.LE.IPRT) GO TO 390 REZ3440
C *** NOT PROJECTILE-MATERIAL REZ3450
370 IF (RHOFIL.EQ.0.) GO TO 380 REZ3460
IF (J.GE.JFILB.AND.J.LE.JFILA) GO TO 400 REZ3470
C *** NOT FILLER-MATERIAL REZ3480
380 IF (TAYBOT.LT.0.) GO TO 420 REZ3490
IF (J.GE.JTB.AND.J.LE.JTA.AND.I.LE.ITRT) GO TO 410 REZ3500
C *** NOT TARGET. THUS,VACUUM. REZ3510
GO TO 420 REZ3520
C *** ADD PROJ. MATERIAL REZ3530
390 AMX(K)=RHINI*TAU(I)*DY(J) REZ3540
IF (PROJU.EQ.0..AND.VINI.EQ.0..AND.PROJI.EQ.0.) GO TO 420 REZ3550
IF (I.GT.I1) I1=I REZ3560
IF (J.GT.I2) I2=J REZ3570
U(K)=PROJU REZ3580

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V(K)=VINI REZ3590
AIX(K)=PROJI REZ3600
GO TO 420 REZ3610
C *** ADD FILLER REZ3620
400 AMX(K)=RHOFIL*TAU(I)*DY(J) REZ3630
GO TO 420 REZ3640
C *** ADD TARGET MATERIAL REZ3650
410 AMX(K)=RHINIT*TAU(I)*DY(J) REZ3660
IF (TARGV.EQ.0..AND.TARGI.EQ.0.) GO TO 420 REZ3670
IF (I.GT.I1) I1=I REZ3680
IF (J.GT.I2) I2=J REZ3690
V(K)=TARGV REZ3700
AIX(K)=TARGI REZ3710
420 K=K+IMAX REZ3720
430 CONTINUE REZ3730
C *** ADD APPROPRIATE MATERIAL TO CELLS ON THE RIGHT REZ3732
C OF THE OLD GRID. REZ3734
DO 500 I=IL,IMAX REZ3740
K=I+1 REZ3750
DO 490 J=1,JMAX REZ3760
IF (PRYBOT.LT.0.) GO TO 440 REZ3770
IF (J.GE.JPB.AND.J.LE.JPA.AND.I.LE.IPRT) GO TO 460 REZ3780
C *** NOT PROJECTILE MATERIAL. REZ3785
440 IF (RHOFIL.EQ.0.) GO TO 450 REZ3790
IF (J.GE.JFILB.AND.J.LE.JFILA) GO TO 470 REZ3800
C *** NOT FILLER MATERIAL. REZ3805
450 IF (TAYBOT.LT.0.) GO TO 490 REZ3810
IF (J.GE.JTB.AND.J.LE.JTA.AND.I.LE.ITRT) GO TO 480 REZ3820
C *** NOT TARGET MATERIAL. THUS,VACUUM. REZ3825
GO TO 490 REZ3830
C *** ADD PROJECTILE MATERIAL. REZ3835
460 AMX(K)=RHINI*TAU(I)*DY(J) REZ3840
IF (PROJU.EQ.0..AND.VINI.EQ.0..AND.PROJI.EQ.0.) GO TO 490 REZ3850
IF (I.GT.I1) I1=I REZ3860
IF (J.GT.I2) I2=J REZ3870
U(K)=PROJU REZ3880
V(K)=VINI REZ3890
AIX(K)=PROJI REZ3900
GO TO 490 REZ3910
C *** ADD FILLER. REZ3915
470 AMX(K)=RHOFIL*TAU(I)*DY(J) REZ3920
GO TO 490 REZ3930
C *** ADD TARGET MATERIAL. REZ3935
480 AMX(K)=RHINIT*TAU(I)*DY(J) REZ3940
IF (TARGV.EQ.0..AND.TARGI.EQ.0.) GO TO 490 REZ3950
IF (I.GT.I1) I1=I REZ3960
IF (J.GT.I2) I2=J REZ3970
V(K)=TARGV REZ3980
AIX(K)=TARGI REZ3990
490 K=K+IMAX REZ4000
500 CONTINUE REZ4010
C *** REDEFINE JPROJ,USUALLY J-INDEX OF TOP CELL IN REZ4012
C PROJECTILE (INPUT PARAMETER). REZ4014
510 JPROJ=JPROJ/2 REZ4020
C *** REDEFINE ACTIVE GRID MARKERS. REZ4030
C
II=I1*2 REZ4040
REZ4050

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```

520 I2=I2+2 REZ4060
IF (I1.GT.IMAX) I1=IMAX REZ4070
IF (I2.GT.JMAX) I2=JMAX REZ4080
C *** CALL TO REZONE AND CDT COUNTED AS A CALCULATIONAL REZ4082
C CYCLE, SO NC AND T ARE INCREMENTED BEFORE PROCEEDING REZ4084
C ON TO PH1,PH3 AND PH2. REZ4086
C WS=T+DTNA REZ4090
NK=NC+1 REZ4100
C WRITE (5,620) WS,NK,UX(1) REZ4110
C *** REDEFINE CONSTANTS AND CELL LIMITS FOR CALCULATING REZ4122
C TENSIONS AND STRESSES. REZ4124
KMAX=1MAX*JMAX+1 REZ4130
IMAXA=IMAX+1 REZ4140
JMAXA=JMAX+1 REZ4150
KMAXA=KMAX+1 REZ4160
N6=N6/2 REZ4170
JSTR=JSTR/2 REZ4180
IF (NUMREZ.GT.NREZ) NREZ=NUMREZ REZ4190
NPLACE=NREZ-NUMREZ+2 REZ4200
C *** CALCULATE NEW ETI REZ4210
ETH=0. REZ4230
DO 530 K=2,KMAX REZ4240
ETH=ETH+AMX(K)*(AIX(K)+.5*(U(K)**2+V(K)**2)) REZ4250
530 CONTINUE REZ4260
C ***DIVIDE JPM(1) BY 2 TO GET NEW PEAK PRESSURE CELLS. REZ4270
DO 550 I=1,IMAX REZ4280
L=2*I REZ4290
IF (L.GT.IMAX) GO TO 540 REZ4300
JPM(I)=JPM(L)/2 REZ4310
GO TO 550 REZ4320
540 JPM(I)=0 REZ4330
550 CONTINUE REZ4340
IF (Y2.GT.(-1.)) GO TO 610 REZ4350
C *** SCALE EXISTING TRACER POINTS REZ4360
C REZ4370
C REZ4380
DO 560 J=1,JJ REZ4390
DO 560 I=1,II REZ4400
XP(I,J)=XP(I,J)/2. REZ4410
YP(I,J)=YP(I,J)/2. REZ4420
560 CONTINUE REZ4430
C *** REMOVE TRACER POINTS FROM EVERY OTHER CELL AND EVERY REZ4440
C OTHER ROW REZ4450
C REZ4460
C REZ4470
NMP=0 REZ4480
M=0 REZ4490
DO 570 J=1,JJ,2 REZ4500
M=M+1 REZ4510
L=0 REZ4520
DO 570 I=1,II,2 REZ4530
L=L+1 REZ4540
XP(L,M)=XP(I,J) REZ4550
YP(L,M)=YP(I,J) REZ4560
570 NMP=NMP+1 REZ4570
JTPB=1 REZ4580

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JPT=INT(FLOAT(JJ)/2.+.6)
ITPL=INT(FLOAT(II)/2.+.6)+1          REZ4590
                                         REZ4600
                                         REZ4610
                                         REZ4620
                                         REZ4630
                                         REZ4635
                                         REZ4640
                                         REZ4650
                                         REZ4660
                                         REZ4670
                                         REZ4680
                                         REZ4690
                                         REZ4700
                                         REZ4710
                                         REZ4720
                                         REZ4722
                                         REZ4724
                                         REZ4726
                                         REZ4730
                                         REZ4740
                                         REZ4750
                                         REZ4760
                                         REZ4770
                                         REZ4772
                                         REZ4774
                                         REZ4780
                                         REZ4790
                                         REZ4800
                                         REZ4810
                                         REZ4820
                                         REZ4830
                                         REZ4840
                                         REZ4850
                                         REZ4860-

```

C
 C
 C
 C
 C
 C
 *** INITIALIZE REMAINING TRACER POINT STORAGE AND
 *** PLACE NEW TRACER POINTS FIRST IN NEW CELLS ABOVE OLD
 GRID THEN IN NEW CELLS TO THE RIGHT OF OLD GRID.
 580 DO 600 J=JTPB,JPT REZ4650
 DO 600 I=ITPL,II REZ4660
 XP(I,J)=0. REZ4670
 YP(I,J)=0. REZ4680
 K=2*((J-1)*IMAX+I) REZ4690
 IF (AMX(K).EQ.0.) GO TO 590 REZ4700
 ICELL=2*I-1 REZ4710
 JCELL=2*J-1 REZ4720
 C
 C
 C
 *** PLACE NEW TRACER POINTS IN CELLS SO THEY LINE UP
 WITH EXISTING TRACER POINTS BY USING NPLACE WHICH
 IS A FUNCTION OF THE NUMBER OF REZONES PERFORMED.
 XP(I,J)=FLOAT(ICELL-1)+1./2.*NPLACE REZ4722
 YP(I,J)=FLOAT(JCELL-1)+1./2.*NPLACE REZ4724
 590 NMP=NMP+1 REZ4726
 600 CONTINUE REZ4730
 IF (J.GE.JJ) GO TO 610 REZ4740
 C
 *** GO BACK THROUGH LOOPS ADDING POINTS ON RIGHT SIDE OF
 OLD GRID. REZ4750
 C
 JTPB=JTP+1 REZ4760
 JPT=JJ REZ4770
 ITPL=1 REZ4772
 GO TO 580 REZ4774
 610 RETURN REZ4780
 C
 620 FORMAT (1H ////22H PROBLEM REZONED AT T=,1PE12.6,6X,5HCYCLEI4,6X,6REZ484)
 1HDX(1)=,E12.6//// REZ4790
 END REZ4800

C C SUBROUTINE ERROR ERR 10
 C C ERR 20
 C C ERR 30
 C C DIMENSION AMX(2502),AIX(2502),U(2502) ,V(2502) ,P(2502) , ERR 40
 1 X(52) ,XX(54) ,TAU(52) ,JPM(52) , ERR 50
 2 Y(102) ,YY(104) ,FLEFT(102), YAMC(102), SIGC(102), ERR 60
 3 GAMC(102), ERR 70
 4 PK(15), Z(150) , ERR 80
 5 XP(26,51),YP(26,51), ERR 90
 6 PL(204) ,UL(204) ,PR(204) , ERR 100
 7 RSN(52), RST(52), ERR 110
 8 CMXP(5) ,CMYP(5) ,IJ(5) ,JK(5) , ERR 120
 9 DX(52) ,DDX(54) ,DY(102) ,DDY(104) , ERR 130
 \$ SNB(52) ,STB(52) ,UK(52,3) ,VK(52,3) ,RHO(52,3) , ERR 140
 C C *** DIMENSIONED ARRAYS ERR 150
 C C *** Z-BLOCK IS SAVED ON TAPE. ERR 160
 COMMON Z ERR 170
 COMMON PK ERR 180
 COMMON YY, XX ERR 190
 COMMON DDX, DDY ERR 200
 COMMON AMX, AIX, U, V, P ERR 210
 COMMON TAU, JPM ERR 220
 COMMON UL, PL ERR 230
 COMMON XP, IP, CMXP, CMYP ERR 240
 C C *** NON-DIMENSIONED VARIABLES ERR 250
 COMMON AID, AMMV, AMMY, ANPY, AMUR, AMUT, AMVR, , ERR 260
 1AMVT, DELEB, DELER, DELET, DELM, DTODX, DXMIN, EAMMP, EAMPY, , ERR 270
 2E, ERDUMP, I, I3, IWS, J, K, KA, KB, , ERR 280
 3LL, MD, ME, MZT, NERR, NK, NPRINT, , ERR 290
 4NR, NRZ, NULLE, PIDTS, SIEMIN, SNR, SNT, STR, SOLID, , ERR 300
 5SUM, TESTRH, TWOP, URR, WS, WSA, WSB, WSC, WFLAGF, , ERR 310
 6WFLAGL, WFLAGP, , ERR 320
 C C *** THE FOLLOWING EQUIVALENCES MAKE AVAILABLE ERR 330
 C C X(0), Y(0), DX(0), DY(0) ERR 340
 C C ERR 350
 C C ERR 360
 C C EQUIVALENCE (XX(2), X(1)), (YY(2), Y(1)) ERR 370
 C C EQUIVALENCE (DDX(2), DX(1)), (DDY(2), DY(1)) ERR 380
 C C *** SPECIAL EQUIVALENCES FOR PH2 ONLY ERR 390
 C C ERR 400
 C C ERR 410
 C C EQUIVALENCE (UL,FLEFT), (UL(103),YAMC), ERR 420
 C C (PL,GAMC,PR), (PL(103),SIGC) ERR 430
 C C ERR 440
 C C *** SPECIAL EQUIVALENCES FOR PH3 ONLY ERR 450
 C C ERR 460
 C C EQUIVALENCE (UL,RSN), ERR 470
 1 (PL,RST), (P,UK), ERR 480
 2 (P(157),VK), (P(313),SNB), ERR 490
 3 (P(365),STB), (P(417),RHO) ERR 500
 C C ERR 510
 C C *** SPECIAL EQUIVALENCES FOR EDIT ERR 520
 C C ERR 530
 C C EQUIVALENCE (PR(1), IJ), (PR(6), JK) ERR 540
 C C ERR 550
 C C *** Z-STORAGE EQUIVALENCES ERR 560
 C C EQUIVALENCE (Z(1),PROB), (Z(2),CYCLE), ERR 570
 C C ERR 580

1(Z(3),DT),(Z(4),NUMSP),(Z(5),NRELPL),(Z(6),NDUMP7), ERR 590
 2(Z(7),ICSTOP),(Z(8),PIDY),(Z(9),TOPMU),(Z(10),RTMU), ERR 600
 3(Z(11),STK1),(Z(12),NUMREZ),(Z(13),ETH),(Z(14),UN14), ERR 610
 4(Z(15),RHINIT),(Z(16),PROJI),(Z(17),UN17),(Z(18),XMAX), ERR 620
 5(Z(19),NZ),(Z(20),NREZ),(Z(21),AMDM),(Z(22),UVMAX), ERR 630
 6(Z(23),UN23),(Z(24),PMIN),(Z(25),JSTR),(Z(26),DTNA), ERR 640
 7(Z(27),CVIS),(Z(28),STK2),(Z(29),STEZ),(Z(30),NC), ERR 650
 8(Z(31),UN31),(Z(32),NRC),(Z(33),IMAX),(Z(34),IMAXA), ERR 660
 9(Z(35),JMAX),(Z(36),JMAXA),(Z(37),KMAX),(Z(38),KMAXA) ERR 670
 EQUIVALENCE
 1(Z(39),BOTM),(Z(40),BOTMV),(Z(41),NUMSPT),(Z(42),CZERO), ERR 690
 2(Z(43),NUMSCA),(Z(44),PRLIM),(Z(45),PRDELT),(Z(46),PRFACT) ERR 700
 EQUIVALENCE
 1(Z(47),I1),(Z(48),I2),(Z(49),IPCYCL),(Z(50),TSTCP), ERR 720
 2(Z(51),RHOFIL),(Z(52),TARGV),(Z(53),N3),(Z(54),IVARDY), ERR 730
 3(Z(55),VT),(Z(56),NG),(Z(57),RTM),(Z(58),RTMV), ERR 740
 4(Z(59),UN59),(Z(60),N10),(Z(61),N11),(Z(62),GAMMA), ERR 750
 5(Z(63),TOPM),(Z(64),BOTMU),(Z(65),SN),(Z(66),TOPMV), ERR 760
 6(Z(67),PRYBOT),(Z(68),PRYTOP),(Z(69),PRXRT),(Z(70),CYCPH3), ERR 770
 7(Z(71),REZFCT),(Z(72),TARGI),(Z(73),PROJU),(Z(74),BBCUND), ERR 780
 8(Z(75),EVAP),(Z(76),ECK),(Z(77),NECYCL),(Z(78),II), ERR 790
 9(Z(79),JJ),(Z(80),NMP),(Z(81),Y2),(Z(82),EZPH1) ERR 800
 EQUIVALENCE
 1(Z(83),IVARDX),(Z(84),T),(Z(85),NMPPMAX),(Z(86),PMIN), ERR 820
 2(Z(87),INTER),(Z(88),TAYBOT),(Z(89),TAYTOP),(Z(90),IEMAP), ERR 830
 3(Z(91),MC),(Z(92),MR),(Z(93),MZ),(Z(94),MB) ERR 840
 EQUIVALENCE
 1(Z(95),REZ),(Z(96),NODUMP),(Z(97),UN97),(Z(98),UN98), ERR 860
 2(Z(99),UN99),(Z(100),EVAPM),(Z(101),EVAPEN),(Z(102),EVAPMU), ERR 870
 3(Z(103),EVAPMV),(Z(104),EZPH2),(Z(105),SNL),(Z(106),STL), ERR 880
 4(Z(107),TAXRT),(Z(108),IDNMAP),(Z(109),IPRMAP),(Z(110),ROEPS), ERR 890
 5(Z(111),RHINI),(Z(112),VINI),(Z(113),FINAL),(Z(114),IVMAP), ERR 900
 6(Z(115),RHOZ),(Z(116),ESA),(Z(117),ESEZ),(Z(118),ESB), ERR 910
 7(Z(119),ESCAPA),(Z(120),ESESP),(Z(121),ESESQ),(Z(122),ESES), ERR 920
 8(Z(123),ESALPH),(Z(124),ESBETA),(Z(125),ESCAP3),(Z(126),IUMAP), ERR 930
 9(Z(127),SS1),(Z(128),SS2),(Z(129),UMIN),(Z(130),SS4) ERR 940
 EQUIVALENCE
 1(Z(131),PRTIME),(Z(132),EOR),(Z(133),EOT),(Z(134),EOB), ERR 960
 2(Z(135),EMOR),(Z(136),DXF),(Z(137),DYF),(Z(138),RHOMIN), ERR 970
 3(Z(139),STAB),(Z(140),XIENRG),(Z(141),XKENRG),(Z(142),XTENRG), ERR 980
 4(Z(143),STT),(Z(144),DTMIN),(Z(145),TRNSFC),(Z(146),EMOT), ERR 990
 5(Z(147),JPROJ),(Z(148),CNAUT),(Z(149),BBAR),(Z(150),EMOB) ERR1000
 C ERR1010
 C ERR1020
 C ERR1030
 C END OF COMMON ERR1040
 C ERR1050
 C ERR1060
 C ERR1070
 IF (NERR.EQ.1) GO TO 120
 GO TO (10,20,30,40,50,60,70,80,90,100), NR
 10 WRITE (6,130) NK ERR1100
 . GO TO 110 ERR1110
 20 WRITE (6,140) NK ERR1120
 . GO TO 110 ERR1130
 30 WRITE (6,150) NK ERR1140
 . GO TO 110 ERR1150

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40      WRITE (6,160) NK          ERR1150
      GO TO 110                 EKR1170
50      WRITE (6,170) NK          ERR1180
      GO TO 110                 EKR1190
60      WRITE (6,180) NK          ERR1200
      GO TO 110                 EKR1210
70      WRITE (6,190) NK          ERR1220
      GO TO 110                 EKR1230
80      WRITE (6,200) NK          ERR1240
      GO TO 110                 EKR1250
90      WRITE (6,210) NK          ERR1260
      GO TO 110                 EKR1270
100     WRITE (6,220) NK         ERR1280
110     WRITE (6,230) I,J,K,(M,Z(M),Z(N),M=1,150) ERR1290
C       *** IF NR=1, ERROR IS IN INPUT DECK
C       IF(NR.EQ.1) GO TO 120    EKR1292
C       *** IF NR=5 AND NK=130, EDIT PRINT HAS JUST BEEN DONE. BY
C           SETTING ERDUMP=1., EDIT WILL DO A TAPE DUMP BUT NOT
C           ANOTHER PRINT.      EKR1294
C       IF (NR.EQ.5.AND..JK.EQ.130) ERDUMP=1.      EKR1296
NERR = 1          EKR1298
I3=I1            EKR1300
NPRINT=1          EKR1310
WFLAGL=1          EKR1315
NUMSPT=NODUMP7   EKR1320
CALL EDIT         EKR1330
120     CALL EXIT            EKR1340
C
C
130     FORMAT (1H1,5X,30H*** ERROR EXIT - SEE STATEMENT NUMBER ,I5,10H INERR1400
1 INPUT )        EKR1410
140     FORMAT (1H1,5X,30H*** ERROR EXIT - SEE STATEMENT NUMBER ,I5,10H INERR1420
1 SETUP )        EKR1430
150     FORMAT (1H1,5X,30H*** ERROR EXIT - SEE STATEMENT NUMBER ,I5,10H INERR1440
1 CDT )          EKR1450
160     FORMAT (1H1,5X,30H*** ERROR EXIT - SEE STATEMENT NUMBER ,I5,10H INERR1460
1 ES )           EKR1470
170     FORMAT (1H1,5X,30H*** ERROR EXIT - SEE STATEMENT NUMBER ,I5,10H INERR1480
1 EDIT )         EKR1490
180     FORMAT (1H1,5X,30H*** ERROR EXIT - SEE STATEMENT NUMBER ,I5,10H INERR1500
1 MAP )          EKR1510
190     FORMAT (1H1,5X,30H*** ERROR EXIT - SEE STATEMENT NUMBER ,I5,10H INERR1520
1 PH1 )          EKR1530
200     FORMAT (1H1,5X,30H*** ERROR EXIT - SEE STATEMENT NUMBER ,I5,10H INERR1540
1 PH3 )          EKR1550
210     FORMAT (1H1,5X,30H*** ERROR EXIT - SEE STATEMENT NUMBER ,I5,10H INERR1560
1 PH2 )          EKR1570
220     FORMAT (1H1,5X,30H*** ERROR EXIT - SEE STATEMENT NUMBER ,I5,10H INERR1580
1 REZONE)        EKR1590
230     FORMAT (//5X,6H    I=,I3,6H    J=I3,6H    K=I3//16X,7HZ-BLOCK//6X,EKR1600
115H REAL FORMAT ,5X,15H INTEGER FORMAT/2X,1HI,8X,4HZ(I),17X,4HZ(I),17X,4HZ(I)
2I)/(I4,2X,E15.6,5X,I15))      EKR1610
END             EKR1620
                                EKR1630-

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7. DICTIONARY

This section includes a description of the use and location of each of the variables in the program. The following terminology is used in the dictionary:

"Local"		Means name is local to subroutine (not in Blank Common).
"Local (c)"		Means name is in Blank Common (or equivalenced to a variable in Blank Common), but its value is never passed to another subroutine.
"Global"		Means name is in Blank Common (or equivalenced to a variable in Blank Common) and its value is passed from one routine to another.
= Z(N)		Means variable is equivalenced to a member of the Z-array, the first array in Blank Common. These variables are usually used in setting up and restarting.
ADDVL	Local	Used in SETUP. Used in finding volume of cells containing sphere-boundary.
AID	Local (c)	Used in EDIT in calculation of crater depth.
AIX	Global	Specific internal energy in a cell. (IMAX by JMAX array.)
ALE	Constants	Used in MAP. This array has alphabetic characters for pressure, density, velocity, and energy maps. (Defined in DATA statement.)
AMDM	= Z(21)	INPUT parameter. A cell with compression > AMDM is considered solid. Usual value: 0.95 to 0.99. Used in ES in testing whether to allow negative pressures (tensions). Used in INPUT to calculate SOLID = AMDM * RHOZ, which is used in CNT and PH3.
AMMP	Local	Used in PH2. Mass moving across right boundary of a cell. (See Appendix B)

AMMU	Local	Used in PH2. Radial momentum transported across the bottom boundary of a cell. (See Appendix B)
AMMV	Local ^(C)	Used in PH2. Axial momentum transported across the bottom boundary of a cell. (See Appendix B)
AMMVY	Local ^(C)	Used in PH2. Amount of mass moving across bottom of a cell. (See Appendix B)
AMPY	Local ^(C)	Used in PH2. Amount of mass moving across top of a cell. (See Appendix B)
AMUR	Local ^(C)	Used in PH2. Radial momentum transported across right boundary of a cell. (See Appendix B)
AMUT	Local ^(C)	Used in PH2. Radial momentum transported across top boundary of cell. (See Appendix B)
AMVR	Local ^(C)	Used in PH2. Axial momentum transported across right boundary of a cell. (See Appendix B)
AMVT	Local ^(C)	Used in PH2. Axial momentum transported across top boundary of a cell. (See Appendix B)
AMX	Global	Mass in a cell. (IMAX by JMAX array.)
AREAFC	Local ^(C)	Used in SETUF. Area of a cell-face. Used in setting up a sphere. Equivalenced to DELEB.
B	Local	Used and calculated in PH3
BBAR	= Z(149)	Used in CDT. An INPUT parameter used in local sound-speed calculation whose value depends on the kind of material. (Local sound-speed is approximated as $C_0 + (BBAR) \cdot \sqrt{P(K)}$.)
BBOUND	= Z(74)	Calculated in PH3. Printed in EDIT under "Plastic-Work." Total work done by the plastic stresses.
BOTM	= Z(39)	Calculated in PH2. Printed in EDIT. Total mass lost out bottom of grid.
BOTMU	= Z(64)	Calculated in PH2. Printed in EDIT. Total radial-momentum lost out bottom of grid.

BOTMV	= Z(40)	Calculated in PH2. Printed in EDIT. Total axial-momentum lost out bottom of grid.
CMXP	Local ^(C)	Used and calculated in EDIT for printing the centimeter
CMYP	Local ^(C)	coordinates of the tracer points.
CNAUT	= Z(148)	Used in CDT, INPUT. Approximate sound-speed of material; calculated in INPUT as
		$C_0 = \sqrt{\frac{ESCAPA}{RHOZ}} = \sqrt{A/\rho}$
CRAD	Local ^(C)	Used in EDIT for printing radii of crater depths. Equivalenced to UL array.
CVIS	= Z(27)	INPUT parameter. Used to describe the bottom boundary-condition. Used in PH1, PH2, PH3. Bottom boundary is transmittive when CVIS = -1., reflective when CVIS = 0.
CYCLE	= Z(2)	Used in INPUT, SETUP, CDT, EDIT. Cycle number (an integer value in floating point form).
CYCPH3	= Z(70)	Used in MAIN and PH3. INPUT parameter: Number of times to subcycle PH3. If value is -1., PH3 is omitted.
CZERO	= Z(42)	INPUT parameter. Value of Y_0 for yield strength calculation. Used in PH3. (See STRENG)
DDX	Global	An array equivalenced to the DX array such that DDX(1) = DX(0).
DDY	Global	An array equivalenced to the DY array such that DDY(1) = DY(0).
DELEB	Local ^(C)	Used in PH2. Total energy associated with mass transported across bottom boundary of a cell. (See Appendix B)
DELER	(Local ^(C))	Used in PH2. Total energy associated with mass transported across right boundary of a cell. (See Appendix B)
DELETE	Local ^(C)	Used in PH2. Total energy associated with mass transported across top boundary of a cell. (See Appendix B)

DELI	Local	Used in PH2, PH3. Change of specific internal energy of a cell.
DELM	Local ^(c)	Used in PH2 for total mass moving into or out of a cell.
DELU	Local	Used in PH2, PH3. Change of radial velocity of a cell.
DELV	Local	Used in PH2, PH3. Change of axial velocity of a cell.
DMIN	= Z(24)	INPUT parameter. Allowable relative error in energy sum. If error is > DMIN then calculation is terminated. Used in EDIT. If everything is working right you should be able to use 10^{-3} for DMIN.
DSCALE	Local	Used in MAP as linear scale factor for compression map.
DT	= Z(3)	Time step. Calculated in CDT. Used in SETUP, EDIT, PH1, PH2 and PH3.
DTFACT	Local	Used in PH3 in calculating a variable time step when subcycling the PH3 calculations.
DTMIN	= Z(144)	INPUT parameter. Used in CDT. After STAB = FINAL, if DT < DTMIN execution is stopped.
DTNA	= Z(26)	DT from previous time cycle. Used in INPUT, CDT, EDIT, REZONE and PH1.
DTNOW	Local	Used in EDIT. Used for saving DT when calling CDT to recalculate pressures after a REZONE.
DTODX	Local ^(c)	Used in PH2 for DV/DX.
DTODY	Local	Used in PH2 for DT/DY.
DTSTR	Local	Used in PH3. DT for recycling through PH3.
DUODX	Local	Used in PH3. DU/DX.
DUODY	Local	Used in PH3. DU/DY.
DVODX	Local	Used in PH3. DV/DX

DVODY	Local	Used in PH3. DV/DY.
DX	Global	The radial dimension of cells. Equivalenced to DDX such that DDX(1) = DX(0).
DXF	= Z(136)	An INPUT parameter used to calculate the DX array if the radial dimension of the cells is uniform.
DXSUM	Local	Used in SETUP and REZONE to find cell dimensions of packages when DX is not constant.
DXYMIN	Local ^(c)	Used in CDT. Minimum (DX, DY) of a cell. Used in calculation of SRATIO and DT.
DY	Global	The axial-dimension of cells. Equivalenced to DDY so that DDY(1) = DY(0).
DYF	= Z(137)	INPUT parameter. DY of all cells, if DY is constant.
DYSUM	Local	Used in SETUP and REZONE to find cell dimensions of packages when DY is not constant.
E	Local ^(c)	Used in REZCNE, PH1, and PH3. Temporary storage for energy calculations.
EAMMP	Local ^(c)	Used in PH2. Specific internal energy of mass moving across right edge of cell.
EAMPY	Local ^(c)	Used in PH2. Specific internal energy of mass moving across top of cell.
ECK	= Z(76)	Used in EDIT. Relative error in energy sum. If $ ECK > DMIN$, execution is stopped.
EMOB	= Z(150)	Calculated in PH2. Printed in EDIT. Energy change out of bottom of mesh.
EMOR	= Z(135)	Calculated in PH2. Printed in EDIT. Energy change out right side of mesh.
EMOT	= Z(146)	Calculated in PH2. Printed in EDIT. Energy change out of top of mesh.
ENERGY	Local	Used in PH2 to sum energy of cells.
ENGY	Local	Used in PH2 as temporary storage for energy of a cell.

EOB	= Z(134)	Calculated in PH1. Printed in EDIT. Energy change due to work done at bottom boundary.
EOR	= Z(132)	Calculated in PH1. Printed in EDIT. Energy change due to work done at right boundary.
EOT	= Z(133)	Calculated in PH1. Printed in EDIT. Energy change due to work done at top boundary.
ERDUMP	Local (c)	Used in EDIT and ERROR. Flags EDIT to stop execution because ERROR has been called.
ESA	= Z(116)	INPUT parameter. Value of "a" in equation of state. Used in ES. (= $\gamma - 1$ when using perfect gas equation of state.)
ESALPH	= Z(123)	INPUT parameter. Value of " α " in equation of state. Used in ES.
ESB	= Z(118)	INPUT parameter. Value of "b" in equation of state. Used in ES.
ESBETA	= Z(124)	INPUT parameter. Value of " β " in equation of state. Used in ES.
ESCAPA	= Z(119)	INPUT parameter. Value of "A" in equation of state. Used in ES.
ESCAPB	= Z(125)	INPUT parameter. Value of "B" in equation of state. Used in ES.
ESCLE	Local	Used in MAP as a logarithmic scale factor for energy map.
ESES	= Z(122)	INPUT parameter. Value of ES in equation of state. Used in ES.
ESESP	= Z(120)	INPUT parameter. Value of ES' in equation of state. Used in ES.
ESESQ	= Z(121)	INPUT parameter. ESESQ is usually equal to ESESP. It is used to test whether a cell should be considered hot or cold in free-surface treatment. Used in CDT and PH2.

ESEZ	= Z(117)	INPUT parameter. Value of "E _o " in equation of state. Used in ES.
ESUM	Local	Used in EDIT to sum energy and calculate relative error of energy sum.
ETA	Local	Used and calculated in ES. = ρ/ρ_0 .
ETH	= Z(13)	Theoretical value of total energy in the mesh. Used in SETUP, EDIT, REZONE, PH1, PH2, PH3. Calculated in SETUP initially; in PH2 thereafter. It is redefined in REZONE.
EVAP	= Z(75)	INPUT parameter. Used in PH2. Any cell with density less than EVAP times initial density of "projectile" is "evaporated" and its energy subtracted from theoretical energy of system. (10^{-3} to 10^{-8} are appropriate values.)
EVAPEN	= Z(101)	Calculated in PH2 and CDT. Printed in EDIT. Sum of energy lost through "evaporation" described under EVAP. Adjusted in CDT when "evaporating" energy of isolated cells. Initialized in SETUP. Equivalenced to SIESPH in SETUP.
EVAPM	= Z(100)	Calculated in PH2. Printed in EDIT. Sum of mass lost through "evaporation" described under EVAP. Used in PH2 and CDT when "evaporating" mass of isolated cells. Initialized in SETUP. Equivalenced to RHOSPH in SETUP.
EVAPMU	= Z(102)	Calculated in PH2. Printed in EDIT. Sum of radial momenta lost through "evaporation." Used in PH2 and CDT when "evaporating" momentum of isolated cells. Initialized in SETUP. Equivalenced to VINSPH in SETUP.
EVAPMV	= Z(103)	Calculated in PH2. Sum of axial momenta lost through "evaporation". Printed in EDIT. Used in PH2 and CDT when "evaporating" momentum of isolated cells. Initialized in SETUP. Equivalenced to RHOOUT in SETUP.

EZPH1	= Z(82)	Energy gained through setting negative internal energies to zero in PH1. Printed in EDIT.
EZPH2	= Z(104)	Calculated in PH2. Sum of specific internal energy fluxes less than SIEMIN and negative internal energies set to zero. Printed in EDIT.
FINAL	= Z(113)	INPUT parameter. Maximum value of stability fraction (STAB). If FINAL = 0; the stability fraction will be constant. Used in CDT.
FLEFT	Local (c)	Used in PH2. Radial momentum of mass moving across left side of cell. Equivalenced to UL array. (See Appendix B)
PLOTMA	Local	Used in MAP.
FRX	Local	Used in PH2 for moving tracer-points.
FRY	Local	Used in PH2 for moving tracer-points.
GAMC	Local (c)	Used in PH2. Mass moving across left side of cell. Equivalenced to PL and PR arrays. (See Appendix B)
GAMMA	= Z(62)	Calculated value of GAMMA = ESA +1. Calculated in INPUT. Used in CDT.
HOOP	Local	Used in PH3. Hoop stress.
I	Local (c)	Used in most subroutines as index in radial direction.
IAID	Local	Used in EDIT in crater depth calculation.
ICELL	Local	Used in REZONE when placing tracer points in new cells.
ICP3	Local	Used in PH3: = INT(CYCPH3).
ICSTOP	= Z(7)	INPUT parameter. Used in EDIT. Execution stops on ICSTOP cycle when stopping on cycles rather than time.
IDL	Local	Used in MAP. Number of columns in maps. On cycle 0, IDL = IMAX; otherwise IDL = II.

IDNMAP	= Z(103)	
IEMAP	= Z(90)	
IPRMAP	= Z(109)	
IUMAP	= Z(116)	
IVMAP	= Z(114)	
II	= Z(78)	Defined in INPUT. Used in MAP to specify the number of symbols to be used in the density, energy, pressure, u-velocity, and v-velocity maps, respectively.
IJ	Local (c)	Used in REZONE, EDIT, and SETUP. The number of tracer points in each row.
IK	Local	Used in EDIT. Used to identify which column a tracer point originated in. Equivalenced to PR(l) in EDIT.
IKK	Local	Used in PH3, = IK + 1.
ILIM1	Local	Used in MAP as index for printing values of symbols.
ILIM2	Local	See ILIM1.
IMAX	= Z(33)	INPUT parameter. Number of columns in mesh. IMAX must be an even number if grid is to be rezoned with the exception that IMAX = 1 for a 1-D problem. Used in SETUP, CDT, REZONE, EDIT, PH1, PH2, and PH3.
IMAXA	= Z(34)	IMAX + 1. Used in SETUP and REZONE.
INTER	= Z(87)	INPUT parameter. If INTER ≠ 0, EDIT will print after CDT, PH1 and PH3. If INTER = 99, in addition to extra EDIT prints, stresses are printed in PH3. (LOTS of printing.) If INTER = 7, energy totals are printed in PH2 in addition to the extra EDIT prints. Used in MAIN, EDIT, PH1 and PH2 and PH3.
INTMA	Local	Used in MAP.
IP	Local	Used in EDIT. The column a tracer point is in.
IPCYCL	= Z(49)	INPUT parameter. Used in EDIT. The number of cycles between EDIT prints when printing on cycles rather than time.
IPRT	Local	Used in REZONE. Number of columns in projectile after rezoning.

ISPHMX	Local	Used in SETUP. I-index of right-most column which contains sphere material.
ITPL	Local	Used in REZONE for adding tracer-points in added cells.
ITRT	Local ^(C)	Used in REZONE. Number of columns in target after rezoning.
IVARDX	= Z(83)	Used in SETUP. Flag for variable radial dimension of cells.
IVARDY	= Z(54)	Used in SETUP. Flag for variable axial dimension of cells.
IWS	Local ^(C)	Used as local index in INPUT, SETUP, CDT, EDIT, PH2 and PH3.
IX	Local	Used as index in PH2 for tracer-point movement.
IY	Local	Used as index in PH2 for tracer-point movement.
Il	= Z(47)	INPUT parameter. Il is used to limit calculation in radial direction to "active mesh." Beyond Il nothing is yet disturbed from initial conditions. Il is specified initially as (2 + the column-number of the last column in which there is a non-zero velocity or internal energy). However, Il is never larger than IMAX. Il is increased automatically as inactive cells become active. If IMAX = 1, then Il = 1. Used in CDT, EDIT, REZONE, PH1, PH2 and PH3.
I2	= Z(48)	INPUT parameter. Like Il but for axial-disturbance-limit. I2 is specified initially as (2 + the number of the upper-most row in which there is a non-zero velocity or internal energy). I2 is increased automatically as inactive cells become active. However, I2 is never larger than JMAX. Used in SETUP, CDT, EDIT, REZONE, PH1, PH2, PH3.
I3	Local ^(C)	Used in EDIT as a flag for "short" or "long" prints.
J	Local ^(C)	Used as row-index in most subroutines.

JA	Local	Used in SETUP to calculate J-index of top of sphere.
JB	Local	Used in SETUP to calculate J-index of bottom of sphere.
JCELL	Local	Used in REZONE when placing tracer points in added cells.
JCENTR	Local	Used in SETUP. J-index of row just below center of sphere.
JDL	Local	Used in MAP. Number of rows in maps. On cycle 0, JDL = JMAX; otherwise, JDL = I2.
JFILA	Local	Used in REZONE. The J-index of the row immediately below the target.
JFILB	Local	Used in REZONE. The J-index of the row immediately above the projectile.
JFLAG	Local	Used in PH3. Used in connection with JFM for deciding where to stop calculating stresses.
JINTL	Local	Used in CDT in defining JPM array.
JJ	= Z(79)	Used in REZONE, EDIT and SETUP. Number of tracer points in each column.
JK	Local (C)	Used in EDIT. Used to identify which row a tracer point originated in. Equivalenced to PR(6).
JMAX	= Z(35)	INPUT parameter. Number of rows in mesh. JMAX must be an even number if grid is to be rezoned. Used in SETUP, CDT, EDIT, REZONE, PH1, PH2, PH3.
JMAXA	= Z(36)	JMAX + 1. Used in SETUP and REZONE.
JMP1	Local	Used in REZONE. Limit on do-loop, = JMAX/2 + 1.
JP	Local	Used as an index in CDT. Used in EDIT. The row a tracer point is in.
JPA	Local	Used in REZONE. The J-index of the top row of projectile.
JPB	Local	Used in REZONE. The J-index of the bottom row of projectile.

JPM	Global	Calculated in CDT; used in PH3. Initialized, adjusted and saved on tape in SETUP, INPUT, EDIT and REZONE. JPM(I) is J-index of cell with local maximum pressure in column I.
JPROJ	= Z(147)	INPUT parameter. Usually the J-index of top cell in projectile. Used in SETUP and EDIT. Adjusted in REZONE. The zero point in the crater depth calculation. A division for printout of total energies, mass and momenta.
JRADA	Local	Used in SETUP. The J-index of the top cell on the axis containing a part of the sphere.
JRADB	Local	Used in SETUP. The J-index of the bottom cell on the axis containing a part of the sphere.
JSPHET	Local	Used in SETUP as index in placing sphere.
JSPHTP	Local	Used in SETUP as index in placing sphere.
JSTR	= Z(25)	INPUT parameter. When active-grid gets to JSTR in J direction, stress calculations begin and negative pressures are permitted. JSTR needs to be large enough so that a shock can become well established before stress calculations begin and negative pressures are allowed. Otherwise, meaningless perturbations are calculated in material which is still at rest. Used in PH3, CDT and REZONE.
JTA	Local	Used in REZONE as index.
JTB	Local	Used in REZONE as index.
JTPB	Local	Used in REZONE. Index for "weeding out" and adding tracer points.
JPTT	Local	Used in REZONE. See JTPB.
K	Local ^(c)	Used as cell-index in all subroutines.
KA	Local ^(c)	Used as index in CDT and PH2.
KB	Local ^(c)	Used as index in CDT.

KK	Local	Used as index in EDIT to remove tracer points from empty cells.
KMAX	= Z(37)	Calculated in SETUP (IMAX*JMAX+1). Used in PH3, SETUP, EDIT, REZONE. Largest value of K (cell-index).
KMAXA	= Z(38)	Calculated in SETUP (KMAX+1). Used in INPUT, SETUP, EDIT and REZONE.
KSPACE	Local	Used in EDIT for spacing printed output.
L	Local	Used as index in EDIT, INPUT, PH2, PH3, REZONE.
LA	Local	Used as index in PH2.
LB	Local	Used as index in PH2.
LJD	Local	Used as index in PH2 and PH3.
LL	Local ^(c)	Used as index in PH1, PH2 and PH3.
LOCA	Local	Used in EDIT and PH3 in assigned GO TO statements.
LOCB	Local	Used in EDIT in assigned GO TO statements.
M	Local	Used as index in SETUP, EDIT, PH2, REZONE, PH3, ERROR.
MA	Local	Used in MAP to specify symbol to be printed for each cell.
MASS	Local	Used in PH2 for temporary storage of the mass of a cell.
MAXEXP	Local	Used in MAP to define logarithmic scale factor for each map.
MB	= Z(94)	Used and calculated in SETUP. The J-index of the bottom row of projectile.
MC	= Z(91)	Used and calculated in SETUP. The J-index of the top row of projectile.
MD	Local ^(c)	Used in SETUP. Flag indicating whether or not there is a target.

ME	Local ^(c)	Used and calculated in SETUP. The number of columns in the target. (If target extends beyond mesh, ME = IMAX.)
MNEXP	Local	Used in MAP to define logarithmic scale factor for each map.
MR	= Z(92)	Used and calculated in SETUP. The number of columns in the projectile.
MSLAVE	Local	Used in PH2 as storage for slaved-cell index when transporting mass across top edge of cell.
MZ	= Z(93)	Used and calculated in SETUP. The J-index of the bottom row of the target.
MZT	Global	Defined in INPUT (MZT = 150). Used in SETUP and EDIT. The number of Z-block words.
N	Local	Used as an index in PH3, PH1, PH2, REZONE and EDIT. In SETUP, N is the J-index of the top row of the target.
N3	= Z(53)	Defined in SETUP. Used in SETUP, EDIT, INPUT in reading and writing tapes. = 0 if there are no tracer points; = 1 if tracer points are used.
N6	= Z(56)	INPUT parameter. Used in ES. Negative pressures are allowed in cells above J = N6 after active-J reaches JSTR value. The value of N6 is reset in REZONE. N6 = 0 allows negative pressures everywhere. On the other hand, to make sure that negative pressures are always set to zero give N6 a very large value (many times as large as JMAX) since in REZONE N6 is cut in half in order to keep it at the same distance (in cm.) from the bottom of the grid.
N10	Global	Used in CDT to identify I-index of cell which controls DT.
N11	Global	Used in CDT to identify J-index of cell which controls DT.

NC	= Z(30)	Cycle number. Set initially to -1 in INPUT. Incremented thereafter in CDT.
NDUMP7	= Z(6)	INPUT parameter. Used in EDIT to control frequency of tape dumps. A tape dump will occur every (NDUMP7) EDIT prints.
NECYCL	= Z(77)	Defined and printed in EDIT. The cycle number associated with the largest relative error in the energy sum.
NERR	Global	Used in ERROR as exit flag. Prevents ERROR from being called more than once during a single run.
NFRELP	= Z(5)	INPUT parameter. Used in EDIT to control frequency of "long" prints. A "long" print will occur every (NFRELP) "short" prints.
NIMAX	Local	Used in REZONE as storage for IMAX/2 when IMAX > 1. NIMAX = 1 when IMAX = 1.
NIMAX1	Local	Used in REZONE as storage for NIMAX + 1.
NJMAX	Local	Used in REZONE as storage for JMAX/2.
NJMAX1	Local	Used in REZONE as storage for NJMAX + 1.
NK	Global	Used in PH2, PH3, EDIT, INPUT, CDT, REZONE and ERROR. Tells which statement of a subroutine caused ERROR to be called.
NKA	Local	Used in PH3 as index.
NKB	Local	Used in PH3 as index.
NMP	= Z(80)	Number of tracer points in use. Used in INPUT, SETUP, REZONE, EDIT and PH2. Initially calculated in SETUF; recalculated in REZONE.
NMPMAX	= Z(85)	INPUT parameter. Maximum number of tracer points to be generated. If fewer points are needed, NMP will have the number actually generated. NMPMAX must not be larger than the number allowed in dimensions of XP and YP. Used in SETUP and REZONE.

NN	Local	Used as index in PH3 and PH2.
NODUMP	= Z(96)	INPUT parameter. Used in EDIT. When NODUMP = 1, no tape dumps are made except on cycle 0. Allows user to restart a problem without writing on the restart tape.
NPLACE	Local	Used in REZONE for lining up added tracer points with original ones.
NPRINT	Global	Used in MAIN, CDT and EDIT. Prevents DT and PRTIME from being altered on intermediate prints. Also, NPRINT = 1 flags EDIT to print and check energy discrepancy.
NR	Global	Used in PH2, EDIT, SETUP and CDT to identify which subroutine called ERROR. Used in ERROR for printing error message.
NRC	= Z(32)	Used in PH1 and PH2 in advancing active grid.
NREZ	= Z(20)	Defined in SETUP. Equals maximum number of rezones allowed. Used in REZONE to line up new tracer points with those already in grid. Used in EDIT to determine the original I and J of each tracer point.
NRT	Local	Used in PH1 and PH2 in advancing active grid.
NRZ	Global	Initialized in SETUP. Equals number of rezones so far performed. Used in EDIT for printout of 1-D problems and for determining the original I and J of each tracer point.
NSLAVE	Local	Used in PH2 as storage for slaved-cell index when transporting mass across right edge of cell.
NULLE	Global	Equivalenced to RHOW in CDT and ES.
NUMREZ	= Z(12)	INPUT parameter. Initially equals number of rezones allowed in one run. Diminished by one after each rezone. Used in EDIT and REZONE.

NUMSCA	= Z(43)	INPUT parameter. Number of times the print interval is to be rescaled. Used in EDIT. See PRDELT for further details.
NUMSP	= Z(4)	Used in EDIT to count the number of "short" prints since the last "long" print.
NUMSPF	= Z(41)	Used in EDIT to count the number of prints (short and long) since the last tape dump.
NZ	= Z(19)	Defined and used in EDIT for 1-D problems. NZ = 4**NRZ. After rezoning the grid NZ is used to scale the values printed by EDIT for the total mass, energy and momentum.
P	Global	Cell-pressure. IMAX by JMAX array. Calculated in ES. Used by PH1. The P-storage space is used for UK, VK, and RHO storage in PH3. The P-array is initialized at the beginning of PH3.
P1 P2 P3 P4 P5 P6 P8 P9 P12	Local Local Local Local Local Local Local Local Local	Used in ES as storage for various terms in the pressure equations.
PABOVE	Local	Used in PH1 as storage for pressure at top of cell.
PBLO	Local	Used in PH1 as storage for pressure at bottom of cell.
PIDTS	Local ^(C)	Defined and used in PH1 as $1. / (\pi * DT * DY)$. Defined and used in PH2 as $1. / (\pi * DT)$.
PIDY	= Z(8)	Defined in INPUT: = π . Used in REZONE, SETUP, PH1, PH2, and PH3.
PK	Global	Used in SETUP and INPUT for defining input parameters. (See Appendix A.) PK(3) used in EDIT to signal a "long" or "short" print on first cycle of a restart run.

PL	Local ^(c)	Used in PH1 for saving pressures on left side of cell. Used in EDIT for crater depth printout. Equivalenced in standard OIL-RPM as follows: PL = RST (for PH3) PL = PR = GAMC (for PH2) PL(103) = SIGC (for PH2)
PMIN	= Z(86)	Used as a pressure cut-off. Calculated and printed in CDT as $(c_0) \cdot (p_0) \cdot (U_{min})$. Initially defined in INPUT as 10^6 .
PR	Local ^(c)	Used in INPUT and EDIT for temporary storage.
PRAMOA	Local	Printed and calculated in EDIT. The positive radial momentum above JPROJ. Equivalenced to PR(8) in EDIT only.
PRAMOB	Local	Printed and calculated in EDIT. The positive radial momentum below JPROJ. Equivalenced to PR(16) in EDIT only.
PRDELT	= Z(45)	INPUT parameter. Gives the initial time interval between EDIT prints. There are five parameters which control printing frequency: PRDELT, IPCYCL, PRLIM, PRFACT, and NUMSCA. If the user is printing on time (PRDELT $\neq 0.$ and IPCYCL = 0.), DT will be adjusted so that a print will occur exactly every PRDELT seconds. If the user is printing on cycles (PRDELT = 0., IPCYCL $\neq 0.$), a print will occur every IPCYCL cycles. PRLIM, PRFACT and NUMSCA are used to increase the print interval. PRLIM is the time (or cycle) at which PRDELT (or IPCYCL) and PRLIM are multiplied by PRFACT. The new value of PRLIM establishes the next time (or cycle) when the print interval will be rescaled. This process continues at most NUMSCA times. EXAMPLE: You wish to print every 1×10^{-8} sec. until you reach 1×10^{-7} sec., then every 1×10^{-7} sec. until 1×10^{-6} sec. and every 1×10^{-6} sec. thereafter: PRDELT = $1. \times 10^{-8}$ PRFACT = 10. PRLIM = $1. \times 10^{-7}$ NUMSCA = 2.

PRFACT	= Z(46)	INPUT parameter. Used in EDIT as a factor for rescaling PRDELT, IPCYCL, and PRLIM when PRLIM-time or cycle is reached. (See PRDELT.) Should be > 1.
PRLIM	= Z(44)	INPUT parameter: time or cycle at which to rescale PRDELT (or IPCYCL) and PRLIM by PRFACT. (See PRDELT.)
PRMAS	Local (C)	Used and calculated in EDIT. Total mass below JPROJ. Equivalenced to PR(12) in EDIT only.
PRMV	Local (C)	Used and calculated in EDIT. Total axial momentum below JPROJ. Equivalenced to PR(12) in EDIT only.
PRMVP	Local (C)	Used and calculated in EDIT. Total positive axial momentum below JPROJ. Equivalenced to PR(14) in EDIT only.
PROB	= Z(1)	INPUT parameter. Identifying problem number. Used in EDIT and INPUT.
FROJI	= Z(16)	INPUT parameter. Initial specific internal energy of projectile. Used in SETUP and REZONE.
PROJU	= Z(73)	INPUT parameter. Initial radial velocity of projectile. (Usually = 0) Used in SETUP and REZONE.
PROPI	Local	Calculated and used in EDIT. For 1-D problems the totals for energy, mass, momentum per unit area are printed. (i.e., they are divided by 4** (Number of rezones)) and stored in PROPI for printing.
PRR	Local	Used in PH1 as temporary storage of pressure and pressure averages.
PRTIME	= Z(131)	Initially set to PRDELT in INPUT. Thereafter calculated in EDIT. When T = PRTIME, it is time to print.
PRXRT	= Z(69)	INPUT parameter. The outer radius of projectile (in cms.). PRXRT must be at a cell-boundary. Used in SETUP and REZONE.
PRYBOT	= Z(67)	INPUT parameter. Y-value of bottom of projectile (in cms.). PRYBOT should be at a cell-boundary. If no "projectile" is to be generated, PRYBOT should be set to -1. Used in SETUP and REZONE.

PSCLE	Local	Used in MAP as a logarithmic scale factor for the pressure maps.
PTEMP	Local	Used in CDT when calculating JFM array (the maximum pressure location in each column).
PW	Local	Used in PH3 to calculate plastic work when INTER = 99.
RADIUS	= PK(12) = Z(162)	INPUT parameter. Radius of sphere (in cms.). The radius need not be a multiple of DX. Used in SETUP. Equivalenced to PK(12) in SETUP.
RAMOMA	Local	Printed and calculated in EDIT. Total radial momentum above JPROJ. Equivalenced to PR(7) in EDIT only.
RATIO	Local	Used in CDT in calculation of DT. Ratio of $(DX, DY)_{min}$ to $(U, V, \text{local sound speed})_{max}$.
RC	Local	Used and calculated in PH1 as distance from axis to center of a cell.
RELERR	Local	Used in EDIT for storing and printing maximum relative error in the energy sum.
REZ	= Z(95)	Flag defined in PH2 and used in EDIT. Signals when the REZONE subroutine should be called. (The rezone flag is turned on when material begins to flow out through transmittive boundaries. In REZONE each set of four cells in the mesh is made into one cell. The new mass is the sum of masses in the four original cells. Momentum and total energy are conserved but in so doing some kinetic energy is changed to internal. (The result is that rezoning has a stabilizing influence.) When all permitted rezones have been done, material is allowed to flow out through transmittive boundaries and the mass and energy are lost from the system.
REZFCT	= Z(71)	INPUT flag for rezoning. If = 1., the grid is rezoned (NUMREZ) times. If = 0., no rezoning is done. Tested in PH2 and EDIT.

RHINI	= Z(111)	INPUT parameter. Initial density of projectile. Used in SETUP and REZONE. In PH2 it is used to determine whether material should be evaporated. (See EVAP)
RHINIT	= Z(15)	INPUT parameter. Initial density of target. Used in SETUP and REZONE.
RHO	Local ^(C)	Used in PH3 for temporary storage of cell density.
RHOFIL	= Z(51)	INPUT parameter. Initial density of filler material between the projectile and target. Used in SETUP and REZONE.
RHOMIN	= Z(138)	INPUT parameter. Cells with $\rho < \text{RHOMIN}$ are by-passed in calculation of DT.
RHOOUT	= Z(103)	INPUT parameter. Used in SETUP. In cells containing sphere boundary RHOOUT is the density of material outside sphere. Equivalenced to Z(103) and EVAPMV in SETUP.
RHOSPH	= Z(100)	INPUT parameter. Used in SETUP as the initial density of sphere. Equivalenced to Z(100) and EVAPM in SETUP.
RHOW	Global	Density of cell. Calculated in CDT, used in ES. Equivalenced to NULLE in CDT and ES.
RHOZ	= Z(115)	INPUT parameter. Normal density. Used in INPUT, CDT, ES, EDIT, PH2 and PH3.
ROEPS	= Z(110)	INPUT parameter. Round-off epsilon used in calculating cutoffs. Used in CDT to calculate UMIN. $UMIN = (\text{ROEPS})(\text{maximum } u \text{ or } v)$ Used in SETUP, EDIT and PH2.
RR	Local	Used and calculated in PH1. Distance (cms.) from axis to center of cell on the right.
RTM	= Z(57)	Calculated in PH2. Printed in EDIT. Total mass lost out right side of grid.

RTMU	= Z(10)	Calculated in PH2. Printed in EDIT. Total radial-momentum lost out right side of grid.
RTMV	= Z(58)	Calculated in PH2. Printed in EDIT. Total axial-momentum lost out right side of grid.
SAVEK	Local	Used and calculated in PH2. Factor used in calculation of energy fluxes across right and top boundaries of cells on reflective boundaries.
SIEMIN	Global	Used in MAP, PH2. Calculated in CDT. SIE cut-off value = $(U_{MIN})^2$.
SIENEW	Local	Used and calculated in PH2. New value of specific internal energy.
SIESPH	= Z(101)	INPUT parameter. Initial value of specific internal energy of sphere. Equivalenced to Z(101) and EVAPEN in SETUP.
SIGC	Local ^(C)	Used in PH2 for energy carried by mass moving across left side of cell. Equivalenced to PL(103). (See Appendix B.)
SIGMU	Local	Used in PH2 for radial momentum moving across cell-boundaries.
SIGMV	Local	Used in PH2 for axial momentum moving across cell-boundaries.
SN	= Z(65)	INPUT flag: When = 0. negative internal energy is to be set to 0. When = 1. negative internal energy is to be left alone. Used in PH1 and PH2.
SNB	Local ^(C)	Used in PH3 for normal stress at bottom of a cell. Equivalenced to P(313).
SNL	= Z(105)	Used in PH3 for normal stress at left of a cell.
SNLX	Local	Used in PH3. = SNL * X(I-1).
SNR	Local ^(C)	Used in PH3 for normal stress at right of a cell. (= S_{11} at right.)
SNT	Local ^(C)	Used in PH3 for normal stress at top of a cell. (= S_{22} at top.)

SOLID	Global	Calculated in INPUT as (RHOL * AMDM). Used in PH2, PH3 and CDT.
SRATIO	Local	Used in CDT to calculate DT. The smallest ratio of minimum cell dimension to maximum velocity.
SS1	= Z(127)	Calculated in INPUT. Used in ES: = 1. / (ESESP-ESES).
SS2	= Z(128)	INPUT parameter controlling reflective (and axis) boundary treatment. Usually = 1. Used in PH2.
SS4	= Z(130)	INPUT parameter. If SS4 ≠ 0., REZONE is called on second cycle of run. Used in EDIT.
STAB	= Z(139)	INPUT parameter. Used in CDT. Initial value of "stability fraction" for the calculation of DT. If FINAL = 0., STAB is constant. Otherwise its value progresses from STAB to FINAL in a geometric progression.
STB	Local (c)	Used in PHj for shear stress at bottom of cell. Equivalenced to P(365).
STEZ	= Z(29)	INPUT parameter: E₀. Used in yield-strength calculation in PH3. See STRENG.
STK1	= Z(11)	INPUT parameter: Y₁. Used in yield-strength calculation in PH3. See STRENG.
STK2	= Z(28)	INPUT parameter: Y₂. Used in yield-strength calculation in PH3. See STRENG.
STL	= Z(106)	Used in PH3 for shear stress at left of cell.
STLX	Local	Used in PH3. = STL * X(I-1).
STR	Local (c)	Used in PH3 for shear stress at right of cell.
STRENG	Local	Calculated and used in PH3: yield strength of material. (Y₀, Y₁, Y₂ supplied by user.)

$$\text{STRENG} = (Y_0 + Y_1 \mu + Y_2 \mu^2) \cdot (1 - \frac{E}{E_0})$$

If STRENG < 0., stresses are set to 0.

If E > E₀, STRENG = 0.

Y₀ is JZERO,

Y₁ is STK1,

Y₂ is STK2,

ρ_0 is RHOZ,

E is AIX of cell,

E₀ is STEZ,

ρ is density of cell,

$\mu = \rho/\rho_0 - 1$.

STT	= Z(143)	Used in PH3 for shear stress at top of cell.
SUM	Local ^(c)	Used in PH2. Sums negative internal energy when negative internal energy is set to zero.
SUME	Local	Used in PH2. Sums energy changes.
SUM1	Local	Used in SETUP to define JRADA.
SUM2	Local	Used in SETUP to define JRADB.
T	= Z(84)	Time in seconds. Initially defined in INPUT. Incremented in CDT. Adjusted in EDIT for printing. Printed by CDT, EDIT, REZONE.
TARGI	= Z(72)	INPUT parameter. Initial value of specific internal energy of target. Used in SETUP and REZONE.
TARGV	= Z(52)	INPUT parameter. Initial value of axial-velocity of target. Used in SETUP and REZONE.
TARMAS	Local ^(c)	Used in EDIT. Total mass above JPROJ. Equivalenced to PR(4) in EDIT only.
TARMV	Local ^(c)	Used in EDIT. Total axial momentum above JPROJ. Equivalenced to PR(5) in EDIT only.
TARMVP	Local ^(c)	Used in EDIT. Total positive axial momentum above JPROJ. Equivalenced to PR(6) in EDIT only.
TAU	Global	Calculated in SETUP and REZONE. Area of cell face: $= \pi(X(I)^2 - X(I-1)^2)$. Used in most subroutines.

TAUDTS	Local	Used and calculated in PH1: = TAU*DT.
TAXRT	= Z(107)	INPUT parameter. Outer radius of target (in cms.). TAXRT should be at a cell-boundary. Used in SETUP and REZONE.
TAYBOT	= Z(88)	INPUT parameter. Axial location of bottom of target (in cms). TAYBOT should be at a cell-boundary. If no "target," TAYBOT = -1. Used in SETUP and REZONE.
TAYTOP	= Z(89)	INPUT parameter. Axial location of top of target (in cms). TAYTOP should be at a cell-boundary. Used in SETUP and REZONE.
TEPRO	Local ^(C)	Used in EDIT. Total energy below JPROJ. Equivalenced to PR(11) in EDIT only.
TESTRH	Global	Calculated in INPUT: = (.2)*RHOZ. Used in CDT in defining pressure scale factor.
TETAR	Local ^(C)	Used in EDIT. Total energy above JPROJ. Equivalenced to PR(3) in EDIT only.
TH03	Local	Used and calculated in PH3: = $\frac{1}{3} \left(\frac{\partial u}{\partial r} + \frac{\partial v}{\partial z} + \frac{u}{r} \right)$.
TIEPRO	Local ^(C)	Used in EDIT. Total internal energy below JPROJ. Equivalenced to PR(9) in EDIT only.
TIETAR	Local ^(C)	Used in EDIT. Total internal energy above JPROJ. Equivalenced to PR(1) in EDIT only.
TKEPRO	Local ^(C)	Used in EDIT. Total kinetic energy below JPROJ. Equivalenced to PR(10) in EDIT only.
TKETAR	Local ^(C)	Used in EDIT. Total kinetic energy above JPROJ. Equivalenced to PR(2) in EDIT only.
TMA	Local	Used in MAP to associate a given density with the printed symbol.
TNOW	Local	Used in EDIT: = time now; saved when EDIT calls CDT after calling REZONE.
TOPM	= Z(63)	Calculated in PH2. Printed in EDIT. Total mass lost out top of grid.

TOPMU	= Z(9)	Calculated in PH2. Printed in EDIT. Total radial-momentum lost out top of grid.
TOPMV	= Z(66)	Calculated in PH2. Printed in EDIT. Total axial-momentum lost out top of grid.
TOTSPH	Local	Used in SETUP. Total volume of sphere.
TRIAL	Local	Used in CDT. Maximum sound-speed or velocity used to define DT.
TRNSFC	= Z(145)	Defined in INPUT: = .4. Used in PH2 to define maximum transport velocity. (See UVMAX.)
TSTOP	= Z(50)	INPUT parameter. Value of T at which execution stops when stopping on time rather than cycles.
TWOPDT	Local	Calculated and used in PH2: = $2\pi \times DT$.
TWOPI	Global	Calculated in INPUT. Used in PH3: = 2π .
U	Global	Radial velocity of cell. (IMAX by JMAX array.)
UAMMP	Local	Used in PH2 for U of mass moving across right cell-edge.
UAMPY	Local	Used in PH2 for U of mass moving across top cell-edge.
UBAR	Local	Used in PH3 in calculating energy sum.
UEEF	Local	Used in PH2 to move tracer-points.
UK	Local ^(C)	Used in PH3. Temporary storage for part of U array.
UKT	Local	Used in PH3. Temporary storage for U(K).
UL	Local ^(C)	Used in PH1 for U on left. Used in EDIT for crater depth printout. Equivalenced as follows in standard OIL-RPM: UL(103) = CRAD (for EDIT) UL = RSN (for PH3) UL = FILEFT (for PH2) UL(103) = YAMC (for PH2)
UMIN	= Z(129)	Calculated in CDT. Used as velocity cutoff in PH2, PH3, and MAP: = (ROEPS)*(maximum sound-speed or velocity).

UMK	Local	Calculated and used in PH2. Temporary storage for $U(K)*AMX(K)$.
UMKP	Local	Calculated and used in PH2. Temporary storage for $U(K+1)*AMX(K+1)$.
UMOM	Local	Calculated and used in PH2: = MASS*U(K).
UNxxx	= Z(xxx)	Unused Z-storage.
UNEW	Local	Calculated and used in PH2. New value of U.
UOTK	Local	Calculated and used in PH2: = UMK/TAU(I).
UOTKP	Local	Calculated and used in PH2: = UMKP/TAU(I+1).
UOX	Local	Used in PH3: = U/X.
URR	Local (c)	Used in PH1 and PH2. Temporary storage for velocity and velocity averages.
USCLE	Local	Used in MAP as logarithmic scale factor of radial velocity map.
UVMAX	= Z(22)	Used and calculated in PH2. Maximum transport velocity. In radial direction UVMAX = TRNSFC*DX(I)/DT. In axial direction UVMAX = TRNSFC*DY(J)/DT.
V	Global	Axial velocity of cell. (IMAX by JMAX array.)
VABOVE	Local	Used in PH1 and PH2 as storage for velocity at top of cell.
VALUE	Local	Used in MAP in printing maximum value of each map symbol.
VAMMP	Local	Used in PH2 for axial velocity of mass moving across right cell-edge.
VAMPY	Local	Used in PH2 for axial velocity of mass moving across top cell-edge.
VBAR	Local	Used in PH3 in calculating energy sum.
VBLO	Local	Used in PH1 as storage for velocity at bottom of cell.
VEFF	Local	Used in PH2 to move tracer points.

VEL	Local	Used in PH1 as subcycle flag.
VFACT	Local	Used in PH3 in setting boundary conditions.
VINI	= Z(112)	INPUT parameter. Initial axial velocity of projectile. Used in SETUP and REZONE.
VINSPH	= Z(102)	INPUT parameter. Initial axial velocity of sphere. Used in SETUP. Equivalenced to Z(102) and EVAPMU in SETUP.
VK	Local (C)	Used in PH3. Temporary storage for part of V array.
VKT	Local	Used in PH3. Temporary storage for V(K).
VMK	Local	Calculated and used in PH2: = V(K)*AMX(K).
VML	Local	Calculated and used in PH2: = V(K+IMAX)*AMX(K+IMAX).
VNEW	Local	Calculated and used in PH2. New value of V.
VOLSPH	Local	Calculated and used in SETUP. Volume of toroid gen- erated by a cell. Used in setting up sphere.
VOW	Local	Calculated and used in ES. = (normal density)/(density of cell).
VSCLE	Local	Used in MAP as logarithmic scale factor for axial velocity map.
VT	= Z(55)	INPUT parameter. Used in PH2 as minimum mass flux (across top or right side of one boundary cell in one cycle) needed to trigger a rezone. Usually $VT \sim \rho_0 \times 10^{-4}$.
WDYF	Local	Used in PH2 as temporary storage for DY(J) or DY(J+1).
WFLAGF	Global	Used in INPUT and EDIT. Flags first cycle. Set = 1. in INPUT. Set = 0. in EDIT.
WFLAGL	Global	Used in MAIN and EDIT. Flags last cycle. Set = 1. in EDIT.
WFLAGP	Local (C)	Used in EDIT. Flags beginning of printout of pro- perties for each cell in a given column.

WS	Local (c)	Used in most subroutines for local working storage.
WSA	Local (c)	Used in most subroutines for local working storage.
WSB	Local (c)	Used in most subroutines for local working storage.
WSC	Local (c)	Used in most subroutines for local working storage.
WSD	Local	Used in PH2 local working storage.
WSMAX	Local	Used in MAP to define scale factors.
WSMIN	Local	Used in MAP to define scale factors.
WSOUT	Local	Used in PH2 for adjusting overemptied cells.
WT	Local	Used in CDT for local working storage.
WTA	Local	See WT.
WTB	Local	See WT.
X	Global	Distance (cms) from axis to outside of cell. Equivalenced to XX array such that X(0) = XX(1).
XIENRG	= Z(140)	Total internal energy. Calculated in EDIT and used for printing labels on tracer point plots.
XKENRG	= Z(141)	Total kinetic energy. Calculated in EDIT and used for printing labels on tracer point plots.
XL2	Local	Calculated and used in SE1UP for placing sphere: $= (X(I-1))^2$.
XMAX	= Z(18)	Calculated in SETUP: = X(IMAX).
XP	Global	Tracer-point x-coordinates. Used in INPUT, SETUP, EDIT, PH2 and REZONE.
XR2	Local	Calculated and used in SETUP for placing sphere: $= (X(I))^2$.
XTENRG	= Z(142)	Total energy. Calculated in EDIT and used for printing labels on tracer point plots.
XUM	Constants	Used in MAP. Has negative alphabetic characters for maps. Defined in DATA statement.

XX	Global	Equivalenced to X array so as to make X(0) available.
Y	Global	Distance (cms) from bottom of grid to top of cell. Equivalenced to YY array such that Y(0) = YY(1).
Y2	= Z(81)	INPUT tracer point flag: when = -2, tracer points are calculated; when = 0, tracer points not calculated.
YAMC	Local (c)	Calculated and used in PH2. Axial momentum of mass moving across 1 ft side of cell. Equivalenced to UL(103). (See Appendix B)
YBOTTM	Local	Calculated and used in SETUP in placing sphere: = Y(J-1).
YC2	Local	Calculated and used in SETUP in placing sphere: = (YCENTR) ² .
YCENTR	= PK(13) = Z(163)	INPUT parameter. Distance (cms) of center of sphere from bottom of grid. YCENTR must be at a cell- boundary. Used in SETUP. Equivalenced to PK(13) in SETUP only.
YDIFFB	Local	Calculated and used in SETUP in placing sphere.
YDIFFI	Local	Calculated and used in SETUP in placing sphere.
YDIFO	Local	Calculated and used in SETUP in placing sphere.
YDIFTT	Local	Calculated and used in SETUP in placing sphere.
YLINTA	Local	Calculated and used in SETUP in placing sphere.
YLINTB	Local	Calculated and used in SETUP in placing sphere.
YLLOWER	Local	Calculated and used in SETUP in placing sphere.
YMAX	Local	Calculated in SETUP: = Y(JMAX).
YP	Global	Tracer-point y-coordinates. Used in INPUT, SETUP, EDIT, PH2 and REZONE.
YRINTA	Local	Calculated and used in SETUP in placing sphere.
YRINTB	Local	Calculated and used in SETUP in placing sphere.
YTOP	Local	Calculated and used in SETUP in placing sphere.

YUPPER	Local	Calculated and used in SETUP in placing sphere.
YY	Global	Equivalenced to Y array so as to make Y(0) available.
Z	Special	Storage for most of the input parameters. The Z-array
	Global	(150 words) is written on tape for restarts. Used in INPUT, MAIN, and SETUP. (See Appendix A)

APPENDIX A
Z-STORAGE LISTED NUMERICALLY

See Dictionary for meaning and use.

*1. PROB	30. NC	59. UN59
2. CYCLE	31. UN31	60. N10
3. DT	32. NRC	61. N11
4. NUMSP	2*33. IMAX	62. GAMMA
2*5. NFRELP	34. IMAXA	63. TOPM
2*6. NDUMP7	2*35. JMAX	64. ROTMU
2*7. ICSTOP	36. JMAXA	*65. SN
8. PIDY	37. KMAX	66. TOPMV
9. TOPMU	38. KMAXA	*67. PRYBOT
10. RTMU	39. BOTM	*68. PRYT
*11. STK1	40. BOTMV	*69. PRXRT
2*12. NUMREZ	41. NUMSPT	*70. CYCPH3
13. ET4	*42. CZERO	*71. REZFCT
14. UN14	2*43. NUMSCA	*72. TARGI
*15. RHINIT	*44. PRLIM	*73. PROJU
*16. PROJI	*45. REDELT	74. BBOUND
17. UN17	*46. PRFACT	*75. EVAP
18. XMAX	2*47. I1	76. ECK
19. NZ	2*48. I2	77. NECYCL
20. NREZ	2*49. IPCYCL	78. II
*21. AMDM	1*R 50. TSTOP	79. TJ
22. UVMAX	*51. RHOFL	80. NMP
23. UN23	*52. TARGV	*81. Y2
*24. DMIN	53. N3	82. EZPH1
2*25. JSTR	2*54. IVARDY	2*83. IVARDX
26. DTNA	55. VT	84. T
*27. CVIS	2*56. N6	2*85. NMFMX
*28. STK2	57. RTM	86. FMIN
*29. STEZ	58. PTMV	2*87. INTER

* User-supplied input-values.

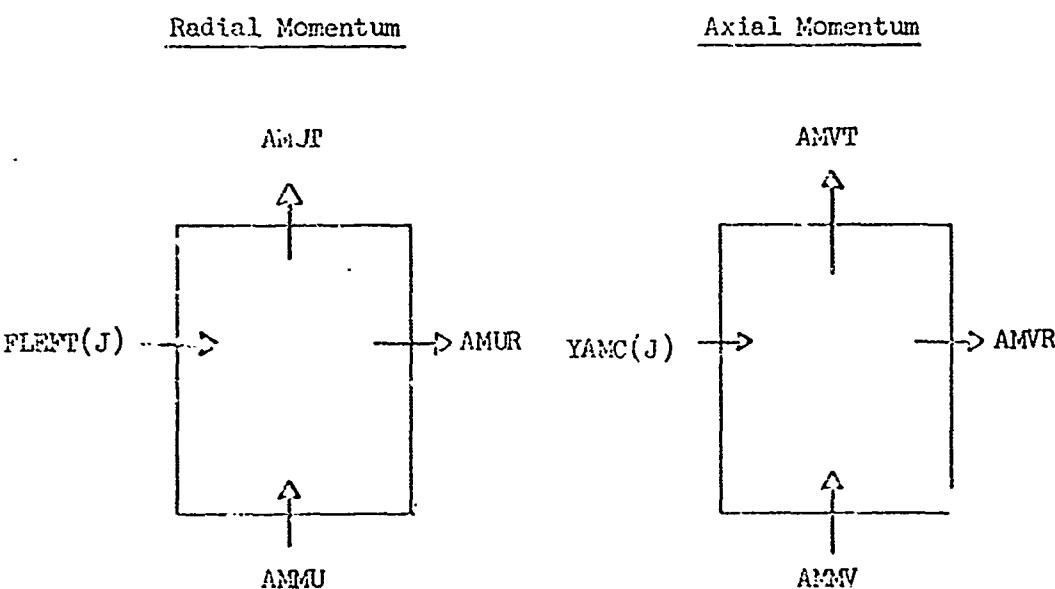
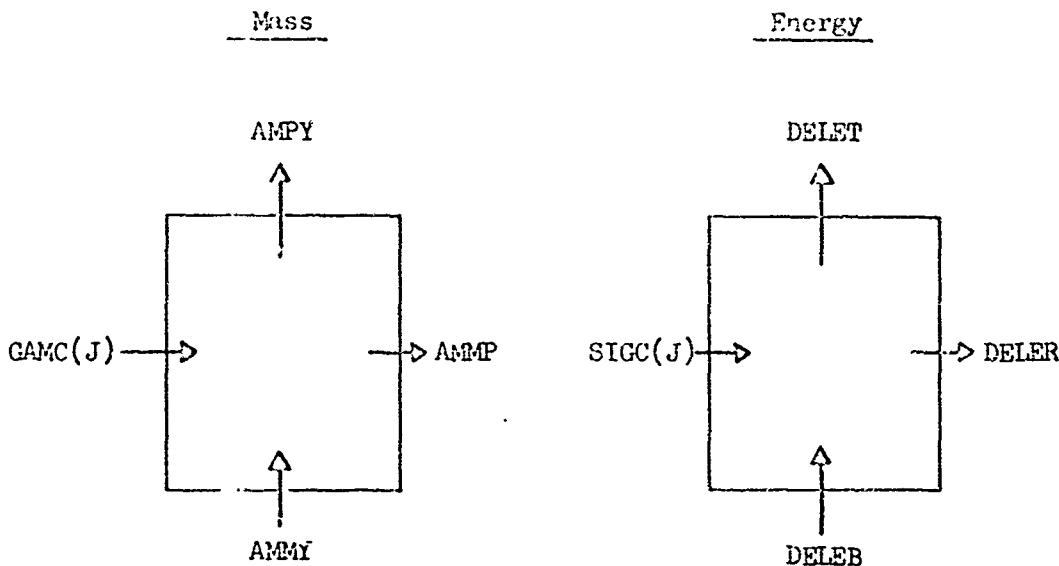
2* Must have a "2" in column 1.

1* Must have a "1" in column 1.

R Must be included in a restart input input deck.

*88. TAYBOT	*122. ESES	*R153. PK(3): When = -1., program will restart from tape and do a "long" EDIT print of the pickup cycle. When = -2., program will restart from tape and do a "short" EDIT print of the pickup cycle.
*89. TAYTOP	*123. ESALPH	
90. IEMAP	*124. ESBETA	
91. MC	*125. ESCAPB	
92. MR	126. IUMAP	
93. MZ	127. SS1	
94. MB	128. SS2	
95. REZ	129. UMIN	*162. Radius of sphere (RADIUS).
2*96. NODUMP	*130. SS4	*163. Y-center of sphere (YCENTR).
97. UN97	131. PRTIME	1*164. When Z(164) > 0. CARDS will be called by SETUP to read "special" input. (See "OIL- RPM Input for Special Setup" on page 23.)
98. UN98	132. EOR	
99. UN99	133. EOT	
*100. EVAPM(RHOSPH)	134. EOB	
*101. EVAPEN(SIESPH)	135. EMOR	
*102. EVAPMU(VINSPH)	*136. DXF	
*103. EVAPMV(RHOOUT)	*137. DYF	
104. EZPH2	*138. RHOMIN	
105. SNL	*139. STAB	
106. STL	140. XIENRG	
*107. TAIRT	141. XKENRG	
108. IDNMAP	142. XTENRG	
109. IPRMAP	143. STP	
*110. ROEPS	*144. DTMIN	
*111. RHINI	145. TRNSFC	
*112. VINI	146. EMOT	
*113. FINAL	2*147. JPROJ	
114. IVMAP	148. CNAUT	
*115. RHOZ	*149. BBAR	
*116. ESA	1*150. EMOB = 0 (Last card of input unless restarting from tape.)	
*117. ESEZ	PK array follows the Z array in Blank Common; so PK(1) from the beginning of Blank Common is equivalent to Z(151).	
*118. ESB		
*119. ESCAPA		
*120. ESESP	i*151. PK(1) should be the same as PROB.	
*121. ESESQ	*R152. Cycle to restart on.	

APPENDIX B
VARIABLES USED FOR FLUXES ACROSS CELL BOUNDARIES



REFERENCES

1. Evans, M.W. and F.H. Harlow, "The Particle-in-Cell Method for Hydro-dynamics Calculations," Los Alamos Scientific Laboratory Report LA-2139, November 1957.
2. Johnson, W.E., "Computer Development to Improve SHELL Code," General Atomic Report GA-4673, Contract AF29(601)-6028, October 1963.
3. Johnson, W.E., "OIL, A Continuous Two-Dimensional Eulerian Hydrodynamic Code," General Atomic Report GAMD-5580, October 1964.
4. Tillotson, J.H., "Metallic Equations of State for Hypervelocity Impact," General Atomic Report GA-3216, July 1962.
5. Dienes, J.K., W.E. Johnson and J.M. Walsh, "Annual Status Report on the Theory of Hypervelocity Impact," General Atomic Report GA-6509, June 1965.
6. Allen, R.T., "Equation of State of Rocks and Minerals," General Atomic Report GAMD-7834, March 1967.
7. Walsh, J.M., J.H. Tillotson and W.E. Johnson, "Theory of Hypervelocity Impact, Quarterly Progress Report," General Atomic Report GACD-4518, July 1963.
8. Dienes, J.K. and M.W. Evans, "Cratering Calculations with a Hydrodynamic Strength Code," General Atomic Report GAMD-7369, September 1966.